

Simulation of the Manufacturing and Serviceability of Continuous Fiber-reinforced Plastics

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Webinar: Composite Analysis
02.04.2014

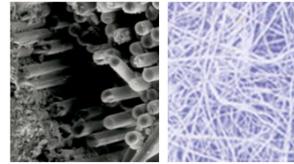
DYNA
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Composites

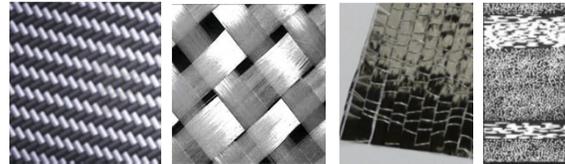
- A composite is a combination of two or more materials, differing in form or composition on a macroscale. The constituents do not dissolve or merge completely into one another, but can be physically identified and exhibit an interface.



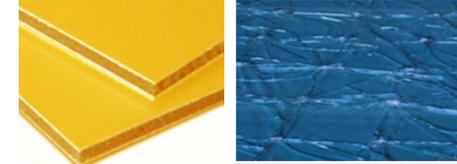
Concrete
(cement/stone/steel)



Short/long fiber
reinforced polymers
(glass/PP)



Endless fiber
reinforced polymers
(glass/carbon/PA/PP/EP)



Sandwich/Laminates
(alloy/polymer/..glass/PVB/...)



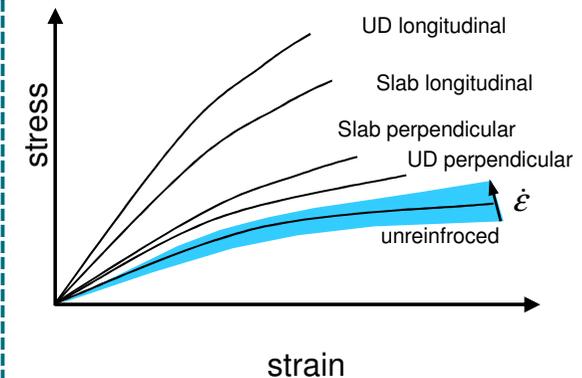
Characteristic structure of fiber reinforced plastics

- Fiber **size** and **geometry** have significant influence on the part performance.
- Fibers show higher strength and stiffness than material in bulk form
 - Fewer internal defects
 - Aligned crystalline structure
- Strongly anisotropic tensile response
 - Typical stiffness ratio: 20:1 – 100:1
 - Fibers linear elastic, matrix non-linear

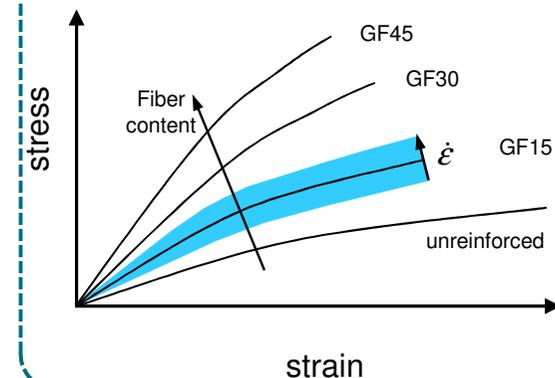


A thorough understanding of the manufacturing process is extremely important

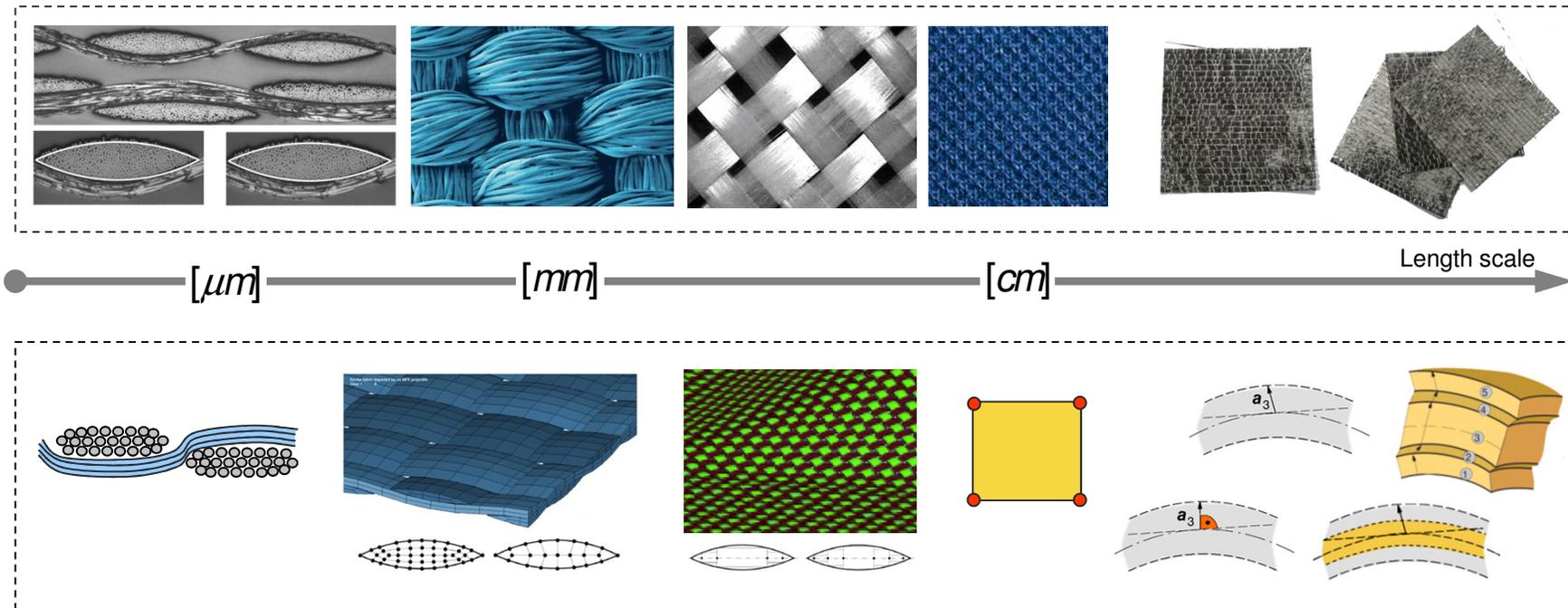
dependence on fiber orientation



dependence on fiber content



Length scale and modeling techniques



- The modeling strategy is to be defined based on
 - the length scale
 - the effects to be captured by the simulation



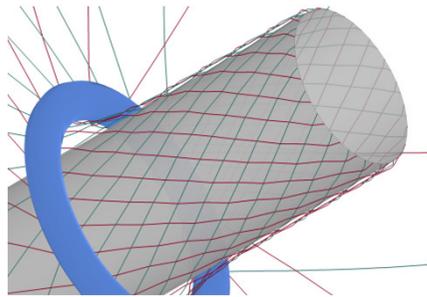
Agenda

- Process simulation
 - Winding and Braiding
 - Draping
 - Thermoforming

- Crashworthiness analysis
 - Short and long fiber reinforced plastics
 - Continuous fiber reinforced plastics

- Mapping

- Summary

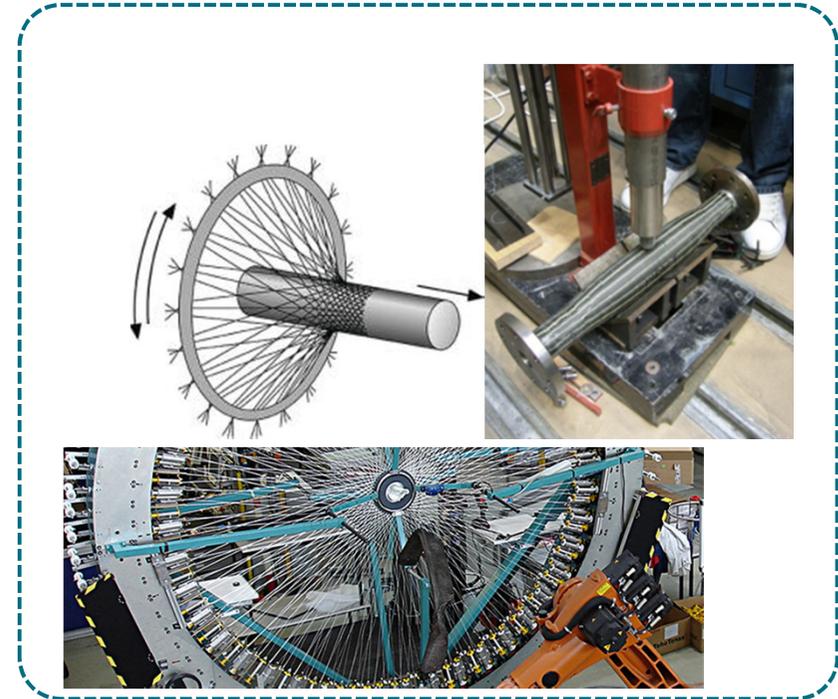


Producibility Winding and Braiding

Winding and Braiding



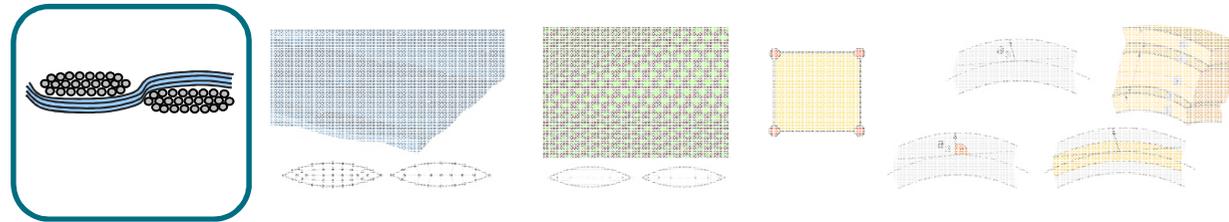
[ICD/ITKE, Uni Stuttgart]



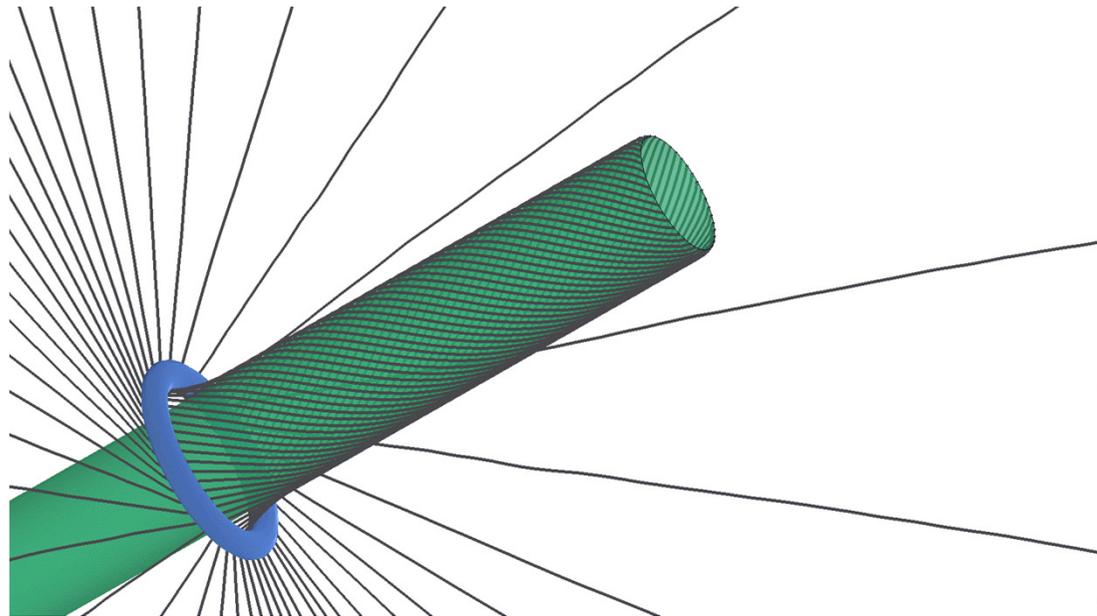
[IFB, Uni Stuttgart]

- Exact positioning and orientation of fibers for complex geometries
- Thorough planning of the manufacturing process is required

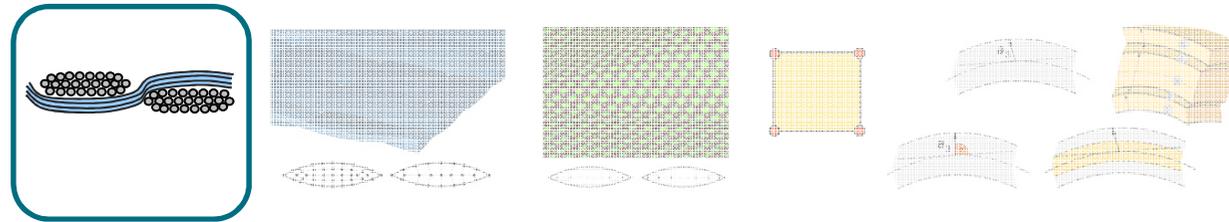
Winding and Braiding - Simulation



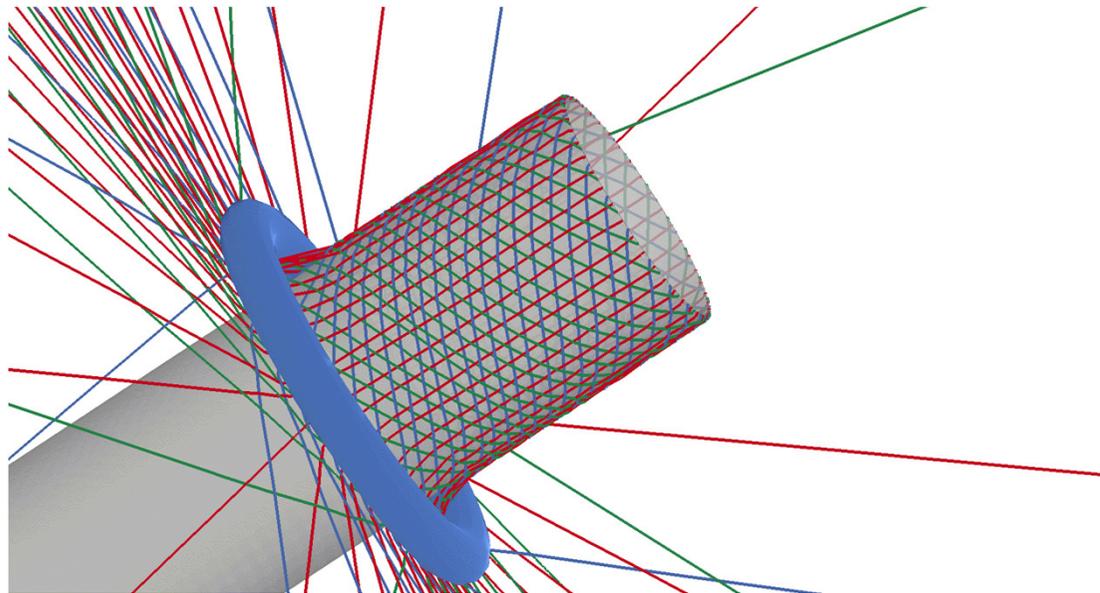
- 21 yarns
- 21543 beam elements
- 1 part
- Simple rotation of the fibers
- Braiding core is pushed through the braiding ring



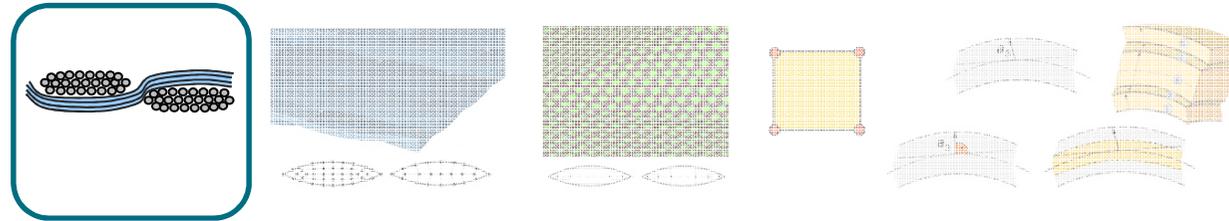
Winding and Braiding - Simulation



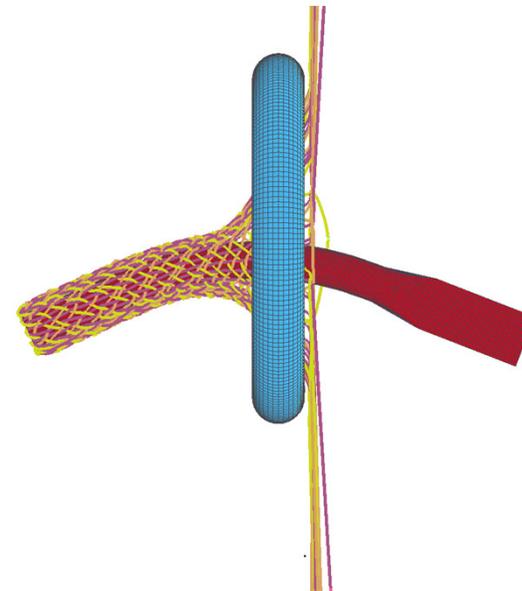
- 84 yarns
- 174348 beam elements
- 3 parts
- Half the elements used as UD – reinforcement
- Fibers are rotated and then moved to create the braiding-pattern
- Braiding core is pushed through the braiding ring



Winding and Braiding - Simulation



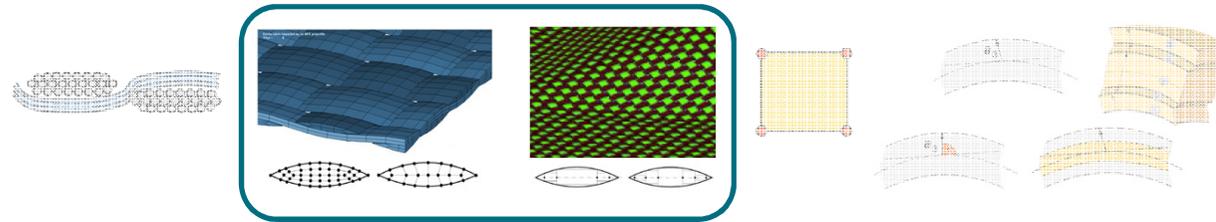
- 48 yarns
- 25236 beam elements
- 48 discrete elements
- 6 parts
- Fibers are rotated and then moved to create the braiding-pattern
- Braiding core is pushed through the braiding ring



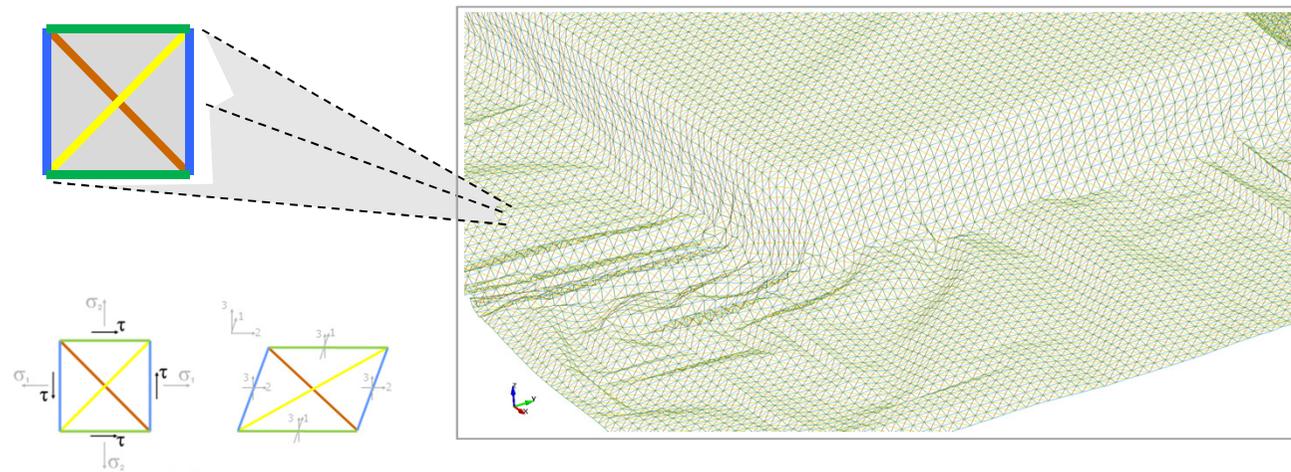


Producibility Draping

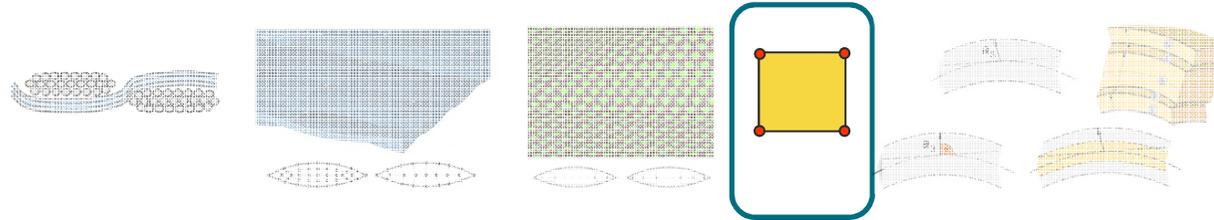
Draping – Simulation with discrete elements



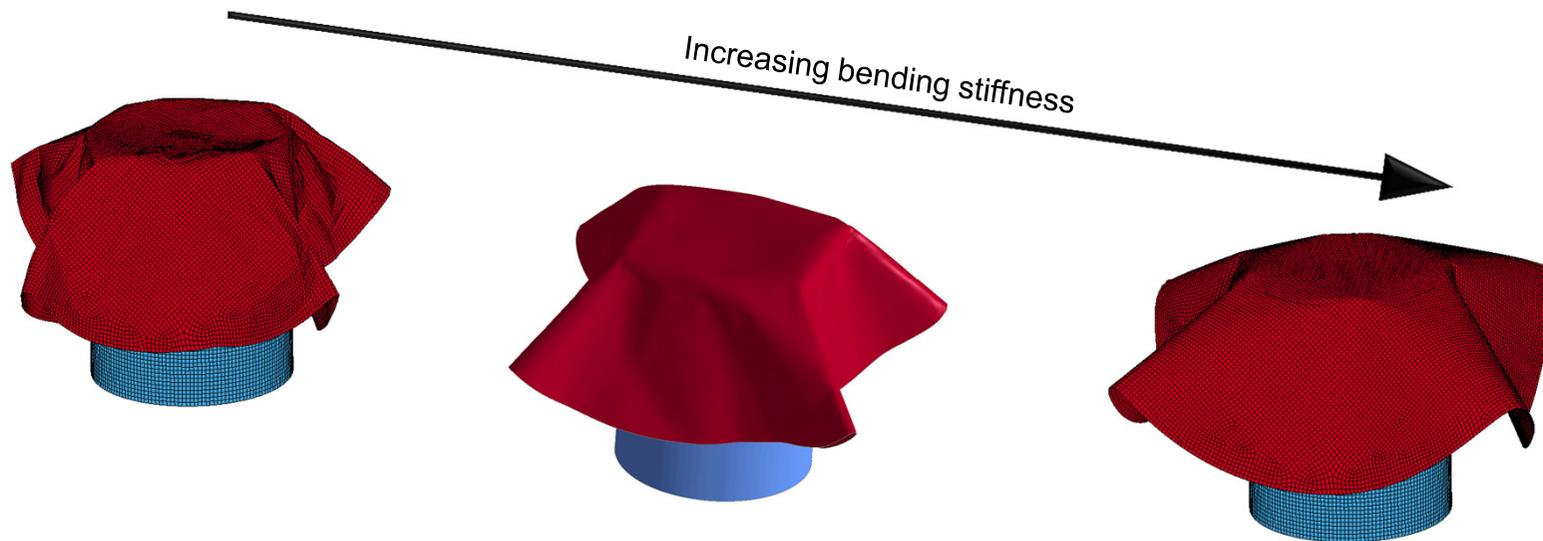
- Warp and weft direction *MAT_LINEAR_ELASTIC_DISCRETE_BEAM
- Diagonal behavior modeled with *MAT_CABLE_DISCRETE_BEAM
- This approach allows to model positive and negative shear loading



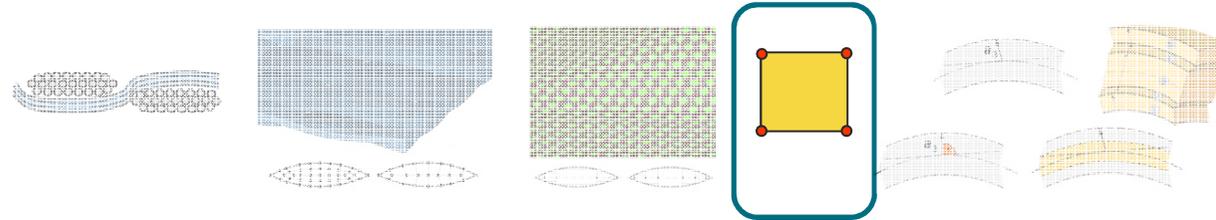
Draping – *MAT_034 (*MAT_FABRIC)



- Material describes an orthotropic material behavior
- Requires discretization with membrane elements
- Allows to add a bending resistance by defining an additional elastic

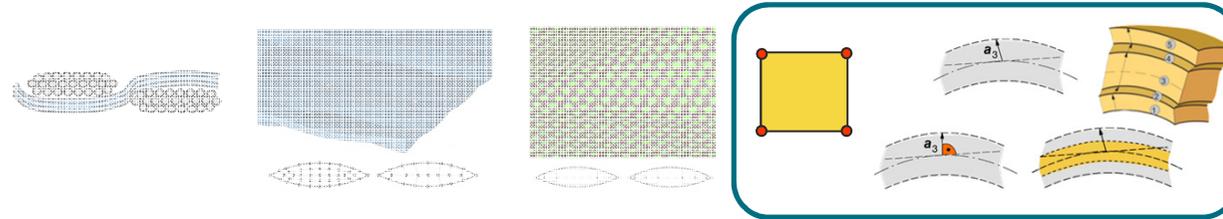


Draping – *MAT_234 / *MAT_235

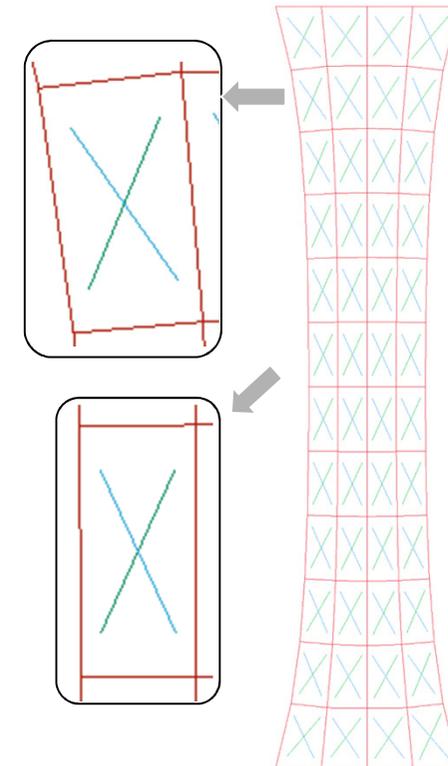


- *MAT_234 (*MAT_VISCOELASTIC_LOOSE FABRIC)
 - Micromechanical approach
 - Mathematical description for geometry and kinematic of symmetrical woven fabric
 - Looking angle is taken into account
 - Viscoelastic enhancement for higher shear strain
- *MAT_235 (*MAT_MICROMECHANICS_DRY_FABRIC)
 - Micromechanical approach with homogenization strategy (RVE)
 - Mathematical description of symmetrical woven fabric
 - Looking angle is taken into account

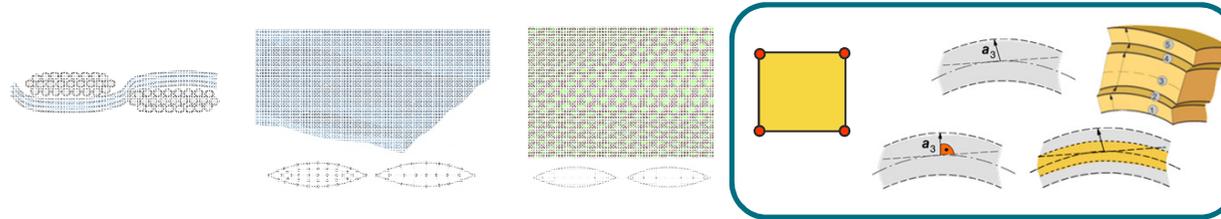
Draping – *MAT_249



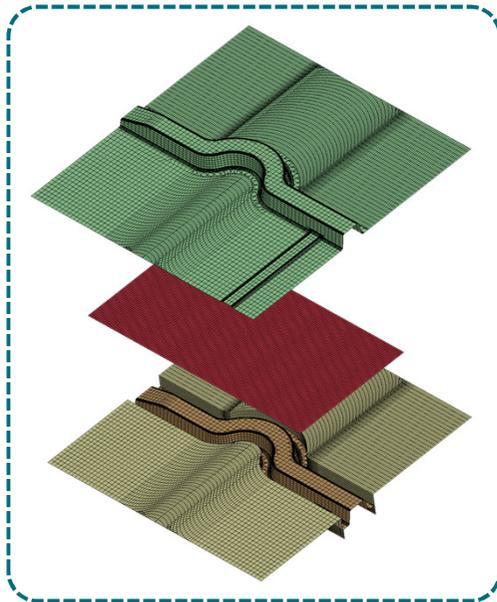
- *MAT_249
 - Macroscopic, hyperelastic and anisotropic material formulation
 - Up to three different fiber families can be defined in any integration point
 - Stress-strain response for tension and compression given as load curve
 - Non-linear elasto-plastic shear behavior also defined by load curve input
 - Contains thermo-elasto-plastic material for thermoplastic matrix



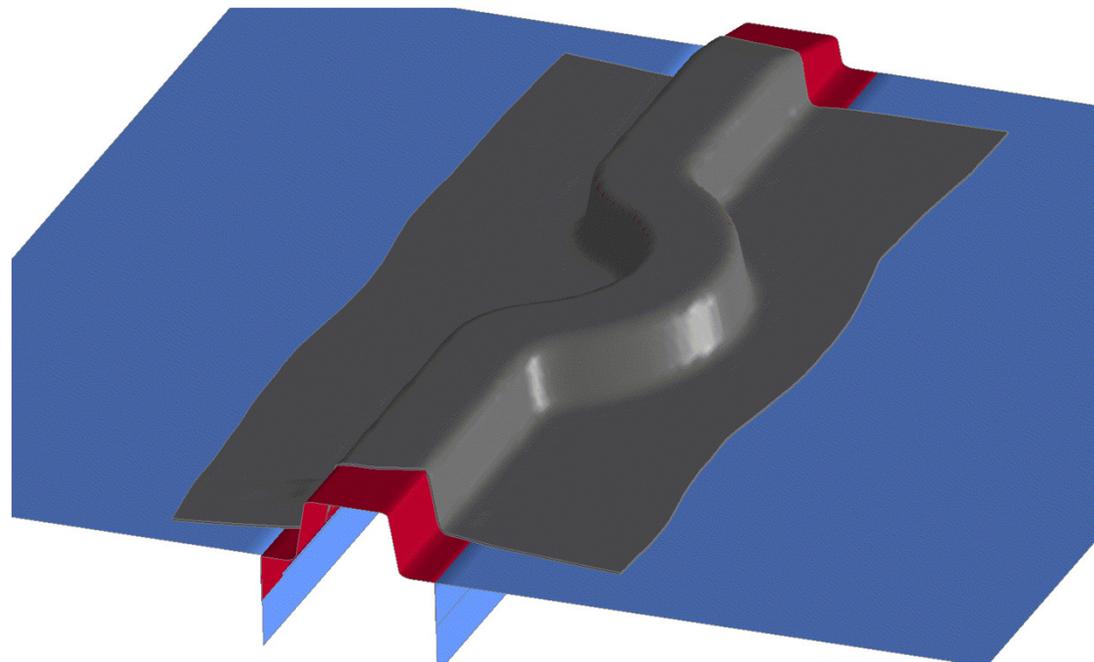
Draping – *MAT_249



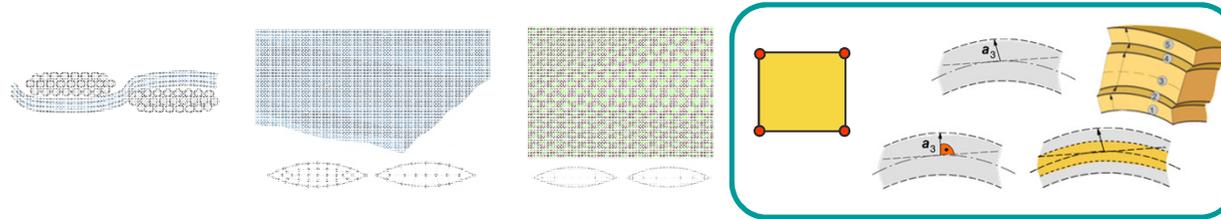
- S-Rail Example



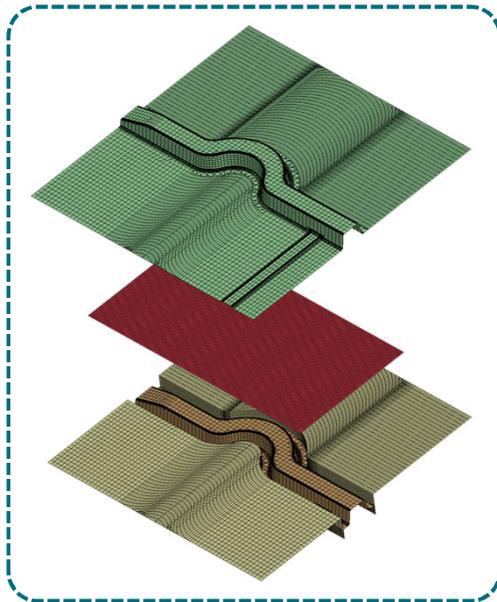
geometry:
Benteler-SGL



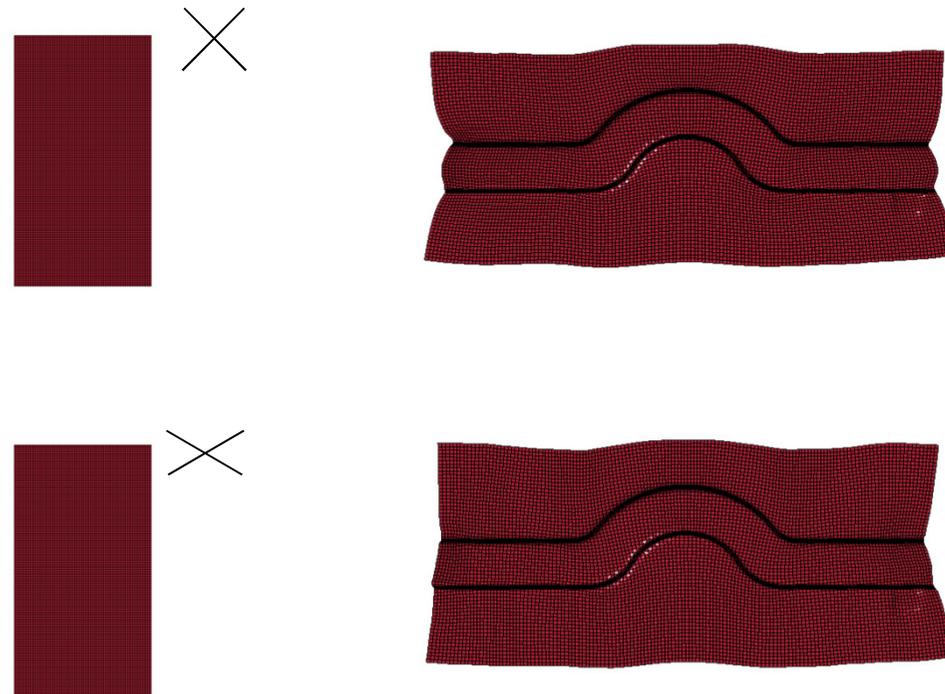
Draping – *MAT_249



- S-Rail Example



geometry:
Benteler-SGL

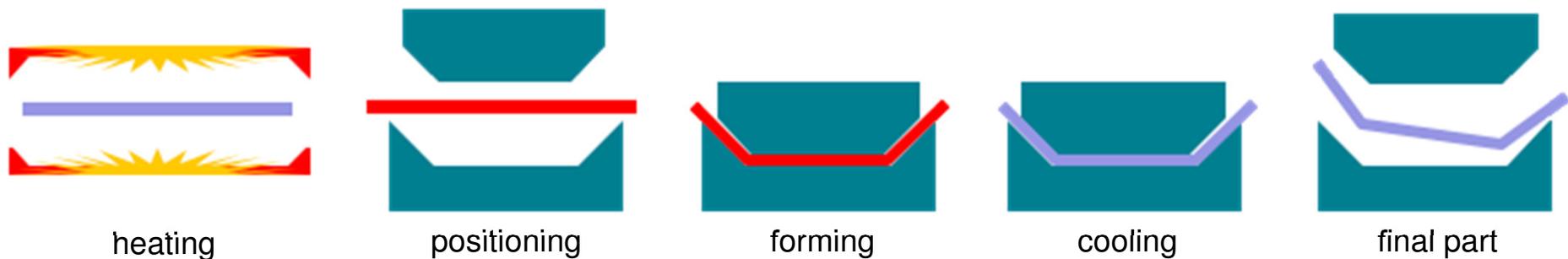




Producibility Organo sheet

Thermoplastic pre-pregs – process overview

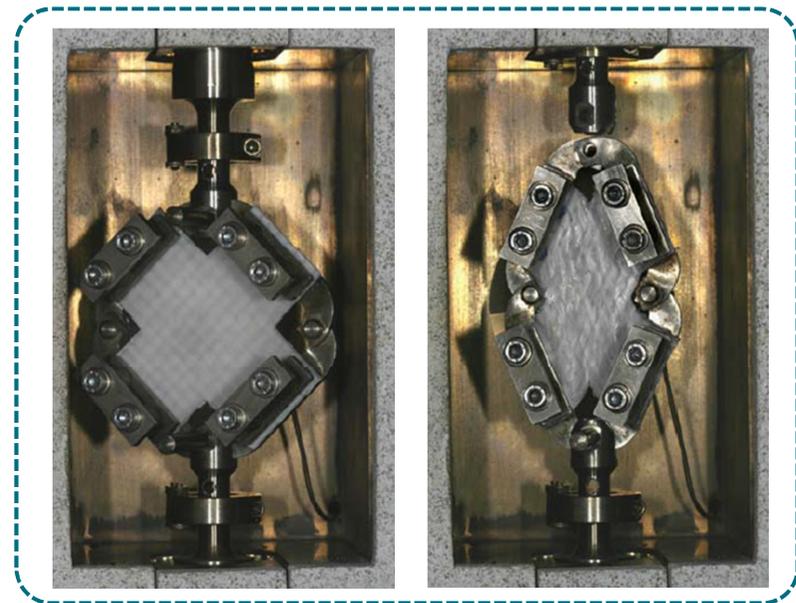
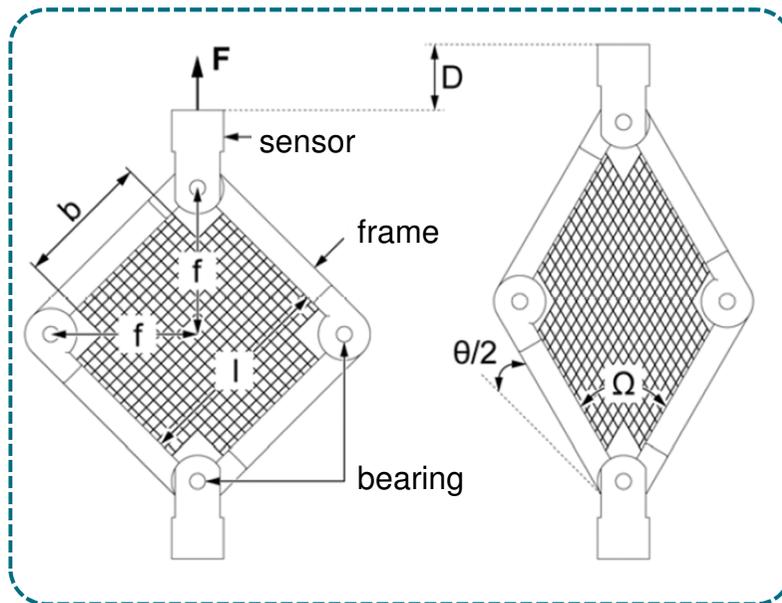
- Properties of thermoplastic matrix material
 - At high temperature, molten material behaves like a viscous fluid
 - At low temperature, material can be described as an elasto-plastic solid
- Process overview



- Process is reversible as no chemical curing occurs
- Relatively short cycle times can be realized

Thermoplastic pre-pregs – picture frame test

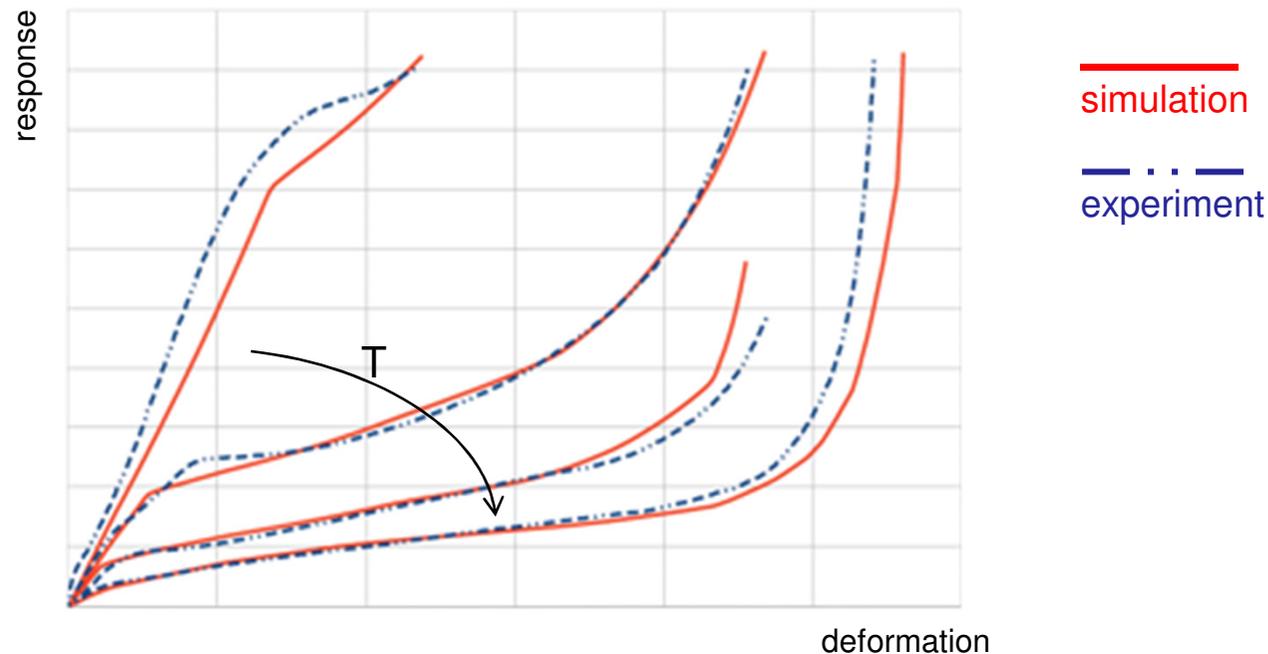
- Standard experimental set-up to characterize shear behavior
- Results show significant temperature dependence
 - At low temperature, matrix material dominates
 - At high temperature, behavior similar as for dry fabric material



Thermoplastic pre-pregs – Validation



- Picture frame test is simulated for different temperatures
- Simulation result show good agreement with experimental data
 - Realistic non-linear shear behavior of fabric (highest temperature)
 - Effect of matrix curing with decreasing temperature is well captured





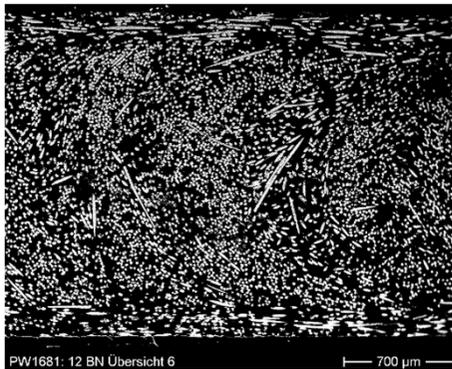
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Serviceability Short and long fibers

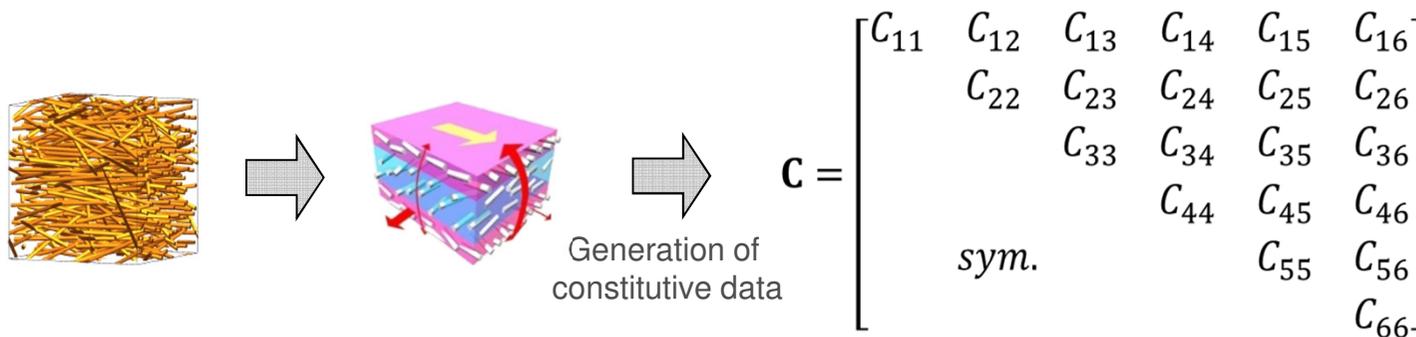
Anisotropic elastic solution with MAT_002_ANIS

New!

- Hyperelastic (total) formulation using Green-Lagrange strain \mathbf{E}

$$\boldsymbol{\sigma} = J^{-1} \mathbf{F} \cdot \mathbf{S} \cdot \mathbf{F}^T = J^{-1} \mathbf{F} \cdot \mathbf{C} \cdot \mathbf{E} \cdot \mathbf{F}^T$$

- Elastic-anisotropic behavior, stiffness matrix with 21 independent coefficients:



- Several possibilities to define material directions, e.g. AOPT, ELEMENT_SOLID_ORTHO, ...
- No plasticity, no damage, no failure (but: brittle failure possible via *MAT_ADD_EROSION)

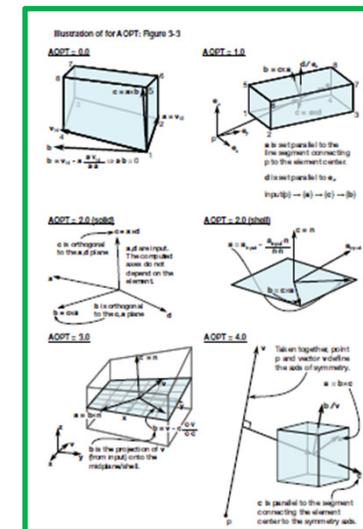
*MAT_(ANISO)TROPIC_ELASTIC



CARD #1	mid	ro	c11	c12	c22	c13	c23	c33
CARD #2	c14	c24	c34	c44	c15	c25	c35	c45
CARD #3	c55	c16	c26	c36	c46	c56	c66	aopt
CARD #4	xp	yp	zp	a1	a2	a3	macf	ihis
CARD #5	v1	v2	v3	d1	d2	d3	beta	ref

$$\sigma_{ij} = C_{ijkl} \epsilon_{kl}$$

- C_{ij} : constants in the 6x6 anisotropic constitutive matrix
- **AOPT**: usual options to define the material's coordinate system
- **ihis**: flag for element-wise definition of the stiffness tensor with *INITIAL_STRESS_SOLID



*INITIAL_STRESS_SOLID

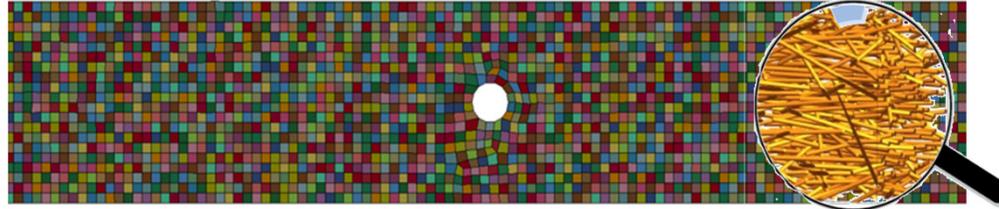


CARD #1	eid	nint	nhisv	large	iveflg	ialegp	nthint	nthhsv	
CARD #2	sigxx		sigyy		sigzz		sigxy		sigyz
CARD #3	sigzx		eps		hisv1		hisv2		hisv3
CARD #4	hisv4		hisv5		hisv6		hisv7		hisv8
CARD #5	hisv9		hisv10		hisv11		hisv12		hisv13
CARD #6	hisv14		hisv15		hisv16		hisv17		hisv18
CARD #7	hisv19		hisv20		hisv21				

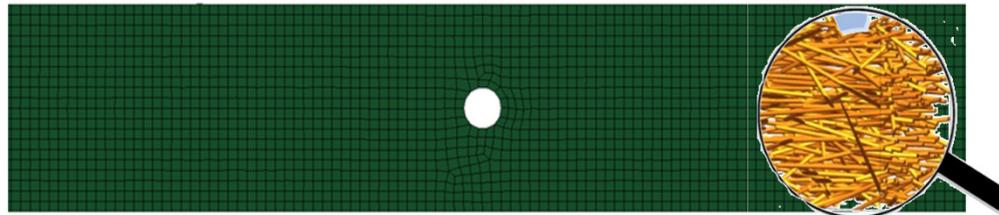
- The matrix entries C_{ij} are written onto the history variables per integration point.
- Setting `ihisv=21` in `MAT_002` will take into account the fully anisotropic stiffness tensor (e.g. `hisv#1` – `hisv#21` have to be defined in `DYNAIN` for instance)

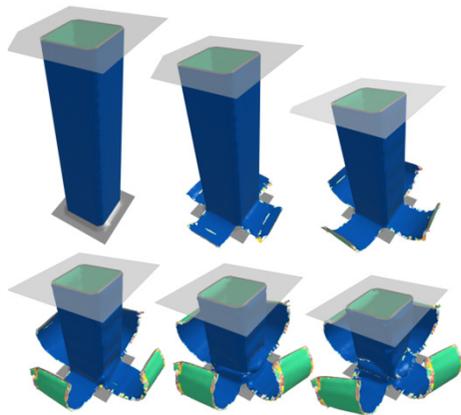
Anisotropic elastic solution with MAT_002_ANIS

- Direct input in material card
 - Drawback: inhomogeneous distribution (e.g. from previous short fiber filling simulation) in component needs individual part definition for every element



- Initialization with *INITIAL_STRESS_SOLID (new option in next Release R7.1)
 - Only one part definition for whole component. Anisotropic coefficients are part of material's history field and can therefore be initialized for each integration point individually.

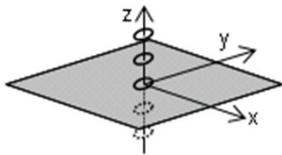




Serviceability Continuous fiber reinforced plastics

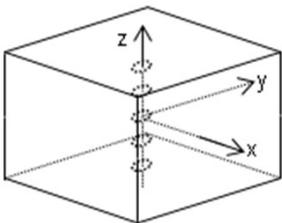
Composite damage – modeling aspects

intralaminar



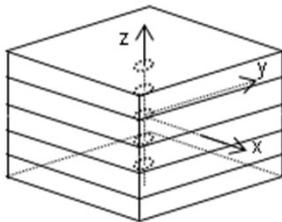
layered thin shell elements

- + numerical „cheap“ (thickness has no influence on critical time step size)
- + combination of single layers to sublaminates
- no stresses in thickness dir.



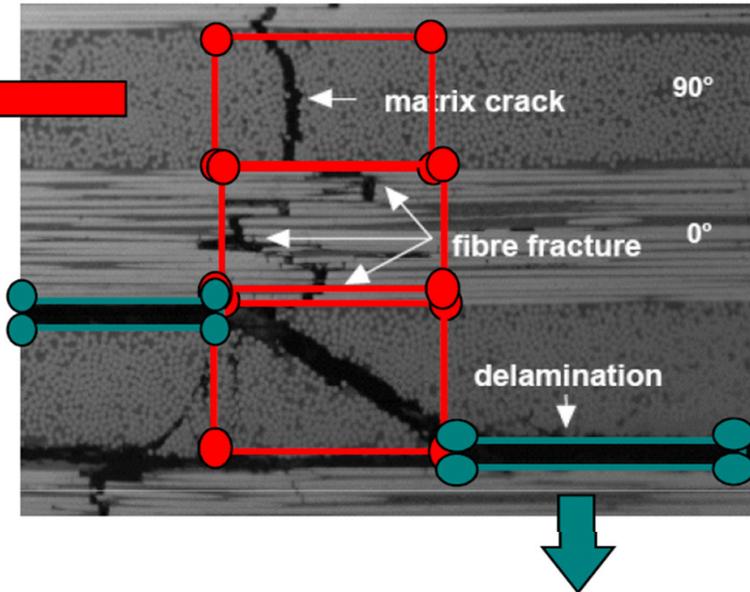
layered thick shell elements

- + 3D stress state
- + combination of single layers to sublaminates
- thickness influences the critical time step size



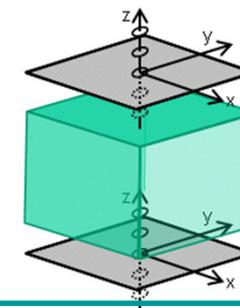
solid elements

- + 3D stress state
- one element for every single layer
- numerical „expensive“



interlaminar

- cohesive elements
- tiebreak contacts



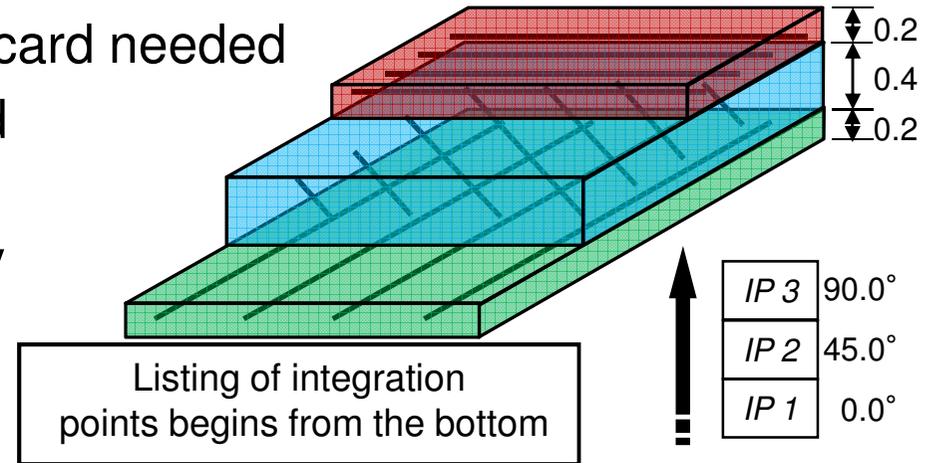
layered thin shell element

cohesive element

layered thin shell element

Ply definition with *PART_COMPOSITE(_TSHELL)

- Part-wise definition of lay-ups
- No *SECTION_SHELL-keyword card needed
- Material models, thicknesses and angles are defined for each layer
- Add as many cards as necessary

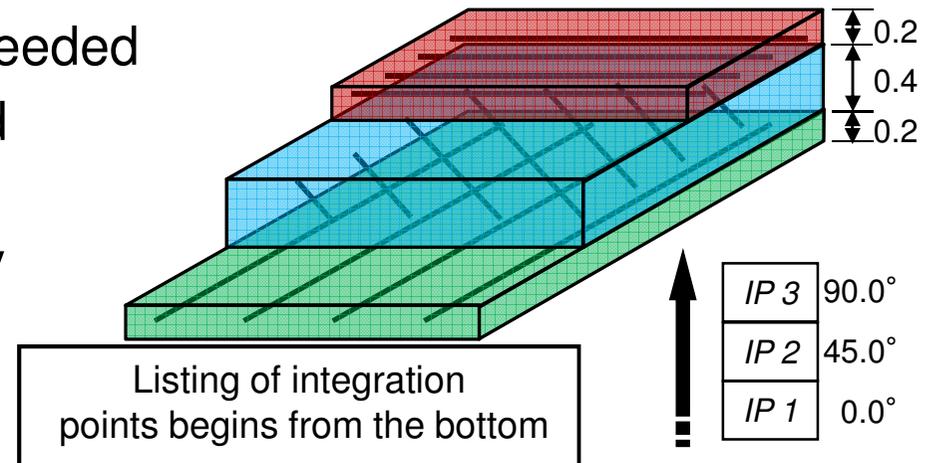


*PART_COMPOSITE (_TSHELL)

	1	2	3	4	5	6	7	8
Card 1	PID	ELFORM	SHRF	NLOC	MAREA	HGID	ADOPT	
	28	2	0.0	0.0				
Card 2	MID1	THICK1	BETA1		MID2	THICK2	BETA2	
	1	0.2	0.0		2	0.4	45.0	
Card 3	MID3	THICK3	BETA3		MID4	THICK4	BETA4	
	3	0.2	90.0					
...								

Ply definition with *ELEMENT_(T)SHELL_COMPOSITE

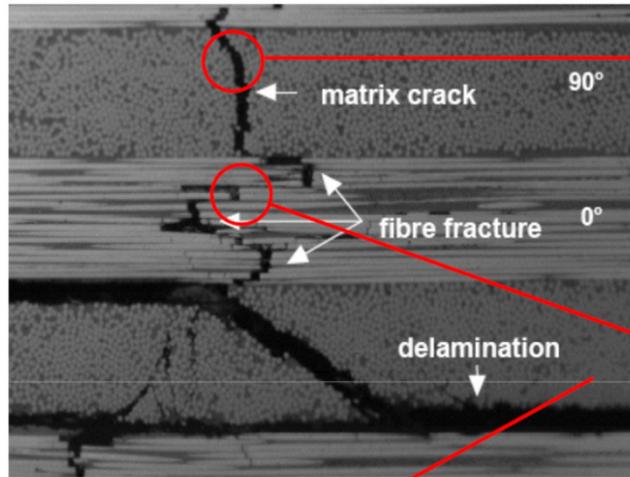
- Element-Wise definition of lay-ups
- *SECTION_SHELL-keyword is needed
- Material models, thicknesses and angles are defined for each layer
- Add as many cards as necessary
- Allows the definition of different lay-ups within one part



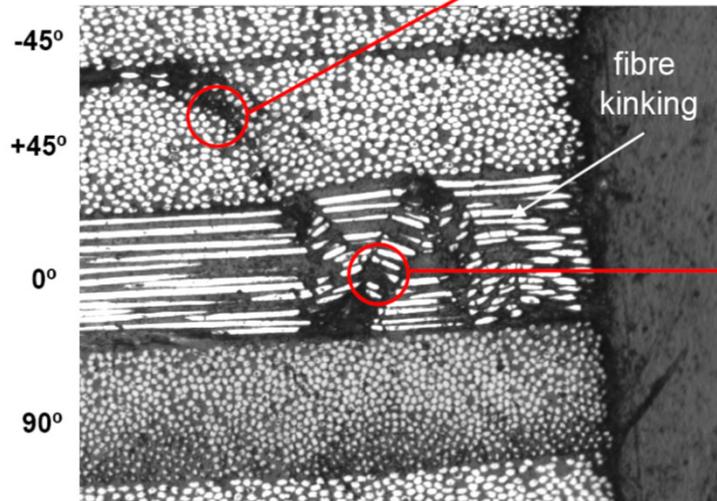
*ELEMENT_(T)SHELL_COMPOSITE

	1	2	3	4	5	6	7	8	9	10
Card 1	EID	PID	N1	N2	N3	N4	N5	N6	N7	N8
	1	2	3	4	5	6	7	8		
Card 2	MID1	THICK1	BETA1		MID2	THICK2	BETA2			
	1	0.2	0.0		2	0.4	45.0			
Card 3	MID3	THICK3	BETA3		MID4	THICK4	BETA4			
	3	0.2	90.0							
...										

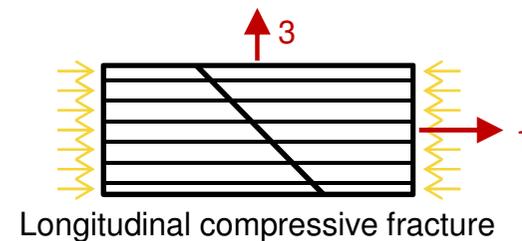
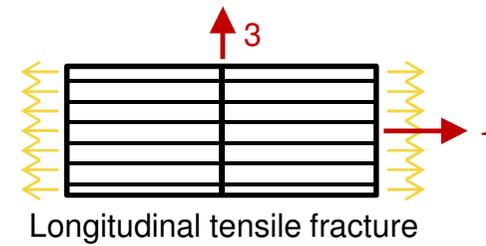
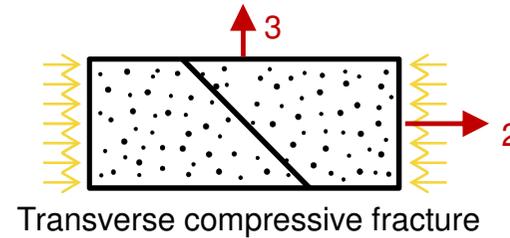
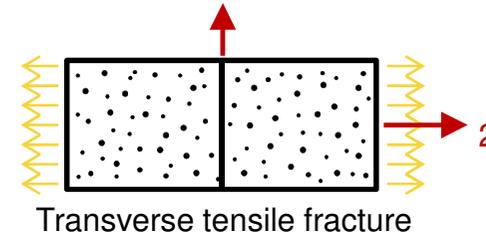
Failure mechanisms in fiber reinforced composites



R Olson,
Imperial College
London



PP Camanho,
PhD thesis, Imperial College London



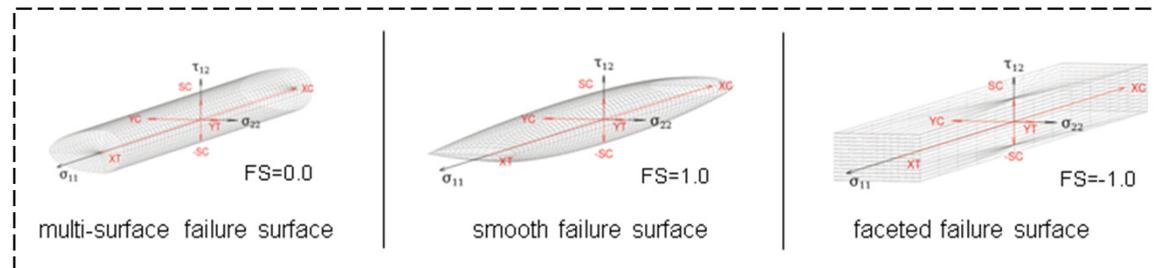
LS-DYNA: Available models for composite structures

- *MAT_022: (*MAT_COMPOSITE_DAMAGE)
 - plane stress
 - Chang-Chang failure criteria: fiber tension, matrix tension/compression
 - fiber compression is missing
 - “sudden” failure: $E1, E2, \nu_{12}, G_{12} = 0.0$

- *MAT_054/055: (*MAT_ENHANCED_COMPOSITE_DAMAGE)
 - plane stress
 - failure criteria (54: Chang-Chang – 55: Tsai-Wu):
fiber tension/compression, matrix tension/compression
 - failure: stresses kept constant till failure strain reached,
then: $E1, E2, \nu_{12}, G_{12} = 0.0$

LS-DYNA: Available models for composite structures

- *MAT_058: (*MAT_LAMINATED_COMPOSITE_FABRIC)
 - plane stress
 - Hashin failure criteria: fiber tension/compression, matrix tension/compression
 - exponential damage model

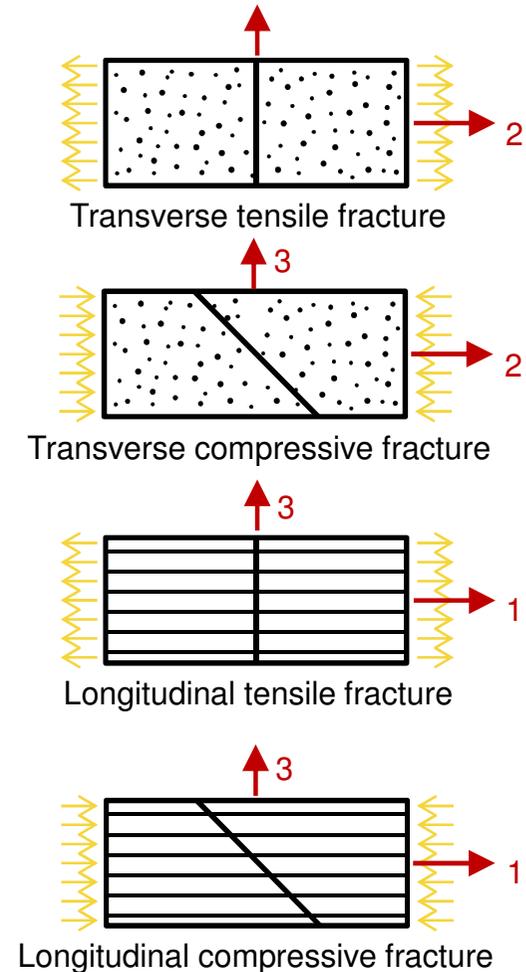
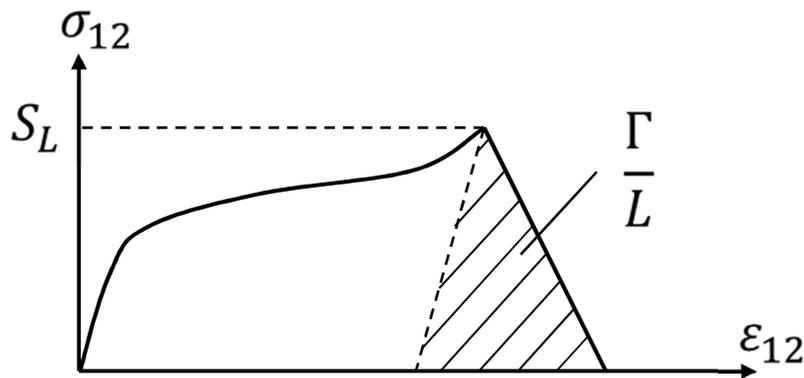


- *MAT_059: (*MAT_COMPOSITE_FAILURE_Option_MODEL)
 - Option: SHELL/SOLID

LS-DYNA: New models for composite structures

New!

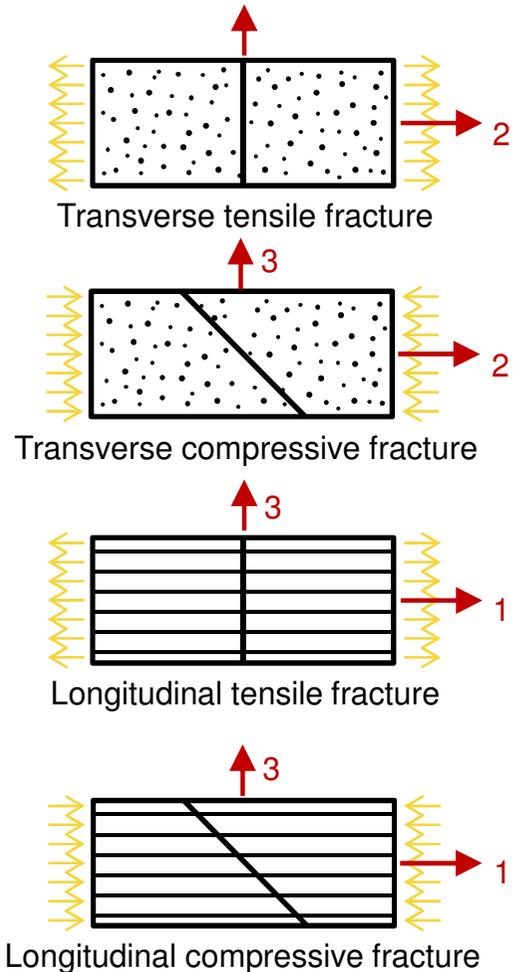
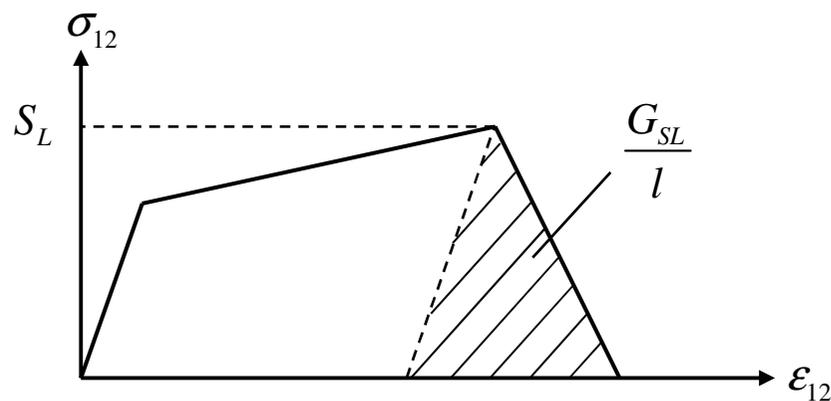
- *MAT_261: (*MAT_LAMINATED_FRACTURE_DAIMLER_PINHO)
 - Coupled failure criterion based on 3D-stress state
 - complex 3D-fibre kinking model
 - Matrix failure invokes search for controlling fracture plane
 - linear softening law based on fracture toughness
 - 1D-plasticity-model (mixed hardening) for in-plane shear behavior defined by load curve



LS-DYNA: New models for composite structures

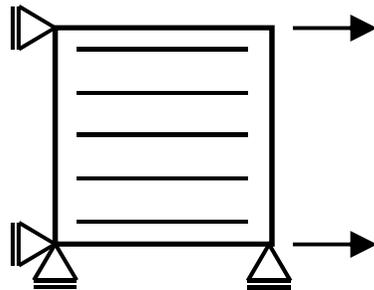
New!

- *MAT_262: (*MAT_LAMINATED_FRACTURE_DAIMLER_CAMANHO)
 - Coupled failure criterion based on 2D-stress state
 - Constant fiber misalignment angle based on shear and longitudinal compressive strength
 - Matrix failure with fixed planes
 - (Bi-)linear softening law based on fracture toughness
 - 1D-plasticity-model (linear mixed hardening) for in-plane shear behavior



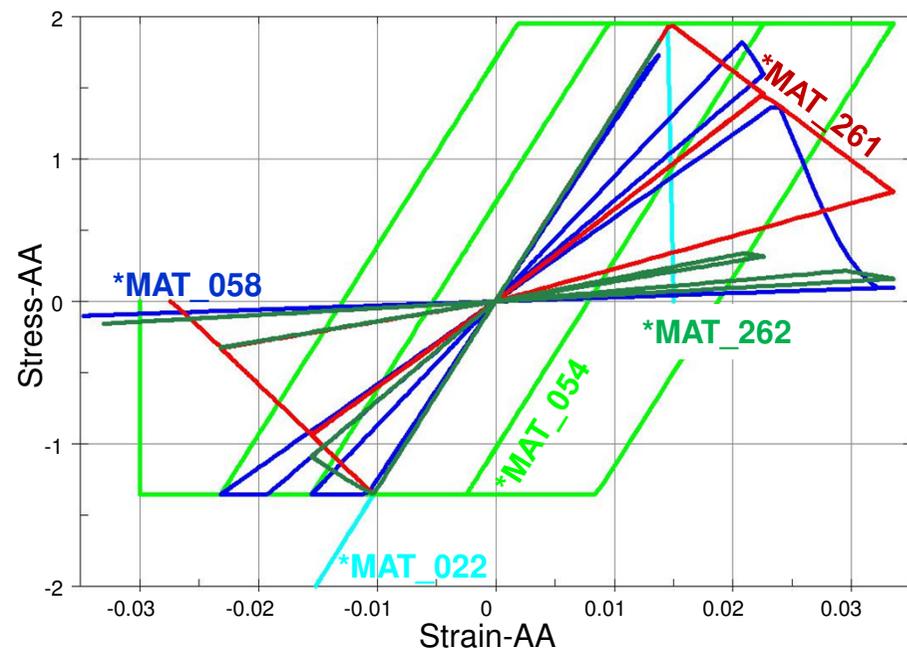
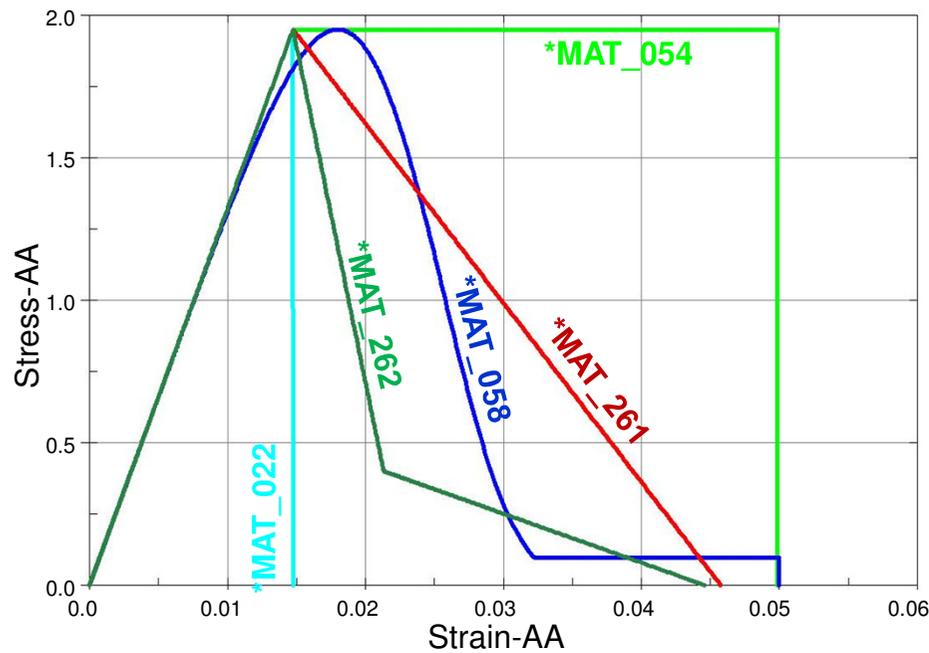
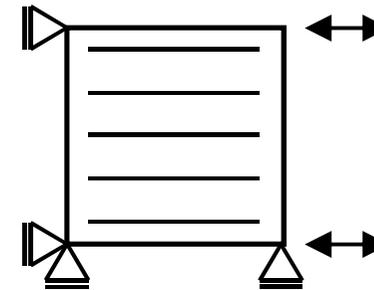
Comparison of different material models

fiber tensile load (A-E)



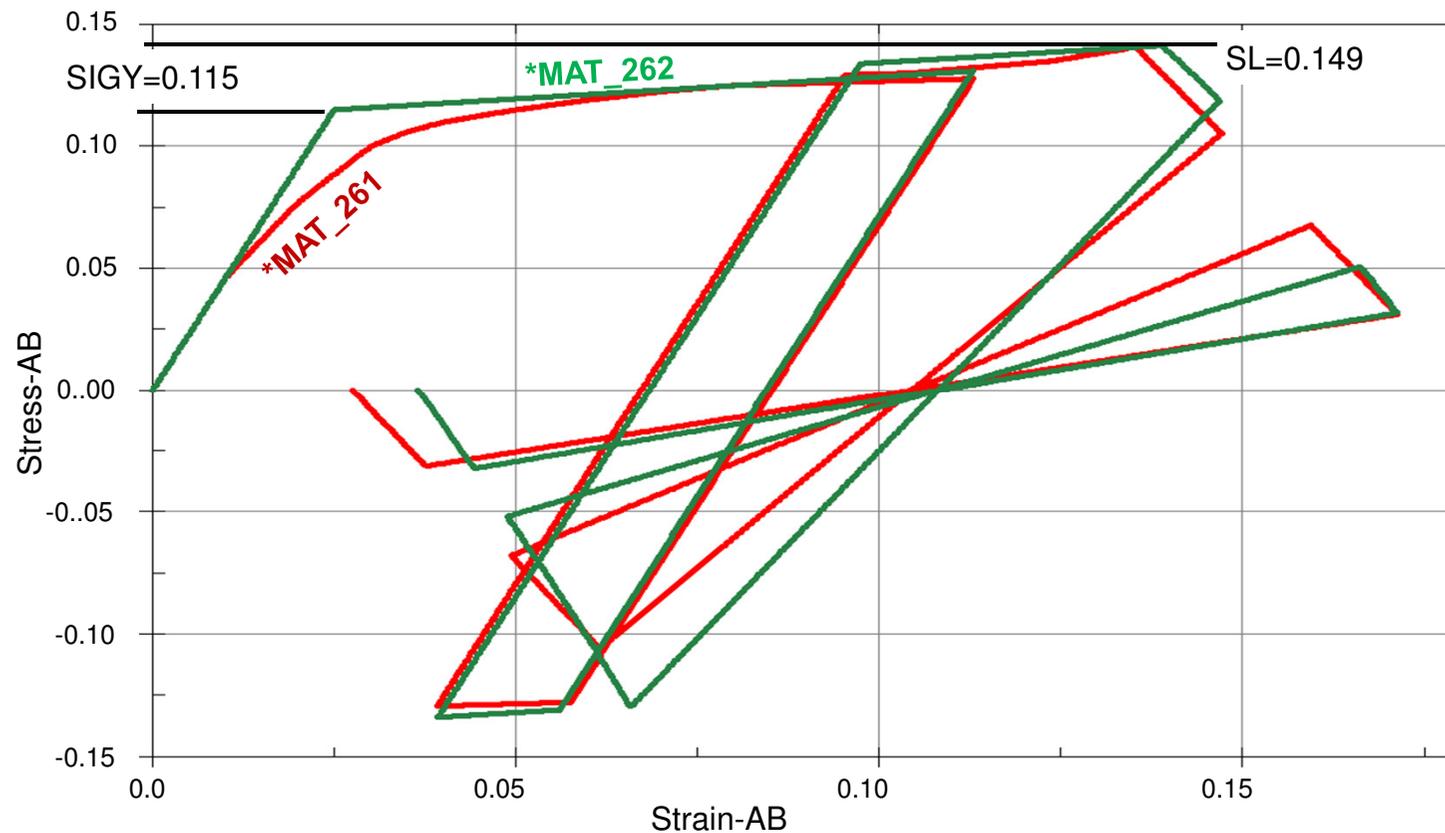
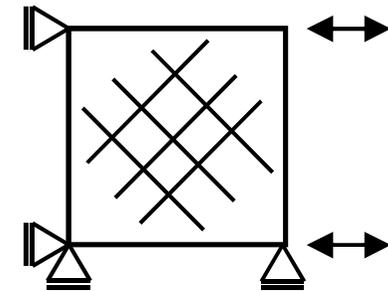
Material Parameter:
 $EA = 132.0 \text{ [kN/mm}^2\text{]}$
 $XT = 1.95 \text{ [kN/mm}^2\text{]}$
 $XC = 1.35 \text{ [kN/mm}^2\text{]}$
 ... (model dependent)

fiber fiber cyclic load (A-K)



Comparison of different material models

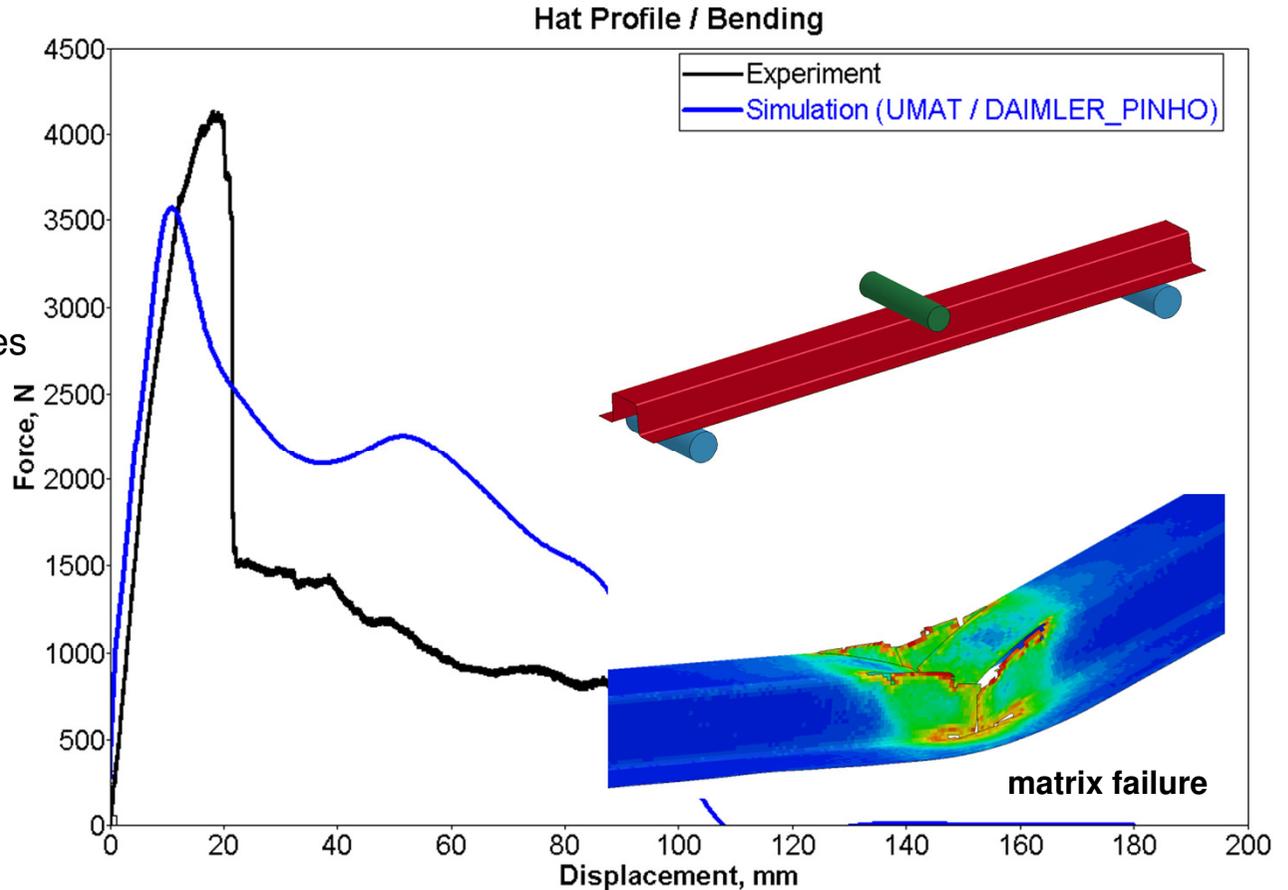
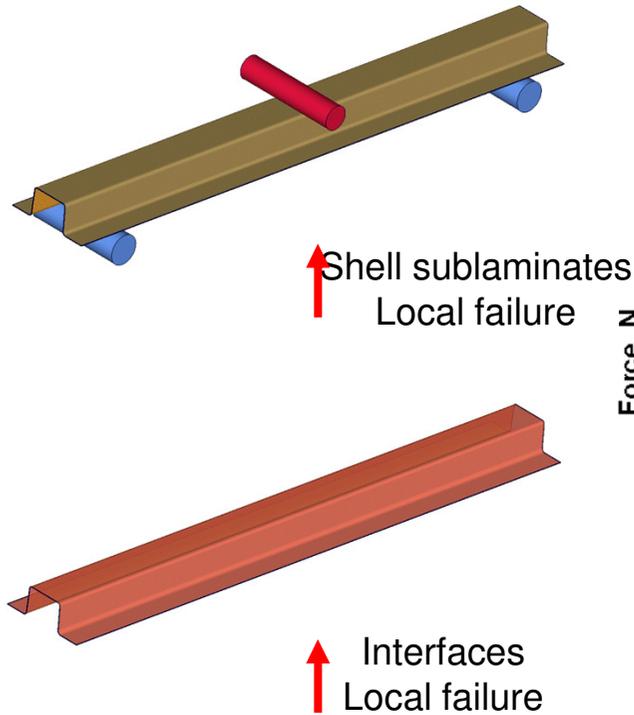
- 1-Element-Test, Single-Layer (,SHELL', ELFORM=2)
- Cyclic test with a +/-45° layup (A-M)



Preliminary results

three point bending of a hat profile

- single shell with a thickness of 2mm / carbon fibers in epoxy resin
- [90°/0°/45°/-45°/0°/90°/-45°/45°/0°/90°]



DAIMLER



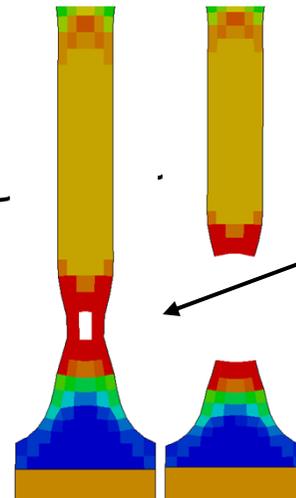
Preliminary results

shear specimen

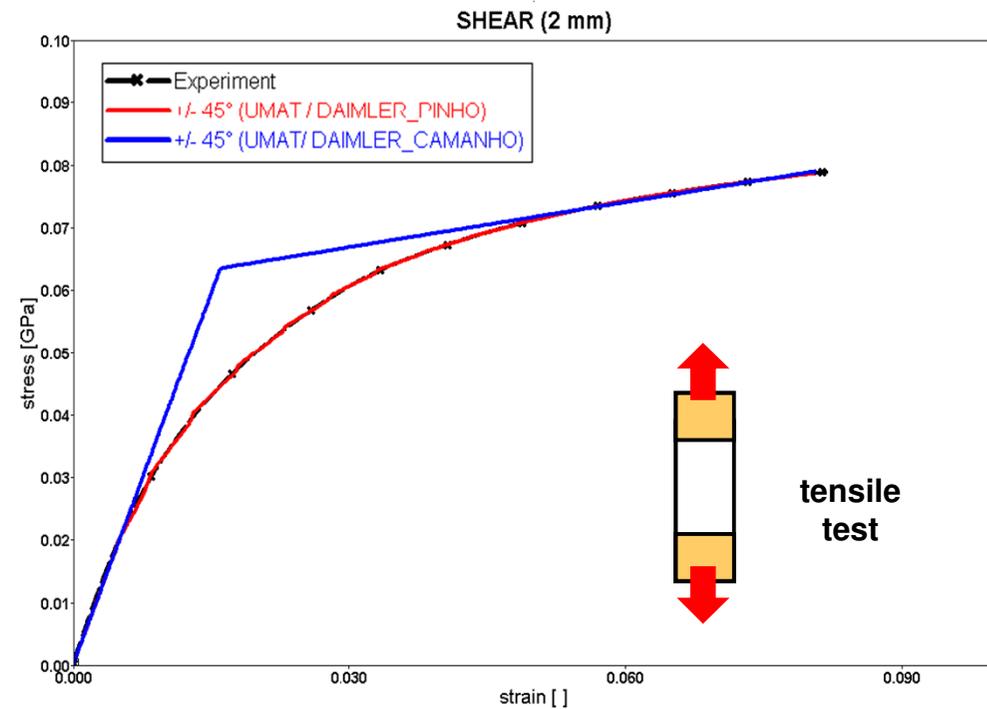
- single shell with a thickness of 2mm / carbon fibers in epoxy resin
- $[45^\circ/-45^\circ]_{3S}$



Experiment



Simulation

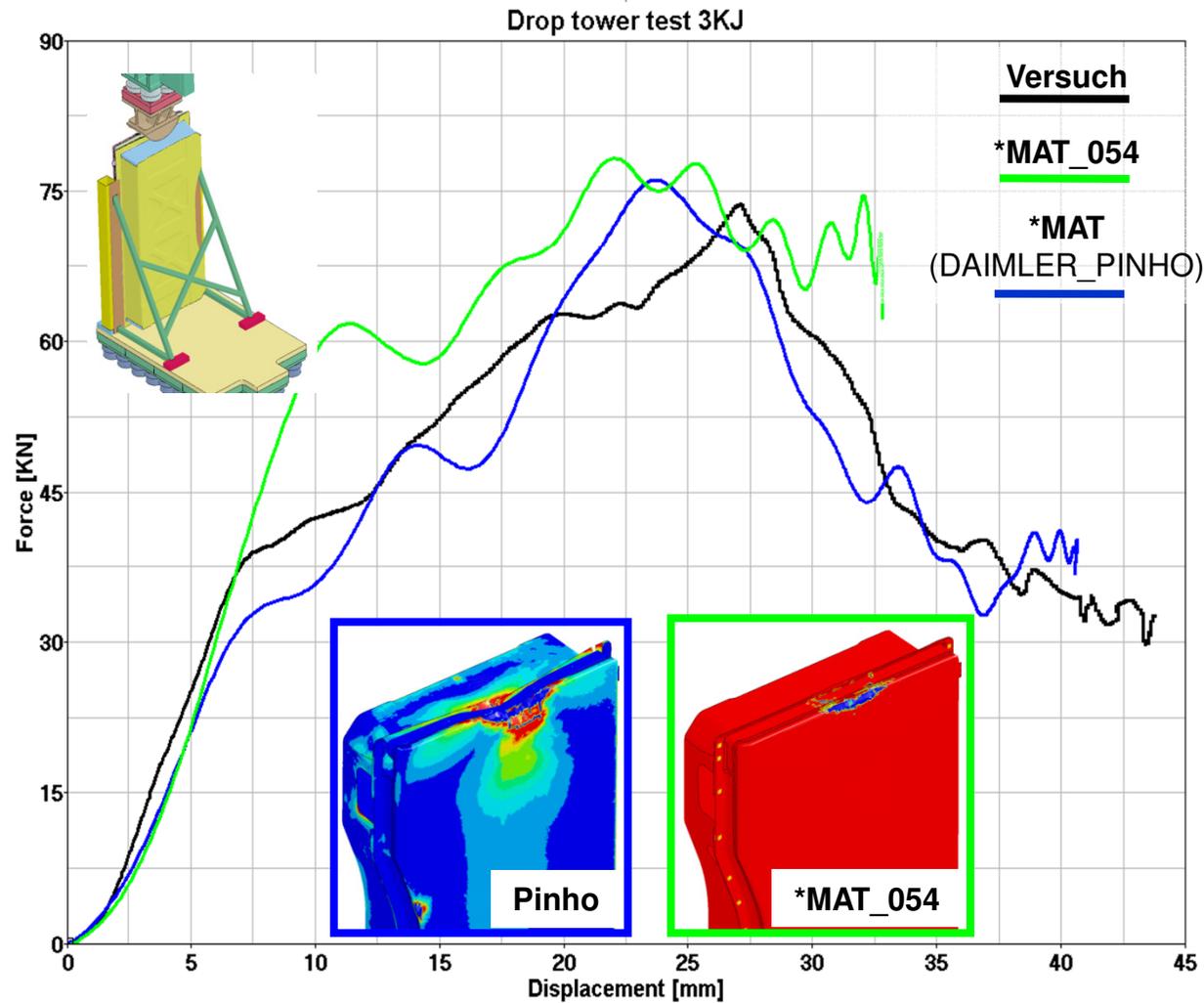


DAIMLER

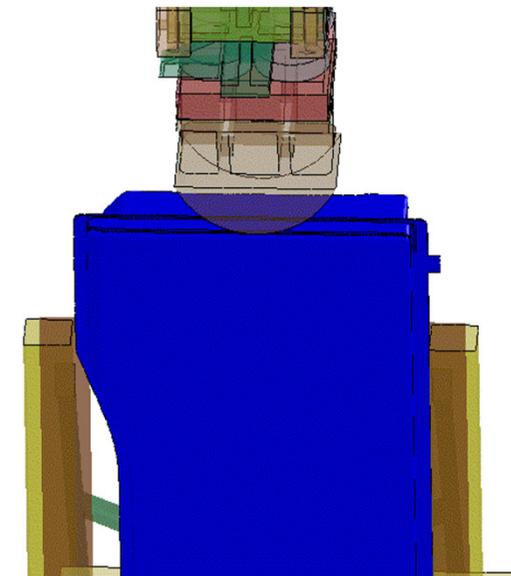
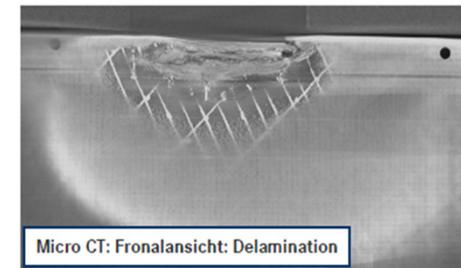


Preliminary results

CFRP Box, Carbon-Epoxy



CT: Evaluation of damage





Agenda

- Process simulation
 - Winding and Braiding
 - Draping
 - Thermoforming

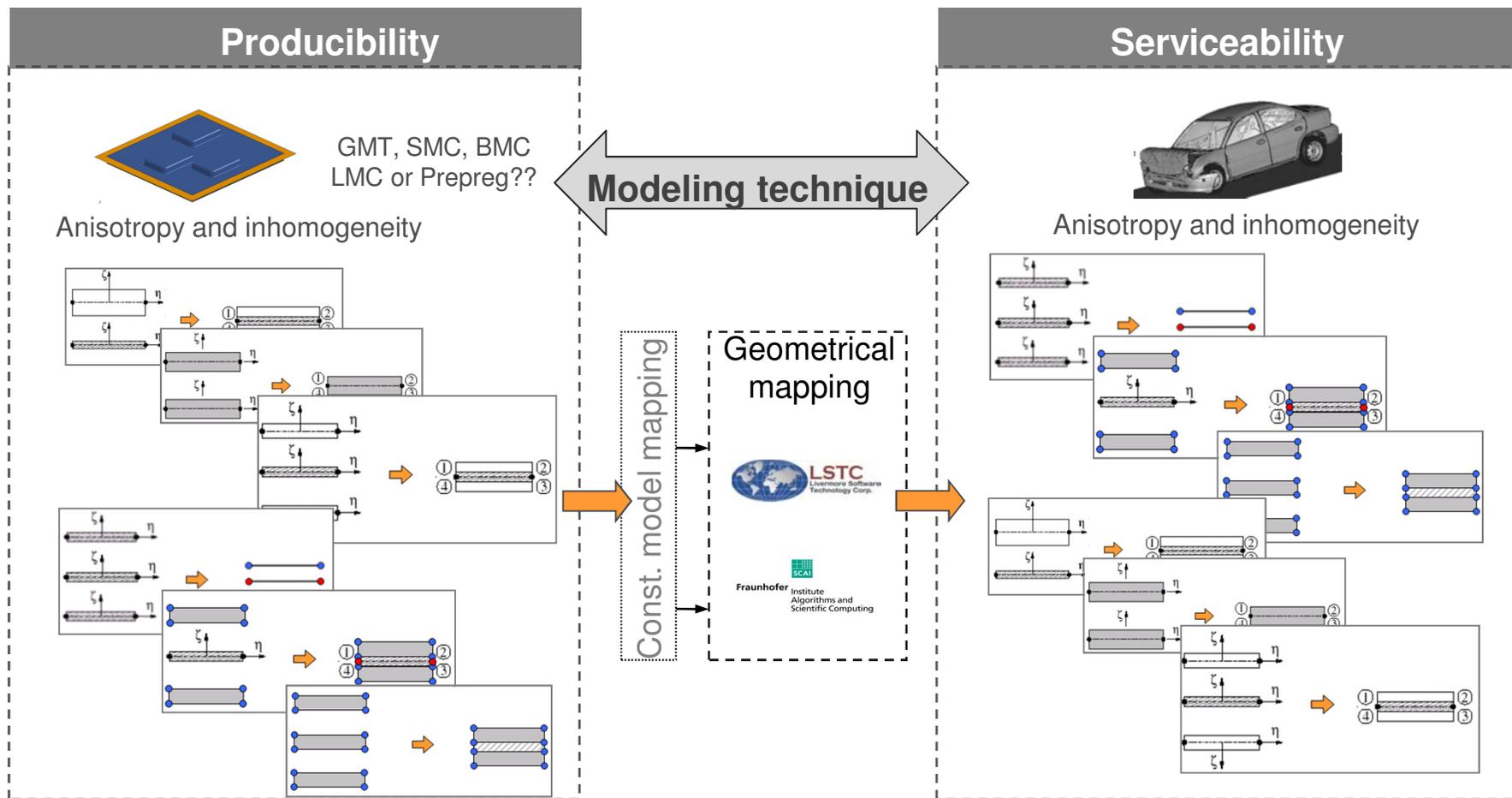
- Crashworthiness analysis
 - Short and long fiber reinforced plastics
 - Continuous fiber reinforced plastics

- Mapping

- Summary

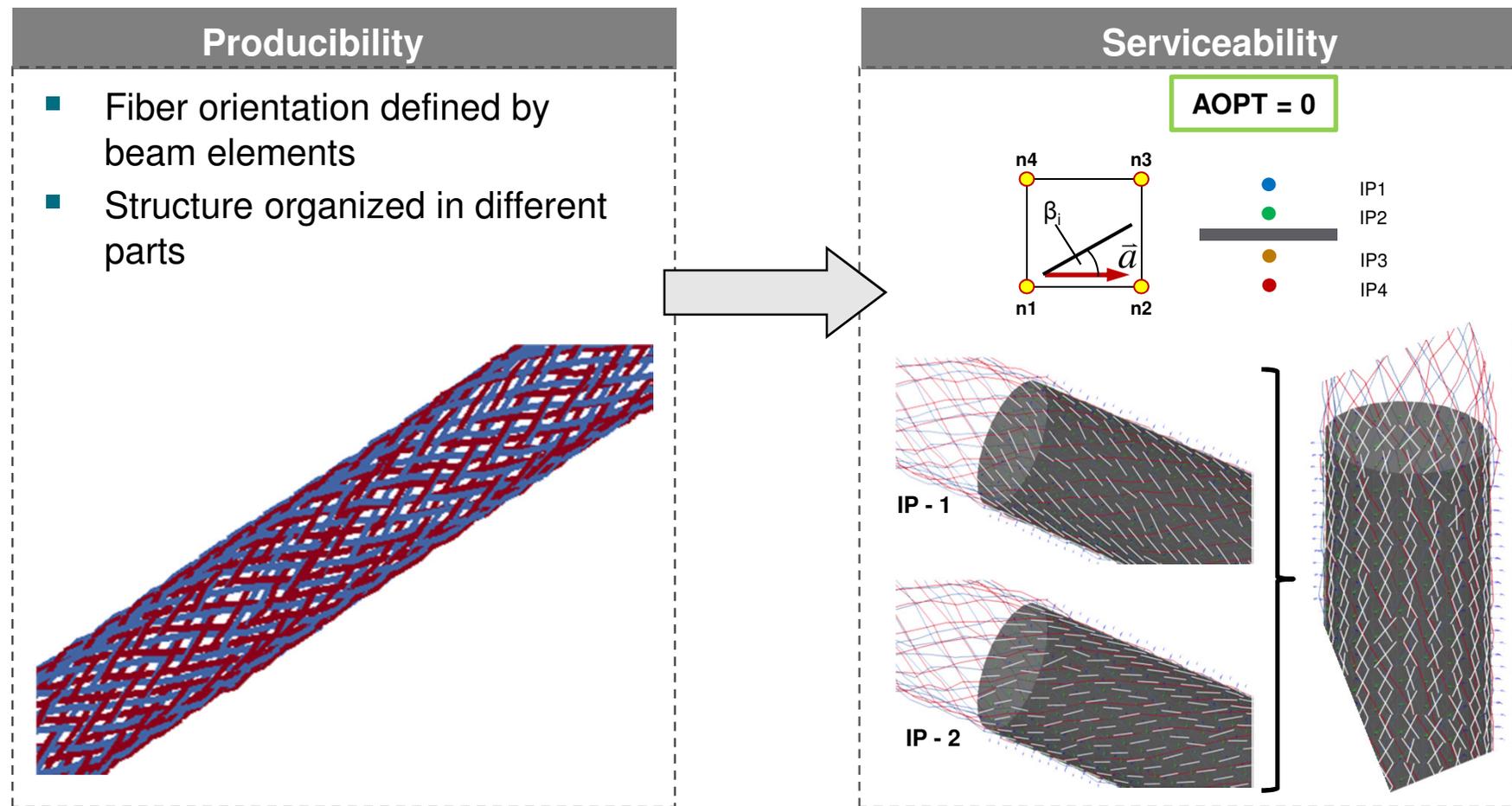
Mapping between producibility and serviceability

- Different applications use different modeling techniques, constitutive models, standards and validation procedures.



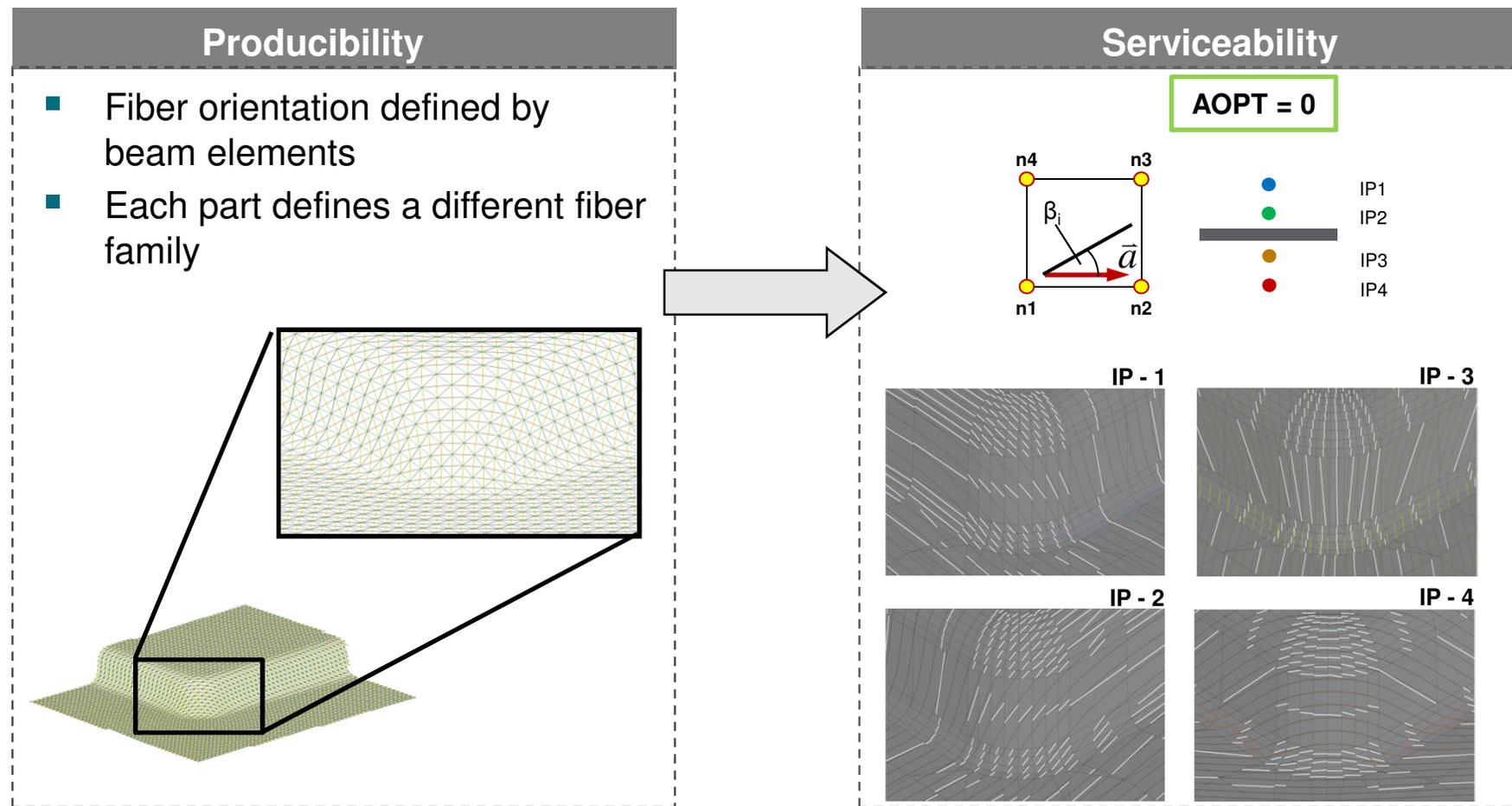
Mapping between producibility and serviceability

- Source: Braiding Simulation
- Target: Crash structure discretized with shell elements



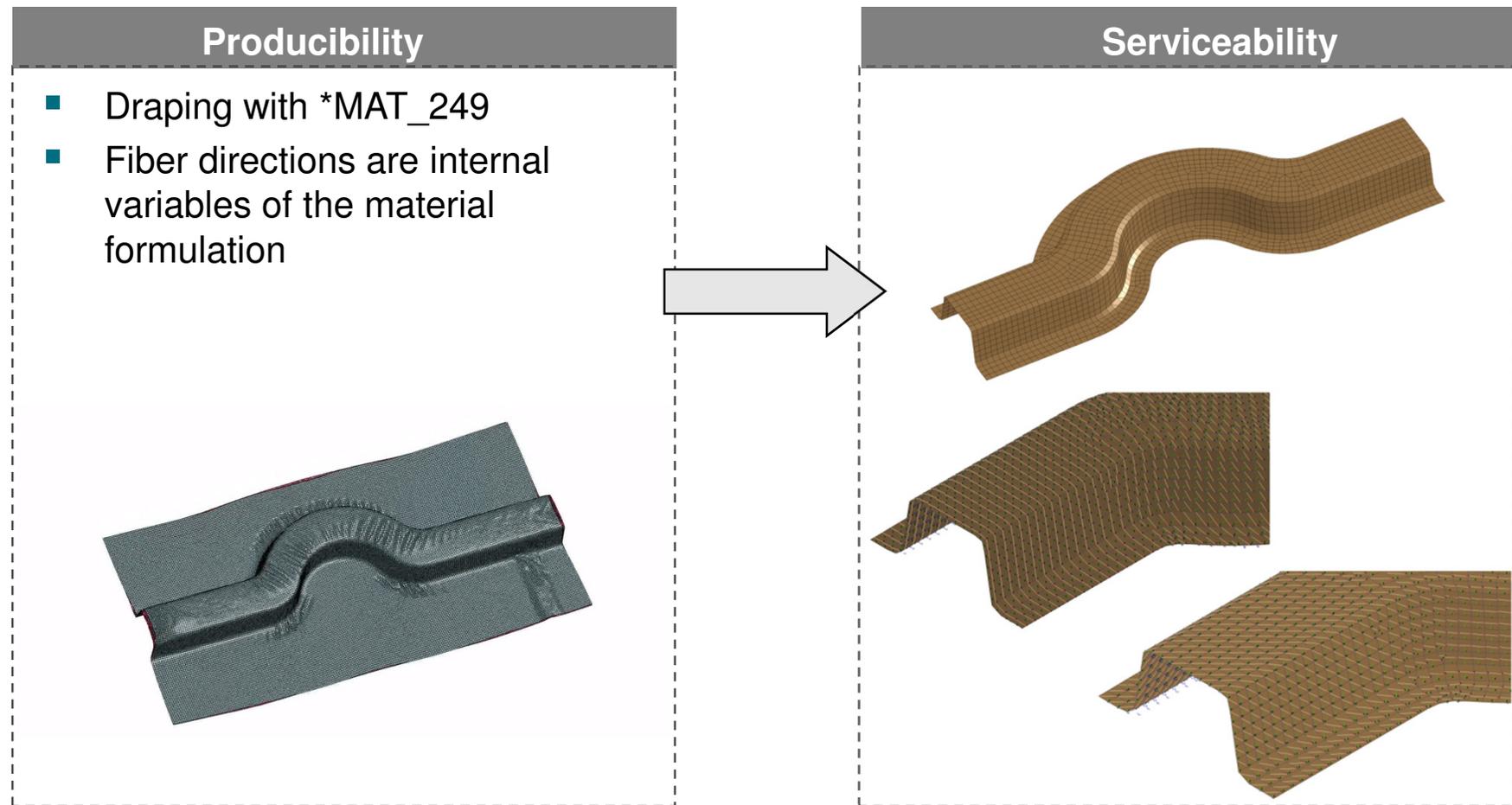
Mapping between producibility and serviceability

- Source: Draping Simulation with beam elements
- Target: Crash structure discretized with shell elements



Mapping between producibility and serviceability

- Source: Draping Simulation with beam elements
- Target: Crash structure discretized with shell elements





Agenda

- Process simulation
 - Winding and Braiding
 - Draping
 - Thermoforming

- Crashworthiness analysis
 - Short and long fiber reinforced plastics
 - Continuous fiber reinforced plastics

- Mapping

- Summary



Summary

- Process simulation with LS-DYNA
 - Tailored modeling techniques for different length scales
 - Examples for winding, braiding and draping processes
 - New thermo-mechanical material model for thermoplastic prepregs
- Serviceability
 - New features for short and long fiber reinforced plastics (work in progress)
 - A variety of different material models for simulation of continuous fiber reinforced plastics
- Mapping
 - Between different length scales
 - Between different modeling approaches



Thank you very much for your attention!

stefan.hartmann@dynamore.de

thomas.kloeppel@dynamore.de

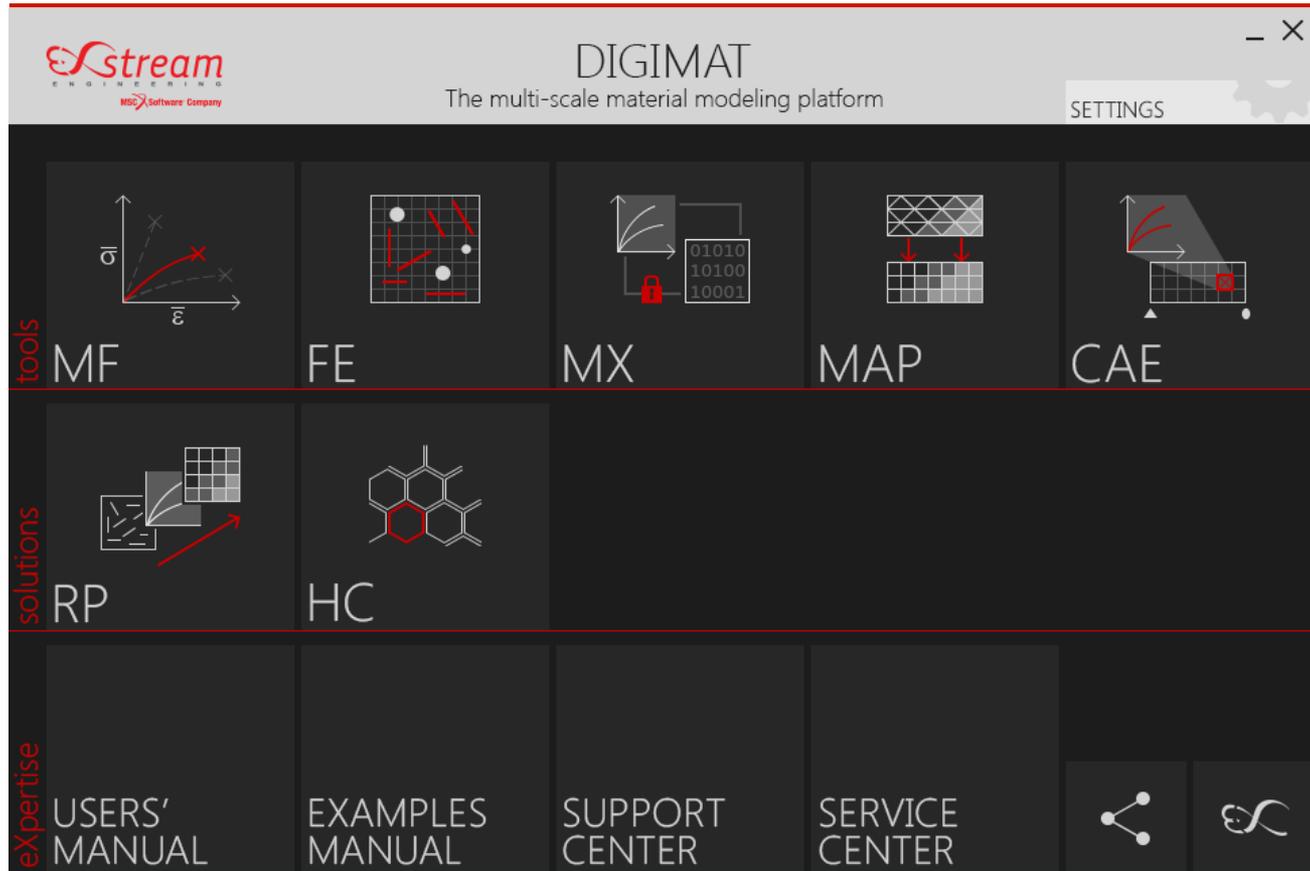
christian.liebold@dynamore.de

Acknowledgement

The research leading to these results has received funding from the Federal Ministry of Education and Research in the project “T-Pult” and from the Federal Ministry for Economic Affairs and Energy (Central Innovation Program SME) in the project “Swim-RTM”.

Process Chain Modeling

Composite Materials



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Product Manager Digimat

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Mobile: +49 (0)176 / 70 55 47 59



e-Xstream engineering

Company

- Who are we...? A **MSC Software Company!**

- ✓ **Team of 30+ persons**

- PhDs (65%)
- MS & BS Engineering (25%)
- Marketing, Finance & Admin (10%)



- ✓ **Material experts**

- Micromechanics

- ✓ **It's all about...**

COMPOSITES



Amsterdam, October
2012

- **Worldwide Partner Network**

- ✓ **Material Experts**

- Material Suppliers

- ✓ **Service Providers**

- Industrial
- R&D

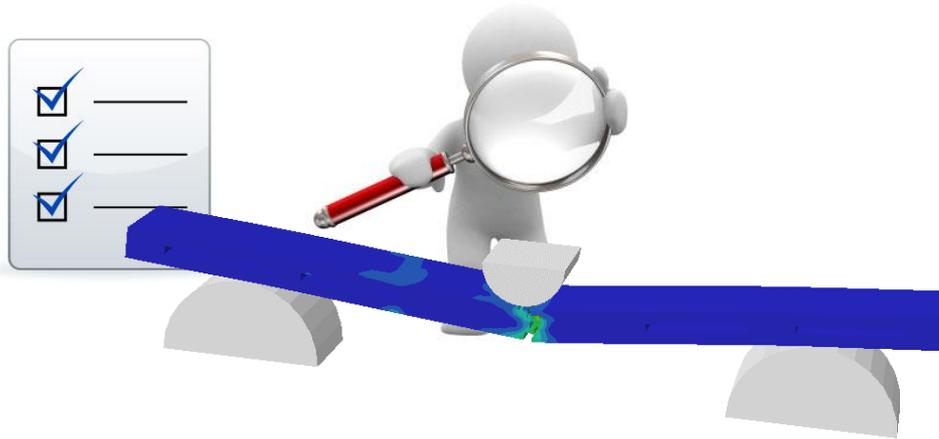
- **Software**

- Providers
- Resellers



Process Chain Modeling

Composite Materials



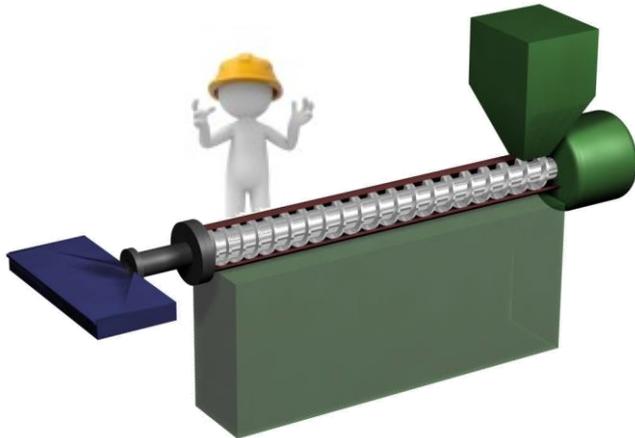
DESIGN

Final performance



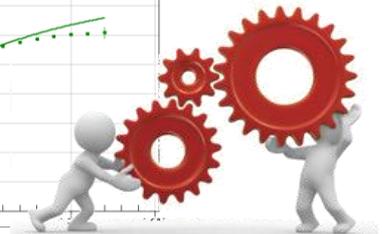
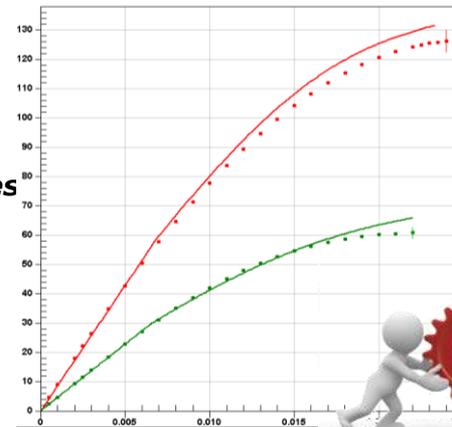
MANUFACTURING

Local microstructure



MATERIAL

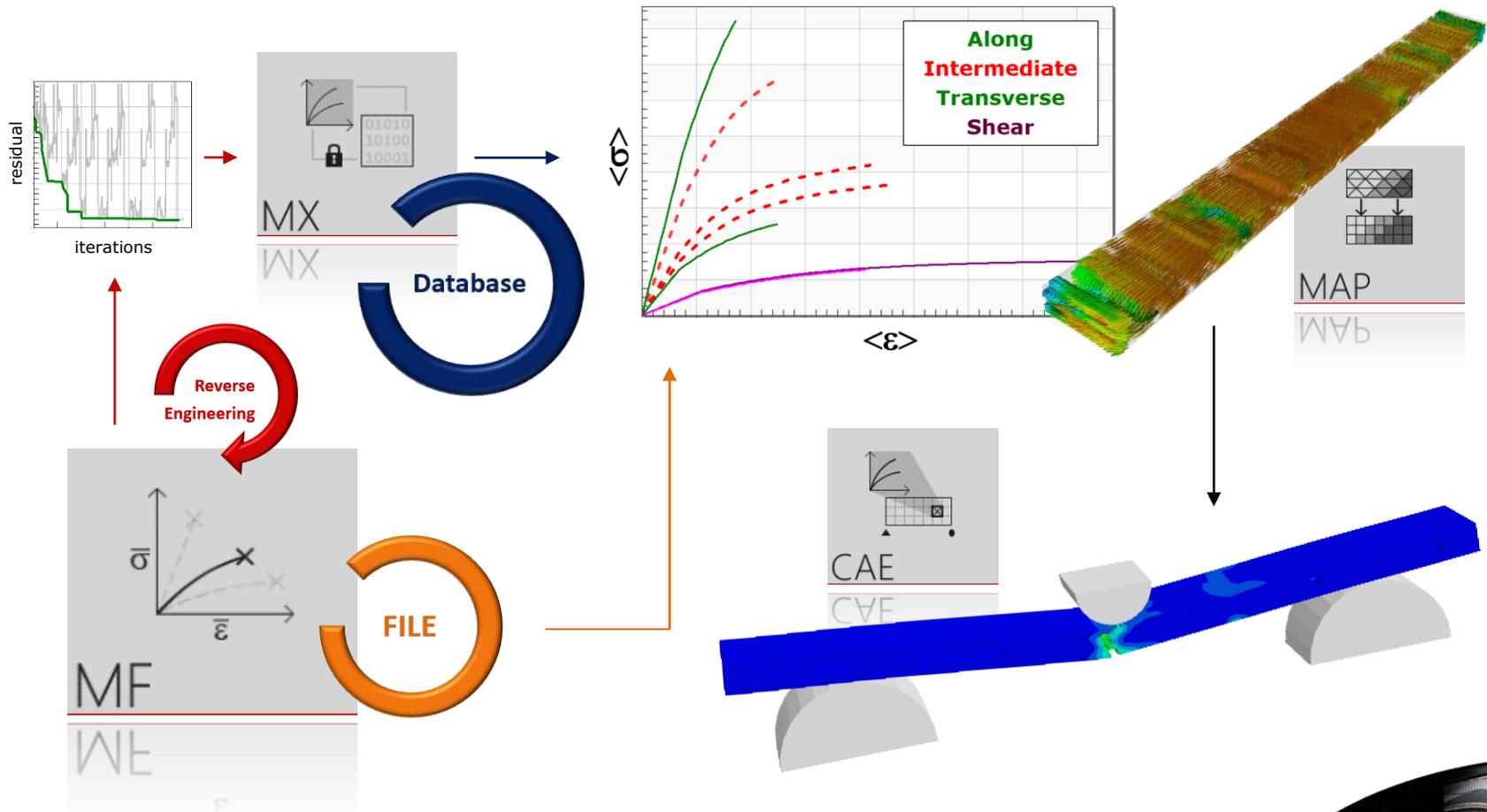
Distributed properties



Process Chain Modeling

Composite Materials

- **Workflow** – From Material to Structural Engineering

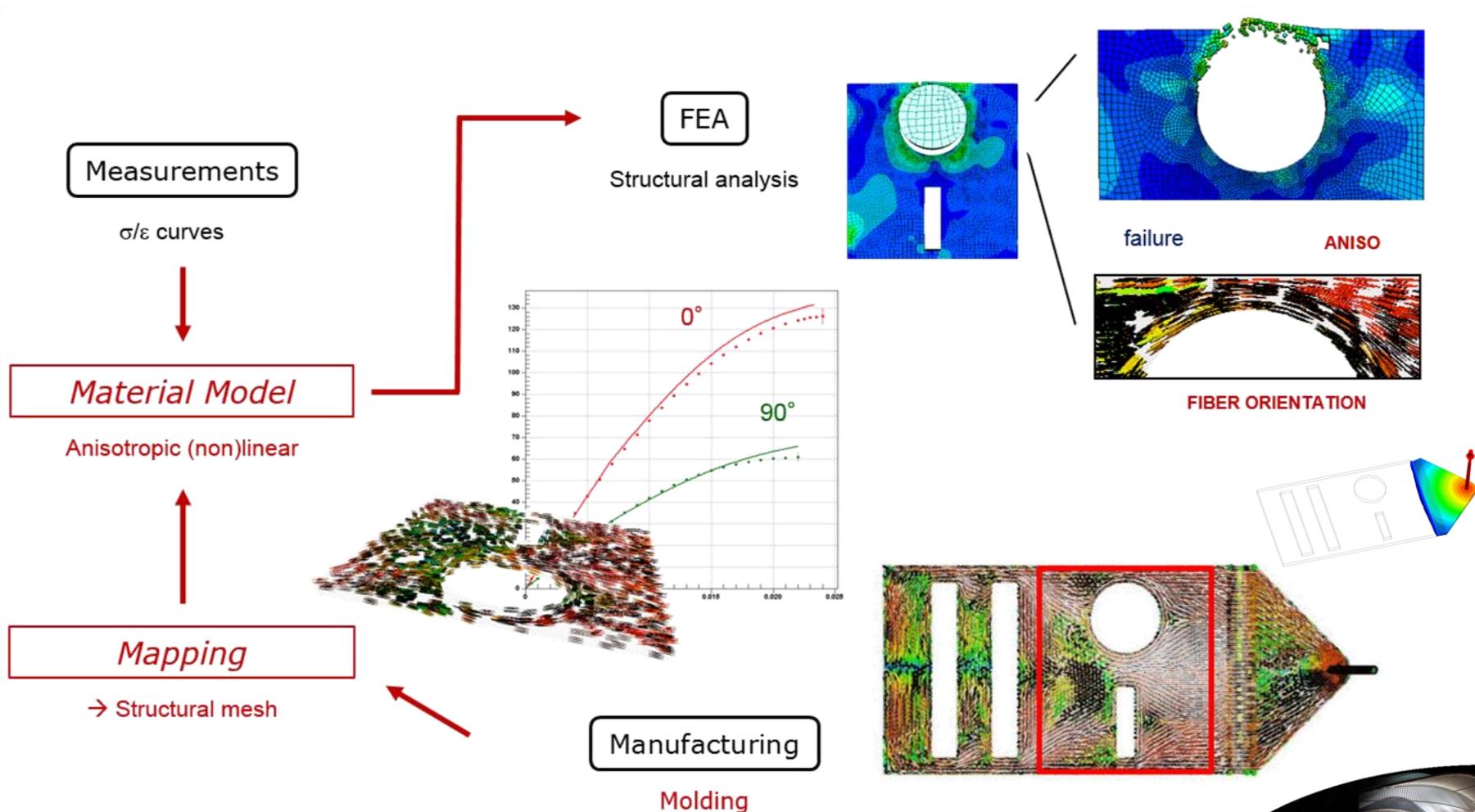


Process Chain Modeling

Composite Materials

- Short Fiber Reinforced Plastics

→ Molding Impact on Stiffness & Failure

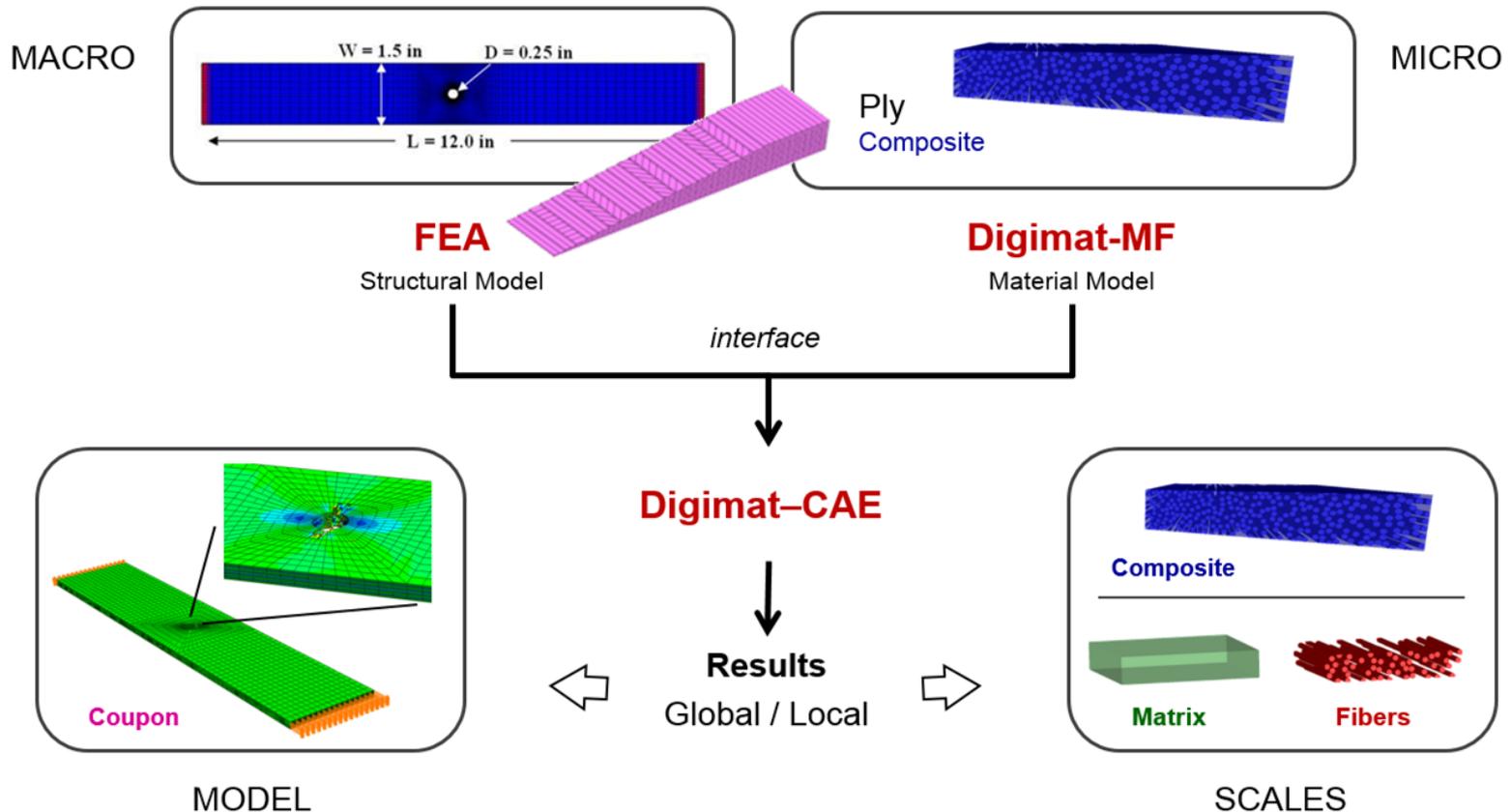


Process Chain Modeling

Composite Materials

- UD Composites

→ Micro / Macro Bridging the Scales

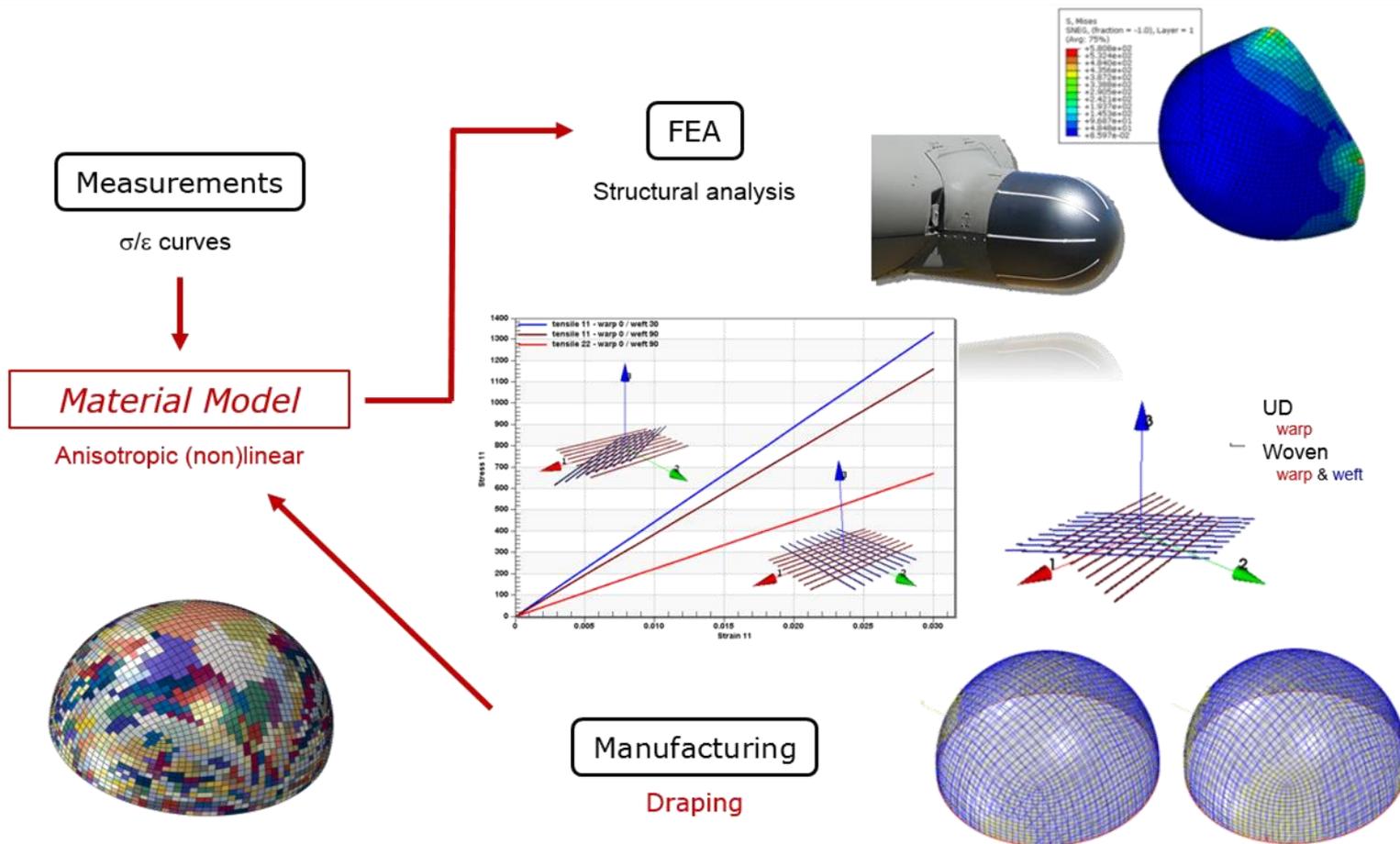


Process Chain Modeling

Composite Materials

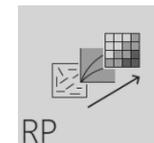
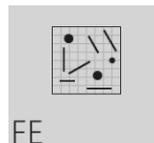
- Woven Composites

→ Draping Impact on Stiffness & Failure

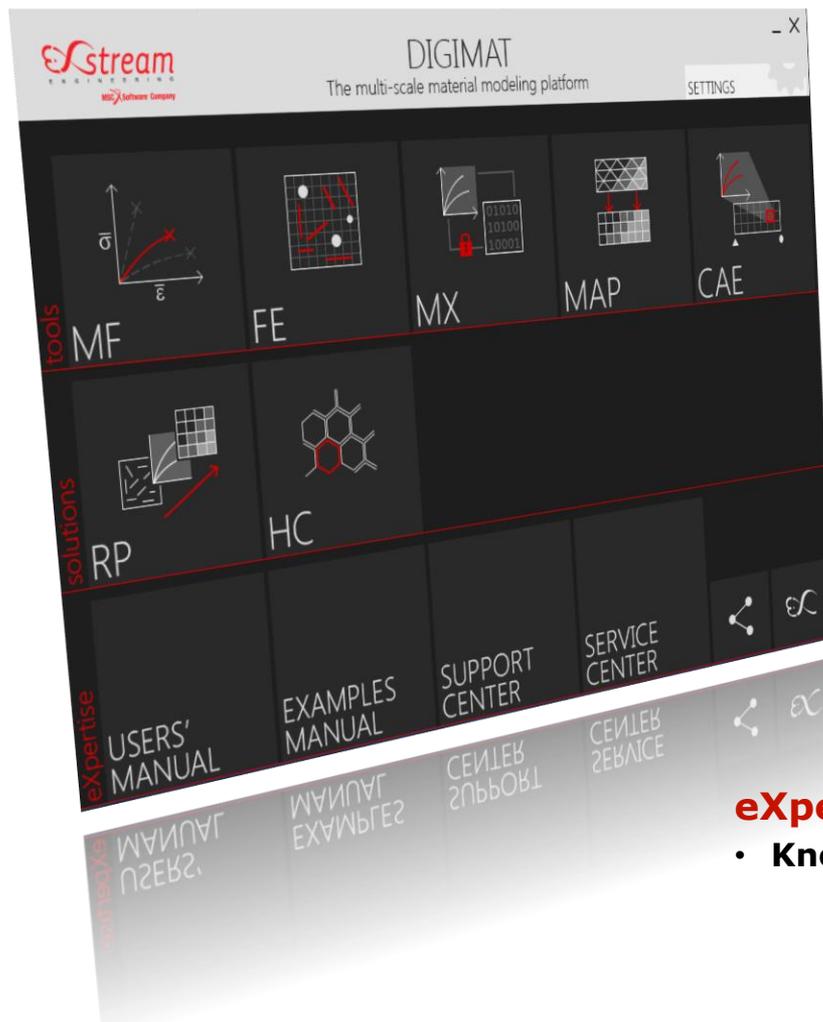


Digmat

Software



Nonlinear Multi-Scale Modeling Platform



Tools

- For experts
- Modular environment

Solutions

- For designers
- Integrated environments
- Workflow oriented

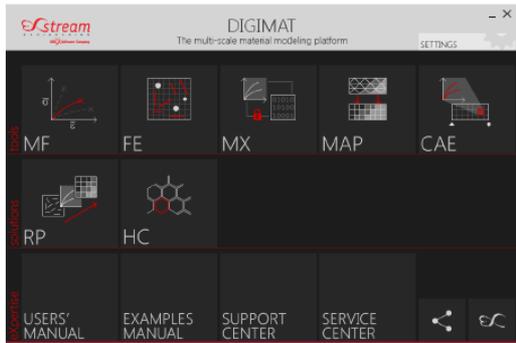
eXpertise

- Knowledge transfer

Release Notes & Highlights



Release Notes 5.0.1 – November 2013



						
p. 4	-	p. 5	-	p. 5-6	p. 2-3	-

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DIGIMAT 5.0.1 RELEASE HIGHLIGHTS

What's new in Digimat 5.0.1?

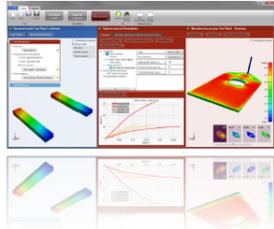


Digimat-RP

GUI guided workflow tool for coupled analyses

With "Reinforced_Elastics" e-Xstream poured 10 years of experience into a GUI guided tool that aids the setup of coupled analysis in an easy and understandable way, uniform to all communities.

This release will support the setup of 3D analyses with Marc, MSC Nastran, Abaqus, Ansys and LS-Dyna based on Moldflow, Moldex3D, Sigmasoft or Timon 3D processing results. All Digimat solution technologies are supported. Jobs can either be run and monitored on a local computer or packaged for the remote solution on a cluster.

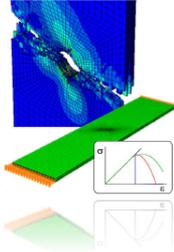


Progressive Failure

UD Composites

Digimat 5.0.1 offers a Matzenmiller-Lubliner-Taylor (MLT) based model for the progressive failure of UD composite materials. Failure progression includes individual damage evolution functions as well as stabilization of failure progression for coupled analyses.

SOL700 is now available in the Digimat-CAE/Nastran interface supporting MSC Nastran 2013.1.



Woven Composites

Improved Robustness

The Hybrid solution method has been enhanced to support elastic, elastoplastic and elasto-viscoplastic material models for woven composites including per-phase failure.

Thermal Dependency

Thermal & Thermo-Mechanical Analyses

Anisotropic thermal conductivity can be used in coupled analyses with Digimat-CAE/Abaqus. Thermo-mechanical analyses are available via Digimat-CAE/Marc. Robustness has been improved by offering Reverse Engineering of thermo-elastoplastic material models in MX and the support of thermo-elastic and thermo-elastoplastic within the Hybrid solution method.

For more information please contact info@e-Xstream.com
www.e-Xstream.com



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∞ **MSC Nastran SOL400**

✓ 2013.1

∞ **Abaqus**

✓ 6.12



∞ **MSC Nastran SOL700**

✓ 2013.1

∞ **Ansys**

✓ 14.5 → Initial stresses...



∞ **Marc**

✓ 2012 → Thermo-mechanical

∞ **LS-Dyna**

✓ 6.1



∞ **Radioss**

✓ v11

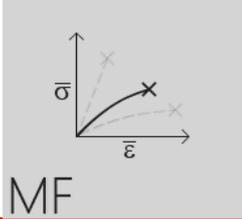


HIGHLIGHTS 5.0.1

**Progressive Failure
Hybrid for Woven**

Progressive Failure

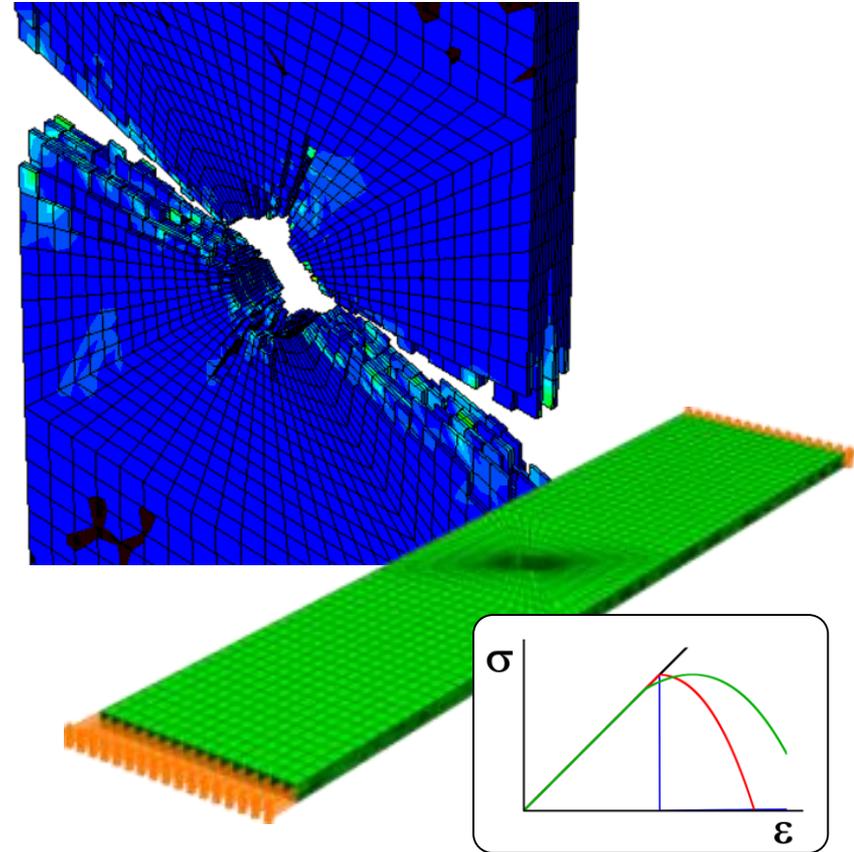
Highlights 5.0.1



UD Composites

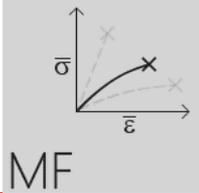
✓ Macroscopic model

- **Stiffness**
 - Linear elasticity
- **Failure**
 - Hashin 2D
 - Hashin 3D
 - Hashin-Rotem 2D
- **Damage**
 - Matzenmiller / Lubliner / Taylor
 - Individual damage control functions
 - Stabilization of failure progression



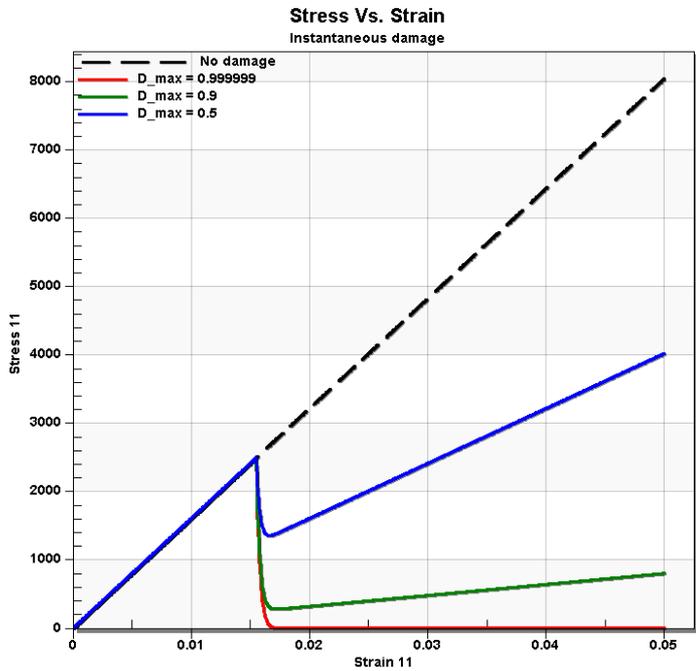
Progressive Failure

Highlights 5.0.1

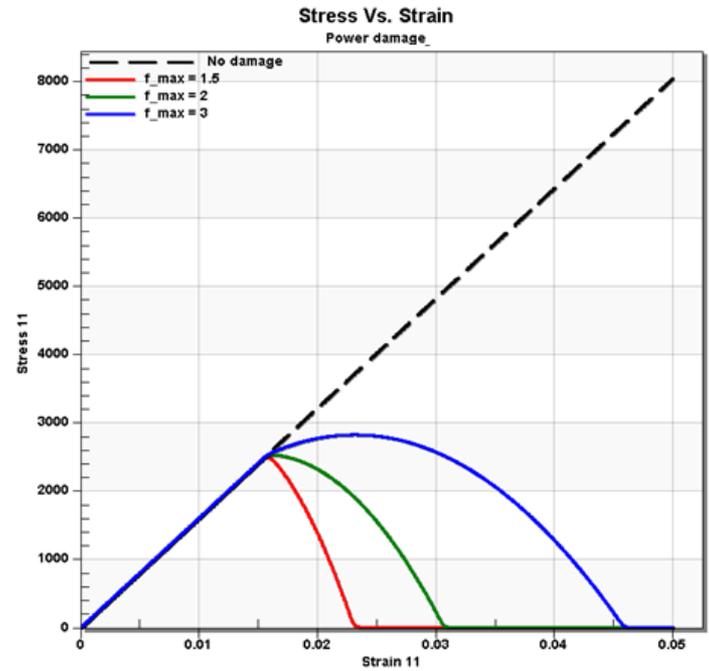


UD Composites

✓ Stiffness / Damage / Failure



Instantaneous failure
Remaining stiffness

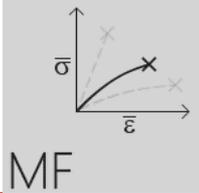


Damage
Complete failure



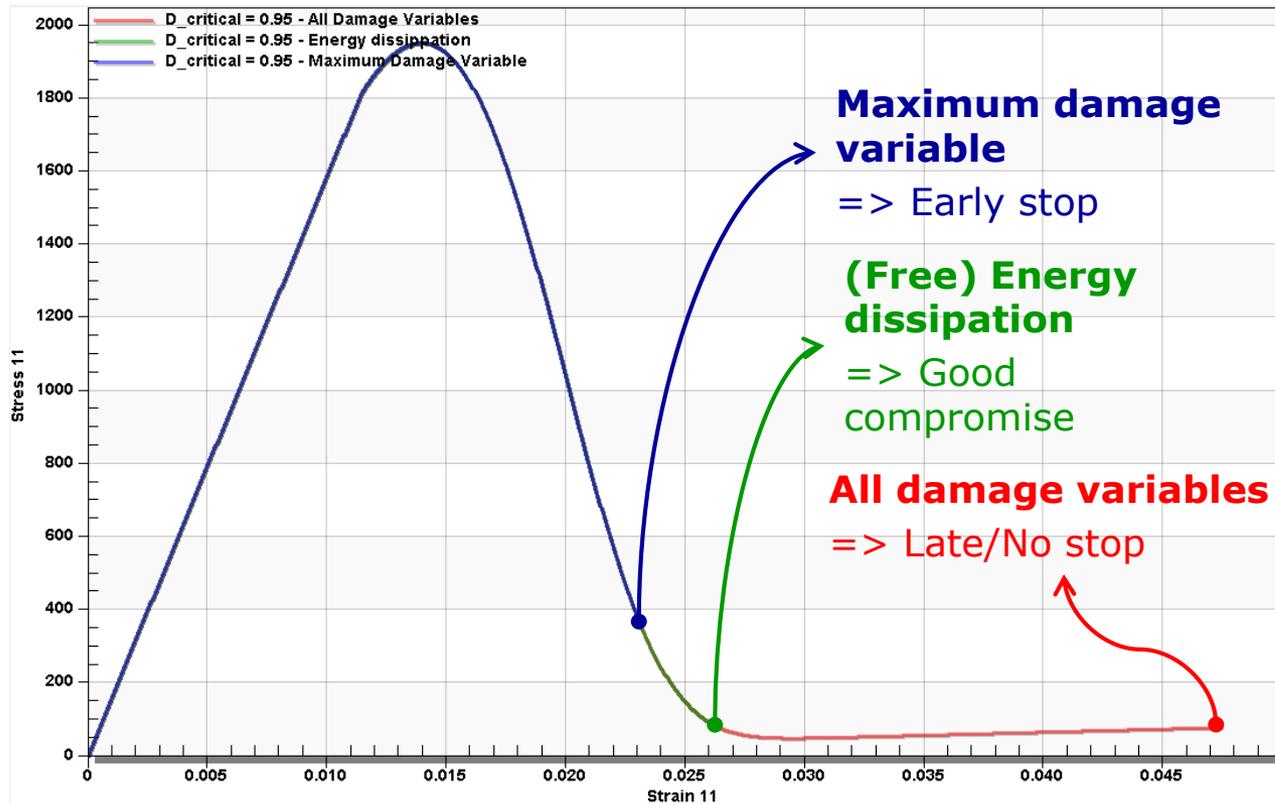
Progressive Failure

Highlights 5.0.1



UD Composites

✓ Analysis control by damage evaluation



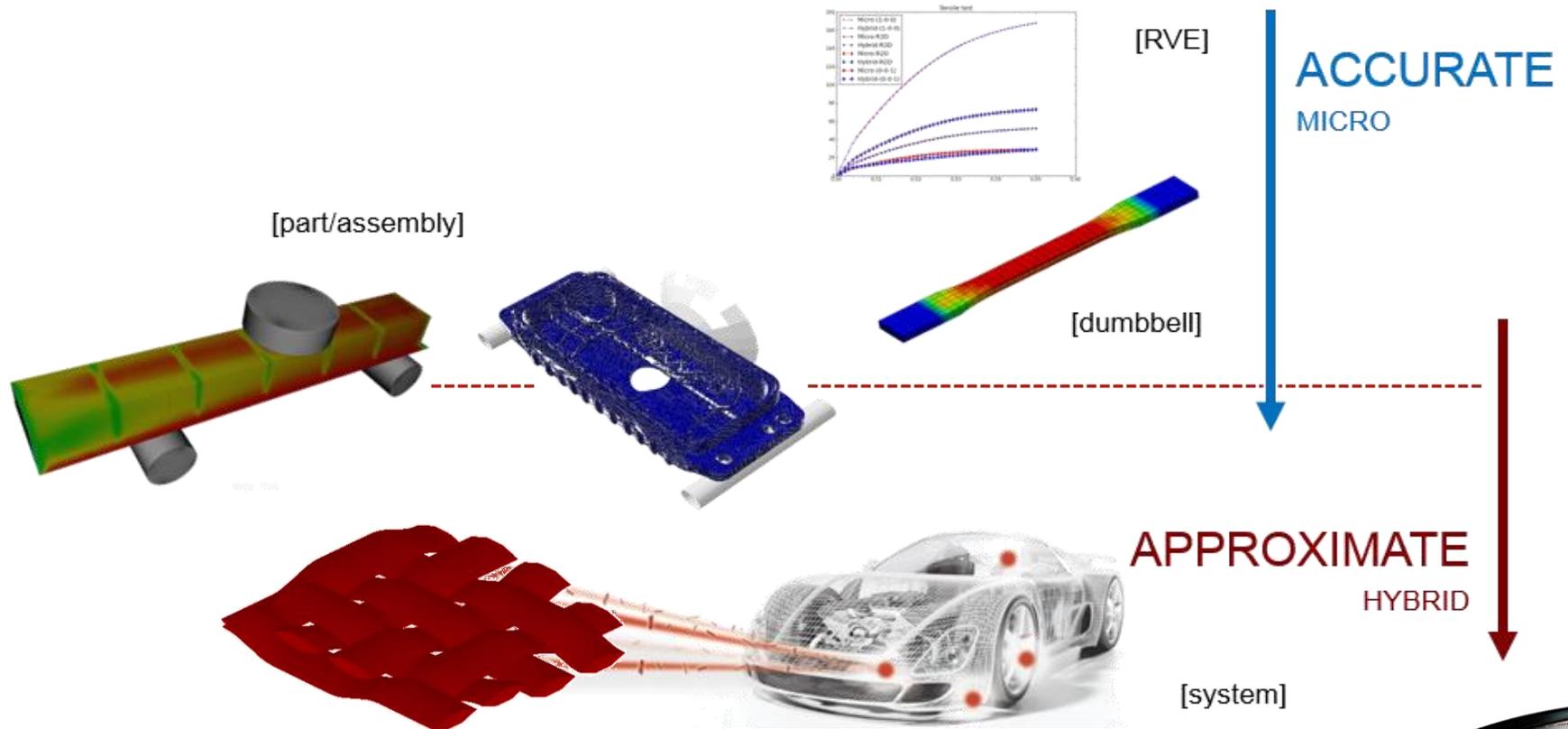
Hybrid for Woven

Highlights 5.0.1



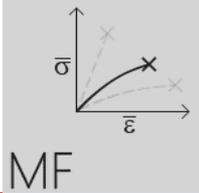
Hybrid solution

✓ Towards system level...



Hybrid for Woven

Highlights 5.0.1

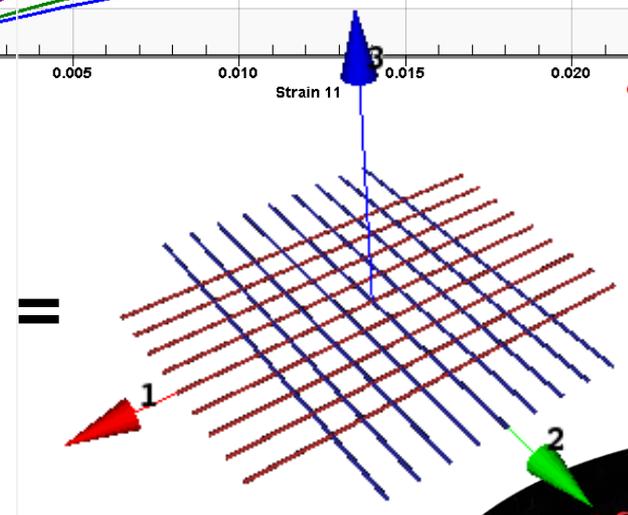
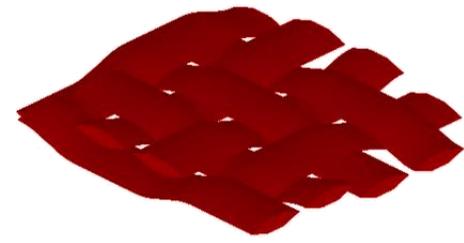
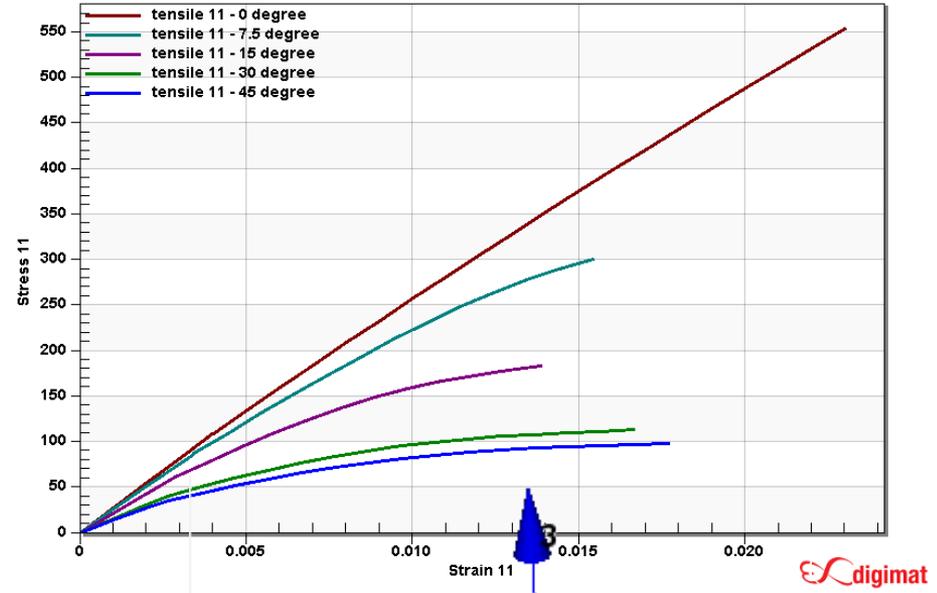


Woven Composites

✓ Material model

- Basic & homogeneous yarns
- Stiffness
 - Elastic
 - Elastoplastic
 - Elasto-Viscoplastic

- Failure
 - Per-phase



digimat



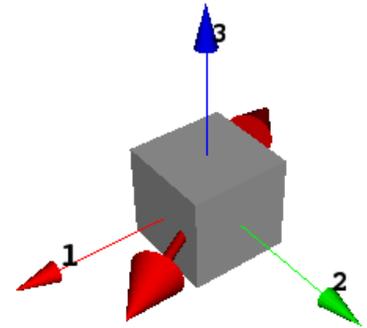
Hybrid for Woven

Highlights 5.0.1

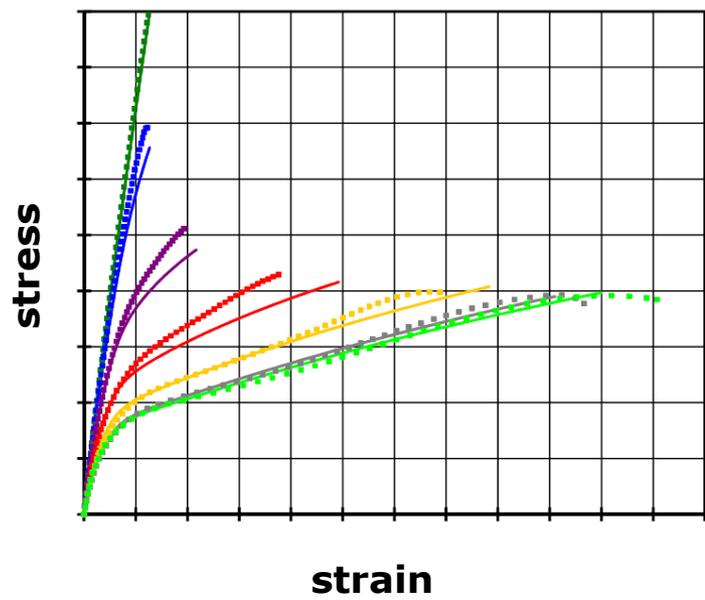


Woven Composites

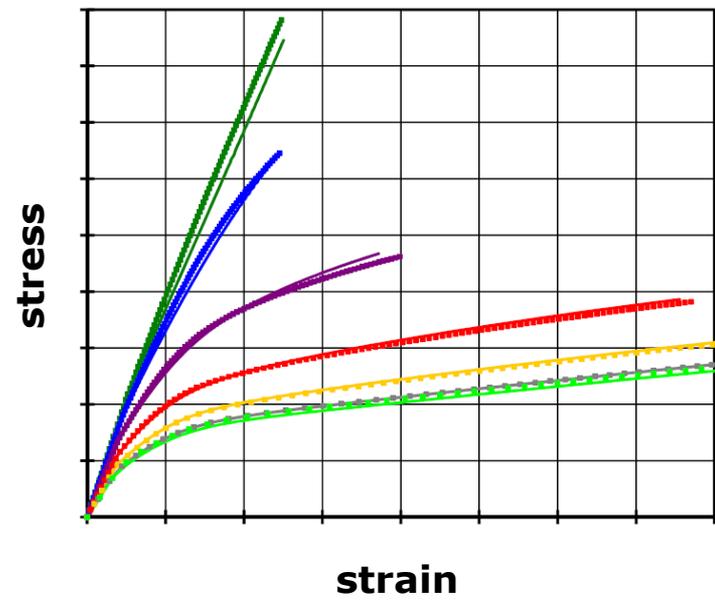
- ✓ Elastoplastic / failure
 - Excellent correlation with experiments



MICRO vs. EXP



MICRO vs. HYBRID



- 0°
- 7.5°
- 15°
- 22.5°
- 30°
- 37.5°
- 45°



DIGIMAT CLASSICS

Short Fiber Reinforced Plastics in Digimat 5.1

Stiffness

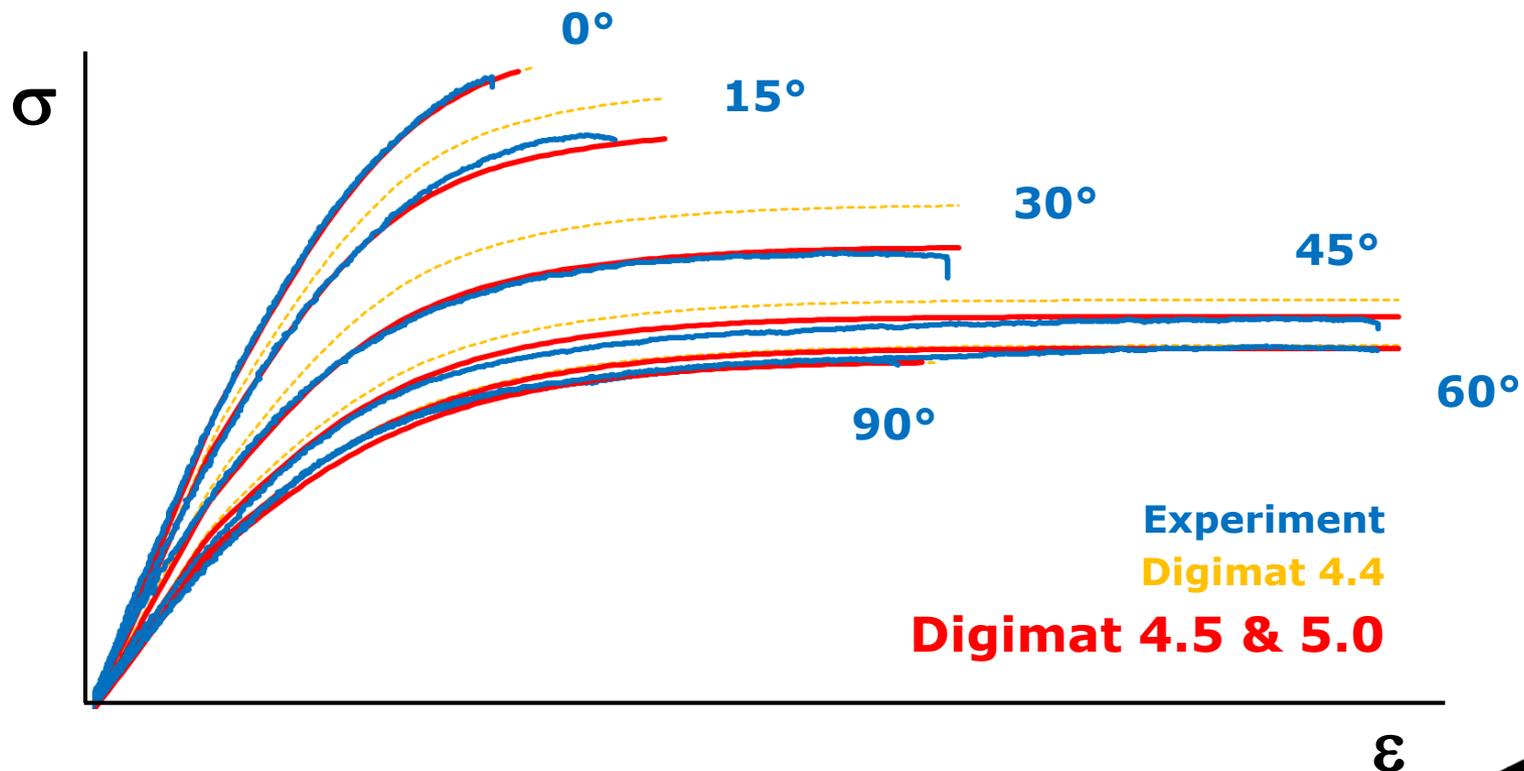
Robust/Fast/Easy



4.5.1

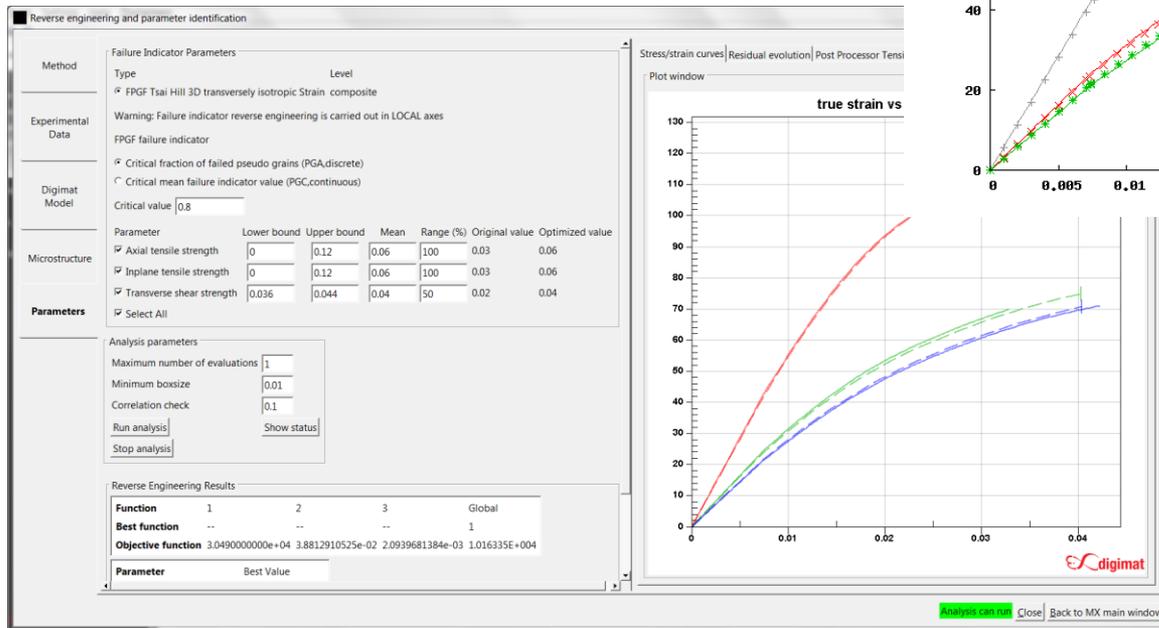
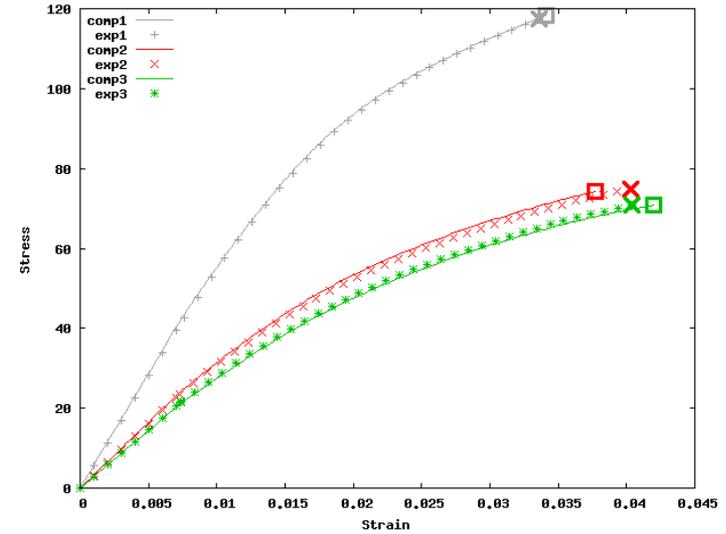
Hybrid solution

✓ Improved accuracy



Reverse Engineering

- ✓ FPGF based failure indicators
 - Tsai-Hill 3D transversely isotropic
 - STRESS
 - STRAIN



Reverse engineering and parameter identification

Method: Failure Indicator Parameters

Type: Level

Experimental Data: Warning: Failure indicator reverse engineering is carried out in LOCAL axes. FPGF failure indicator.

Digmat Model: Critical value: 0.8

Parameter	Lower bound	Upper bound	Mean	Range (%)	Original value	Optimized value
Axial tensile strength	0	0.12	0.06	100	0.03	0.06
Inplane tensile strength	0	0.12	0.06	100	0.03	0.06
Transverse shear strength	0.036	0.044	0.04	50	0.02	0.04

Analysis parameters: Maximum number of evaluations: 1, Minimum boxsize: 0.01, Correlation check: 0.1, Run analysis, Show status, Stop analysis

Reverse Engineering Results:

Function	1	2	3	Global
Best function	--	--	--	1
Objective function	3.0490000000e+04	3.8812910525e-02	2.0939681384e-03	1.016335E+004

Parameter Best Value

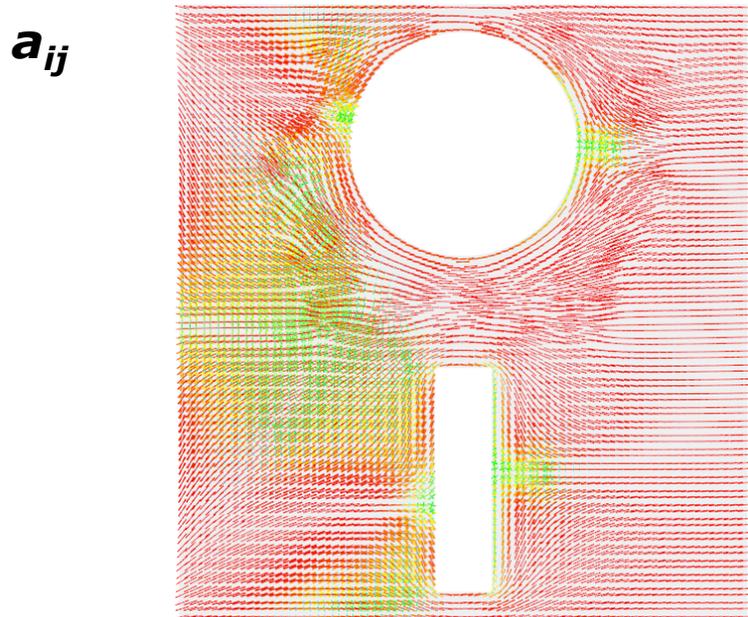
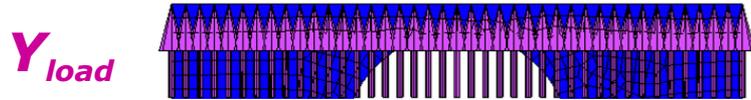
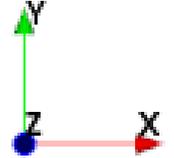
Post-Processing

Robust/Fast/Easy



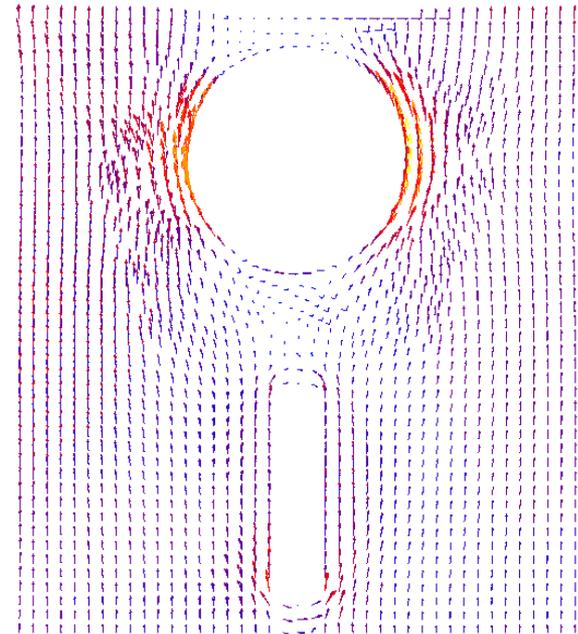
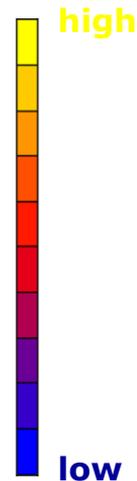
4.5.1

∞ Correlation of local stress states with fiber orientation?



fiber orientation

σ_{ij}

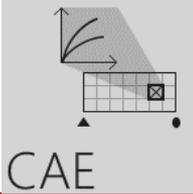


stresses



Post-Processing

Robust/Fast/Easy

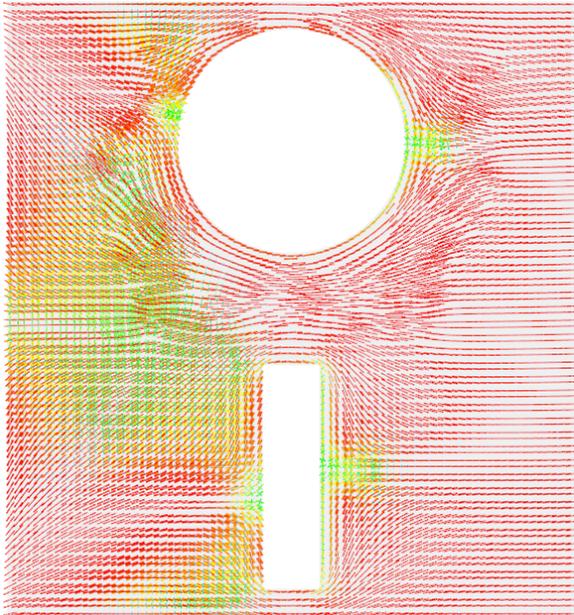


4.5.1

∞ First eigenvalue a_I of the orientation tensor a_{ij}

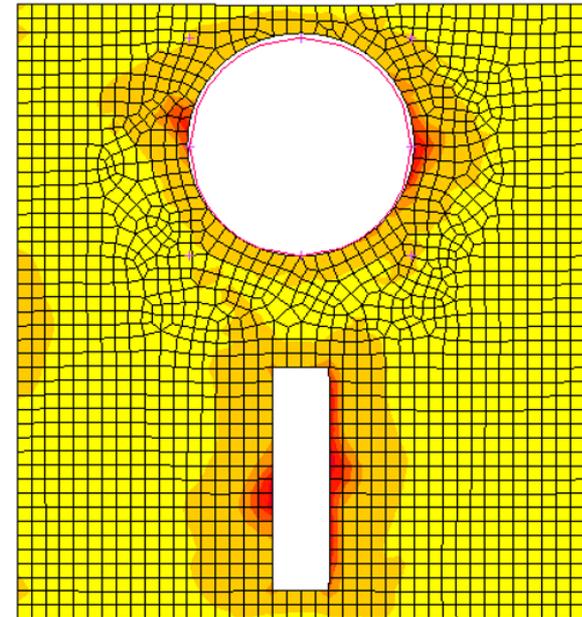
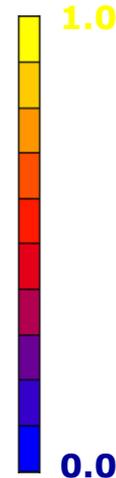
✓ Where do we find areas with strongly oriented fibers?

a_{ij}



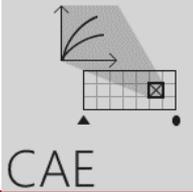
fiber orientation

a_I



Post-Processing

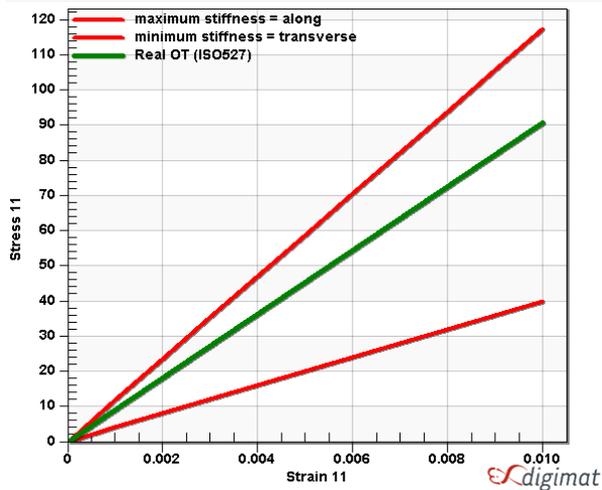
Robust/Fast/Easy



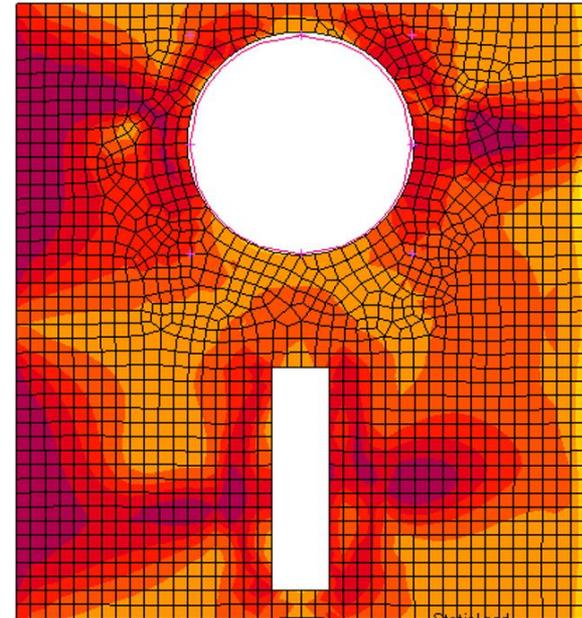
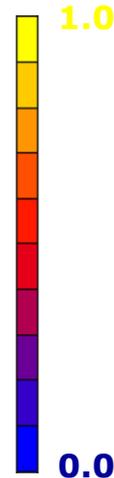
4.5.1

∞ Achieved Potential Stiffness

- ✓ How much of the potential of my material am I using?



APS



Ratio between apparent & ideal stiffness of the material

Post-Processing

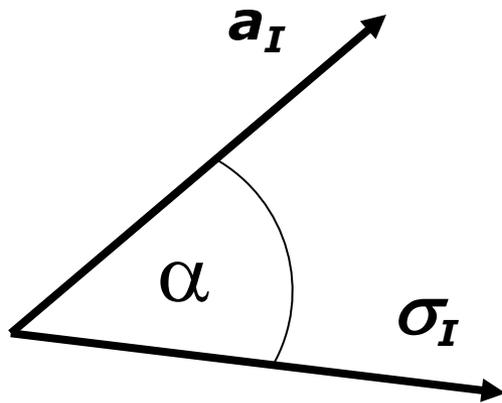
Robust/Fast/Easy



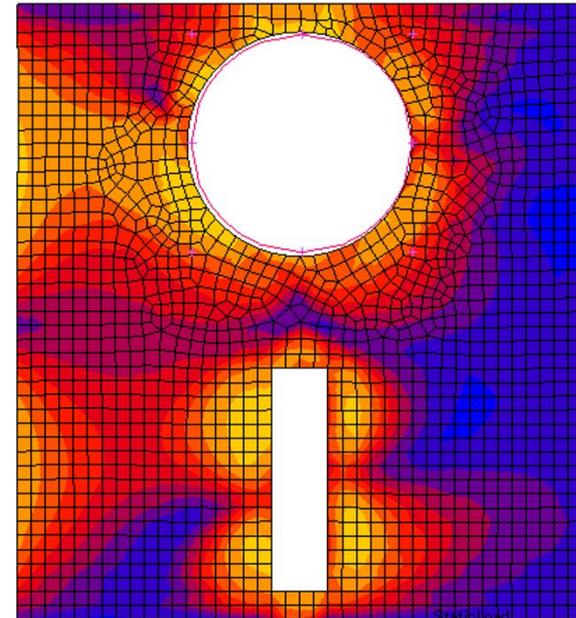
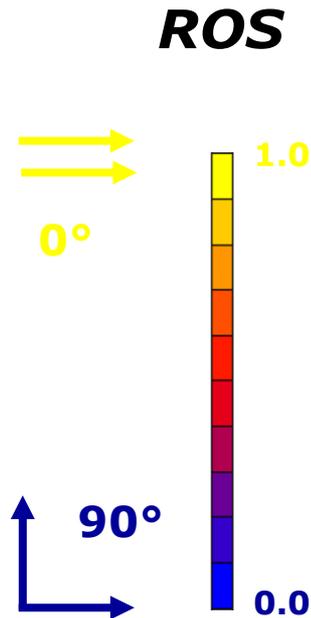
4.5.1

Relative Orientation State

- ✓ How strongly are stress and fiber orientation correlated?



Scalar product between the eigenvectors of a_I and σ_I



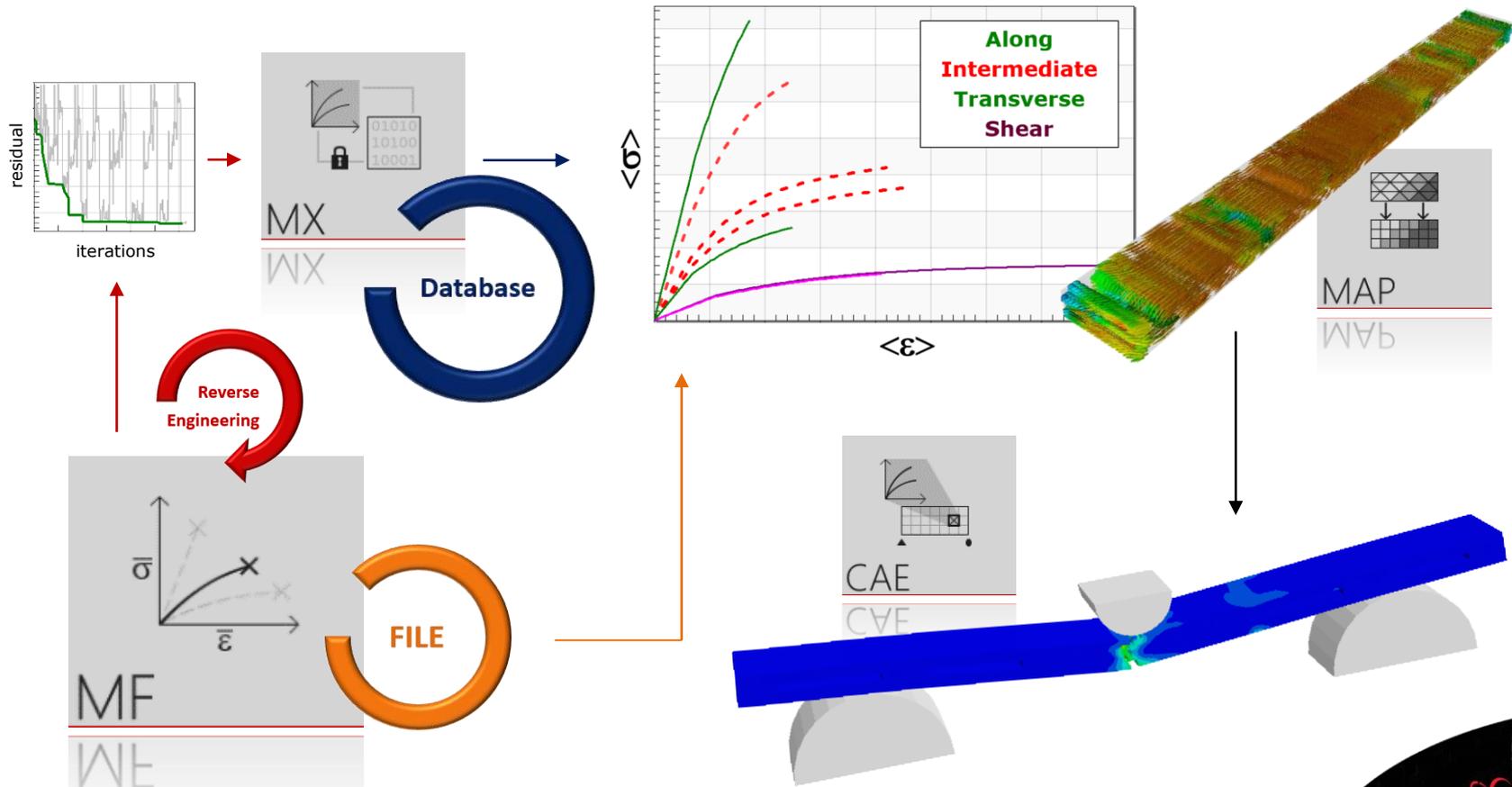
Digimat-RP

**Integrated Workflow Environment
for**

Process Chain Modeling

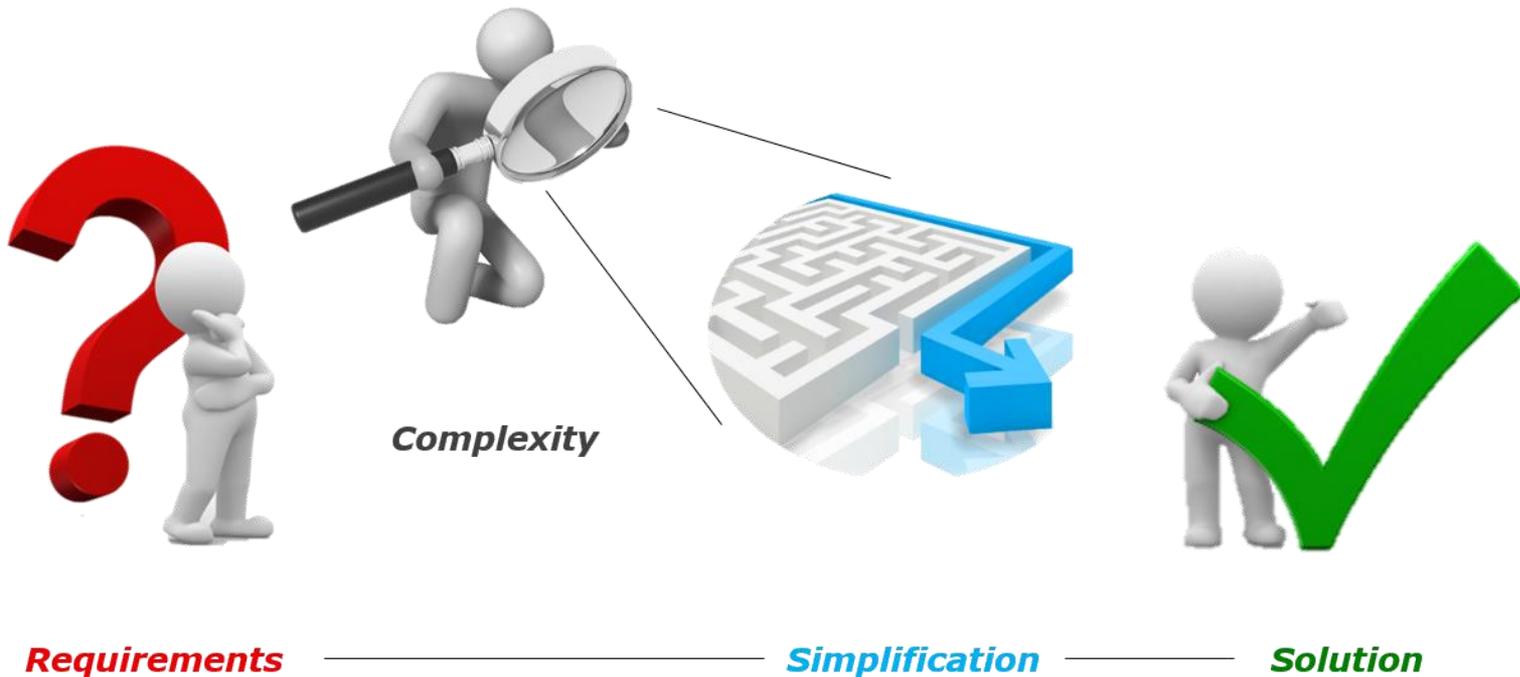
Design of Fiber Reinforced Plastic Parts

✓ Tools for multi-scale modeling



∞ Solutions

- ✓ Integrated workflow environment
- ✓ Usable for experts & non-experts alike

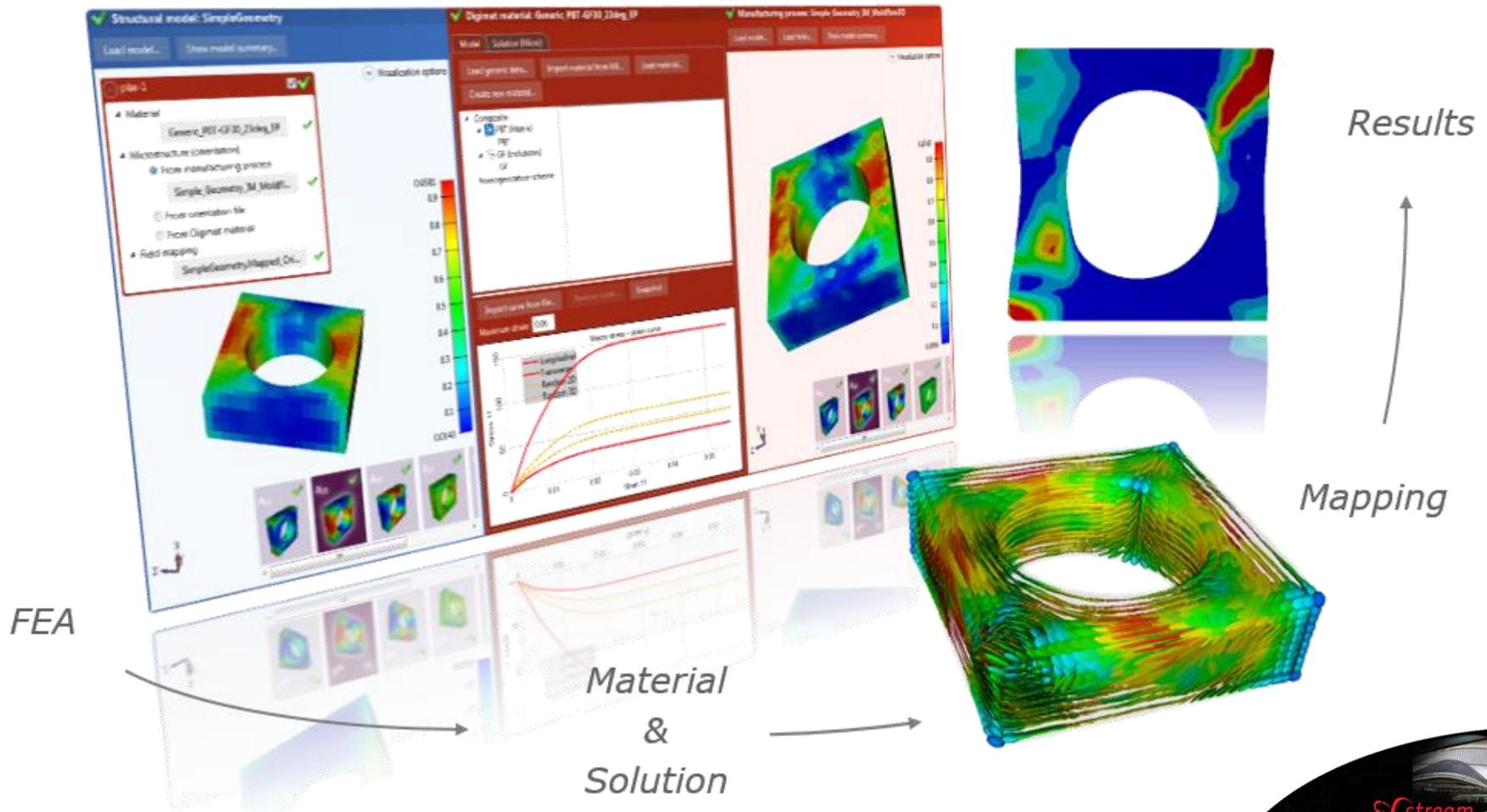


Workflow

Digmat-RP



Integrated Workflow Environment





STRUCTURAL MODEL

✓ Prerequisites

- The structural model must be complete and ready to run with the targeted FEA code
- The regions of the structural FEA model where a Digmat material is to be used must have a specific material assigned
 - If several different Digmat materials are to be used, then each associated region must have its own unique material

✓ Limitations

- 3D solid elements
- Bi-phase Digmat materials only
- No advanced output management

RP acts upon the material model of an existing FEA input deck!





✓ Short (& long) fiber reinforced plastics

- **Injection Molding**

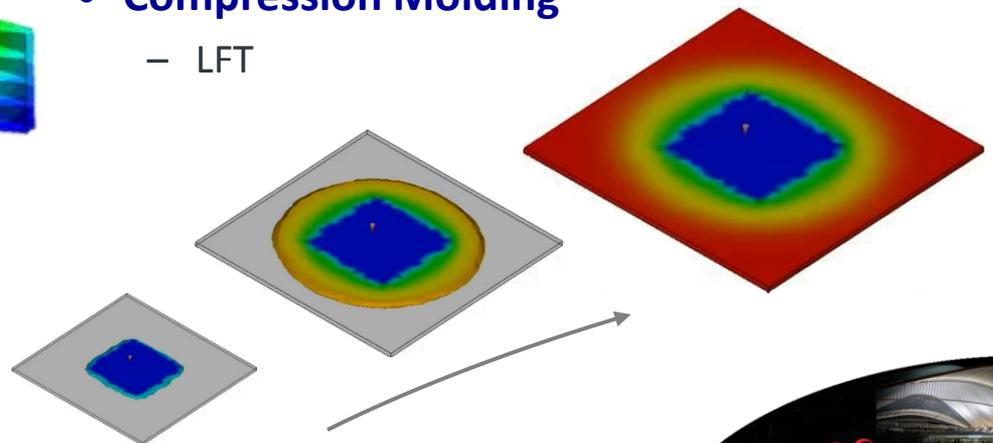
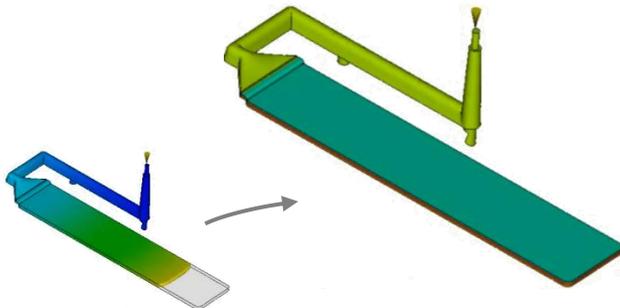
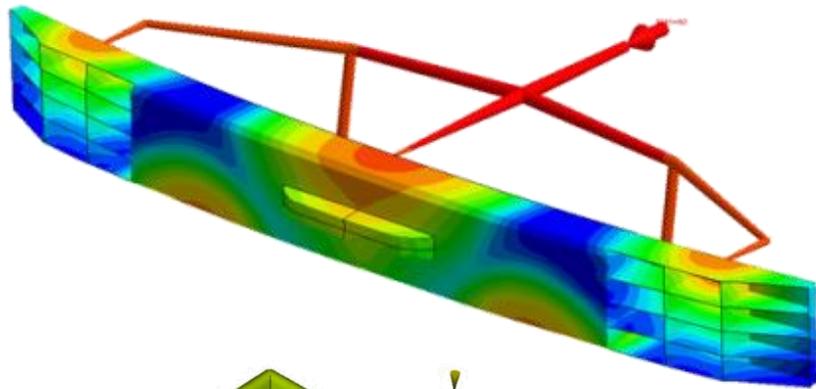
- SFRP

- **Injection-Compression Molding**

- SFRP / LFT

- **Compression Molding**

- LFT



Capabilities

Digmat-RP



✓ Short (& long) fiber reinforced plastics

- **Supported Software**

- *3D analyses*

- ✓ **Moldflow**

- .xml



- ✓ **Sigmasoft**

- .xml



- ✓ **Moldex3D**

- .o2d



- ✓ **3D Timon**

- .bou

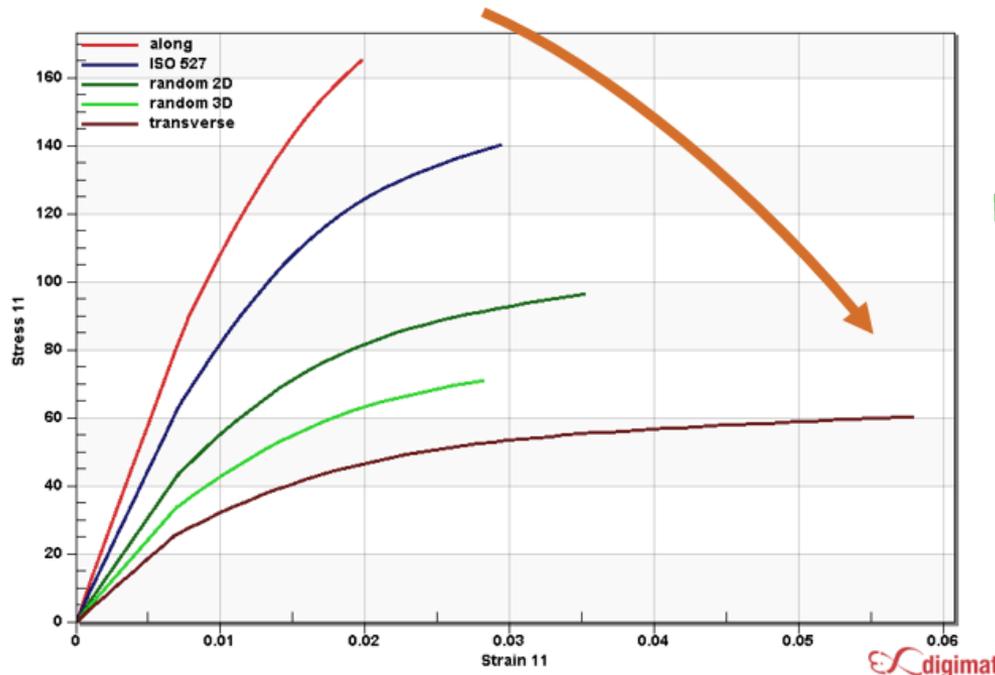


Capabilities

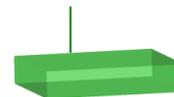
Digmat-RP



- ✓ Short (& long) fiber reinforced plastics
- ✓ Properties



Anisotropy



- (Thermo-) Linear Elasticity
- (Thermo-) Elastoplasticity
- (Thermo-) Viscoelasticity
- (Thermo-) Elasto-Viscoplasticity

+ Failure



✓ Short (& long) fiber reinforced plastics

- **Levels of quality**

- *Choice between the effort to set up the material model and accuracy of results*

- **Quantitative**

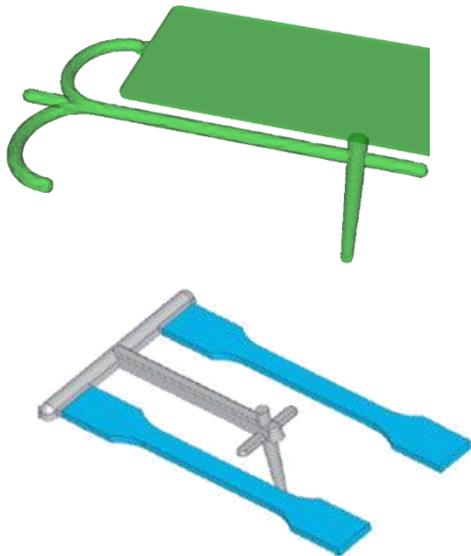
- Data: based on anisotropic measurements
- Effort: expert reverse engineering
(weeks to months)

- **Semi-Quantitative**

- Data: based on ISO 527 dumbbell
- Effort: non-expert reverse engineering
(~5-10 min.)

- **Qualitative**

- Data: representative family curve from CAMPUS database
- Effort: none
(generic & ready to run)



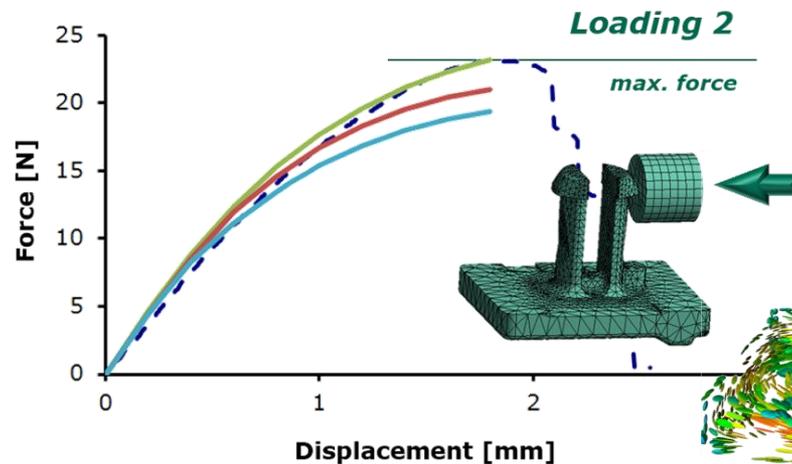
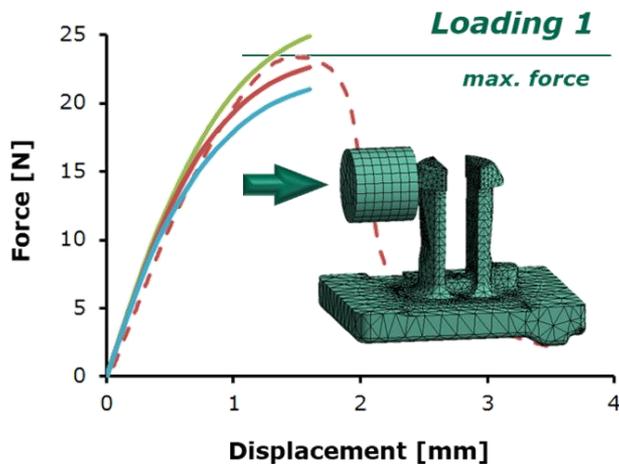


✓ Short (& long) fiber reinforced plastics

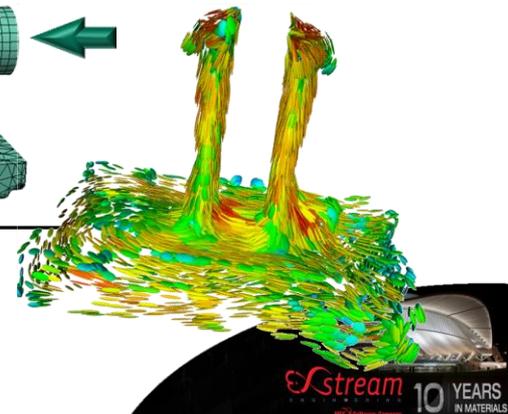
- **Levels of quality**

- *Choice between the effort to set up the material model and accuracy of results*

QUALITATIVE / SEMI-QUANTITATIVE / QUANTITATIVE



INTEVA
PRODUCTS
Ticona





✓ Short (& long) fiber reinforced plastics

• Input

- *Encryption/Decryption of material properties fully supported*

✓ Internal

- Generic grades
 - » Linear elastic

✓ From Tools

- Digmat-MX
 - Material suppliers' grades
 - Generic grades
 - » (Thermo-) Linear elastic
 - » (Thermo-) Elastoplastic

✓ From File

- Digmat-MF (.daf)
 - Build, save & use material model
 - » Any type
- Digmat-CAE (.mat)
 - Re-use previous analyses
 - » Any type
 - Use encrypted
 - » Any type

Capabilities

Digmat-RP



✓ Short (& long) fiber reinforced plastics

• Performances

NVH

E - Linear Elastic

Stiffness (quasi-static)

E/EP - Linear elastic / Elastoplastic

TE/TEP - Temperature dependent

Impact & Failure

VE/EVP - Viscoelastic / Elasto-Viscoplastic

+ FPGF - Failure of SFRP

(Thermal) Creep

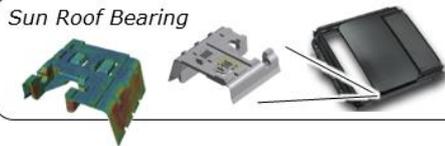
VE / TVE - Viscoelastic

EVP / TEVP - Elasto-Viscoplastic

Front End



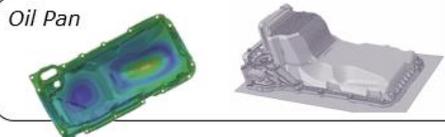
Sun Roof Bearing



Engine Mount



Oil Pan





✓ Short (& long) fiber reinforced plastics

- **Solution Methods**

- *Choice between accuracy of results and performance of the computation (CPU)*

✓ **MACRO**

- Linear elastic weak coupling
- High efficiency in CPU

✓ **MICRO**

- Nonlinear strong coupling
- Highest accuracy in stiffness

✓ **HYBRID**

- Nonlinear weak coupling
- High efficiency in CPU
- High accuracy in stiffness
 - E, EP, EVP, TE, TEP
- Highest accuracy in failure of SFRP

Capabilities

Digmat-RP



✓ Short (& long) fiber reinforced plastics

- **IMPLICIT** – Supported software
 - *3D analyses*

✓ MSC Nastran SOL400

.bdf / .dat



✓ Abaqus STD

.inp



✓ Marc

.dat



✓ Ansys

.cdb / .inp / .dat



Capabilities

Digmat-RP



✓ Short (& long) fiber reinforced plastics

- **EXPLICIT** – Supported software
 - *3D analyses*

✓ MSC Nastran SOL700

.bdf / .dat



✓ Abaqus Explicit

.inp



✓ LS-Dyna

.k / .key



Summary

✓ FEA

- Marc, MSC Nastran (SOL400 /700), Abaqus (Standard/Explicit), Ansys, LS-Dyna (Implicit/Explicit)

✓ Material

- Generic / File (.daf & .mat) / Digmat-MX / Digmat-MF
- Support of encryption

✓ Solutions

- Macro, Micro, Hybrid + User defined templates

✓ Manufacturing

- Moldflow3D, Moldex3D, Sigmasoft, Timon3D

✓ Job management (submission & monitoring)

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