



A Simple Method for an Appropriate Simulation of Short-Fiber-Reinforced Injection Molded Plastics

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CAE Services & Software

Technical Simulation

Contract Simulation Services
in FEA

CAE Staffing

Resident Engineers at
customers' sites

CAE Software

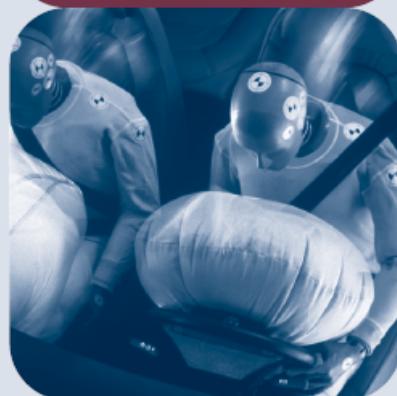
- Process-Structure-Interaction
- Strength & Fatigue Assessment

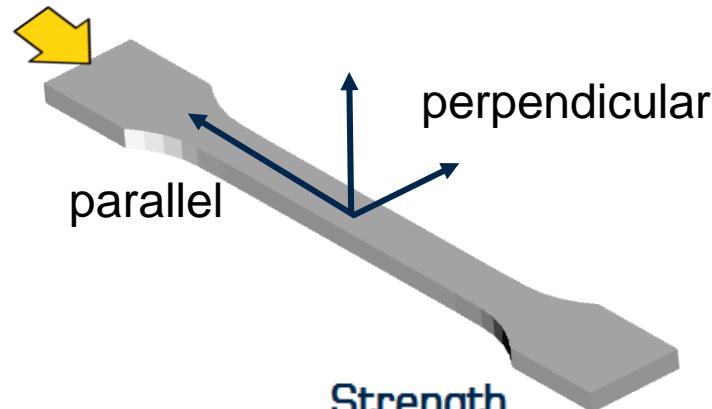
Elastomers



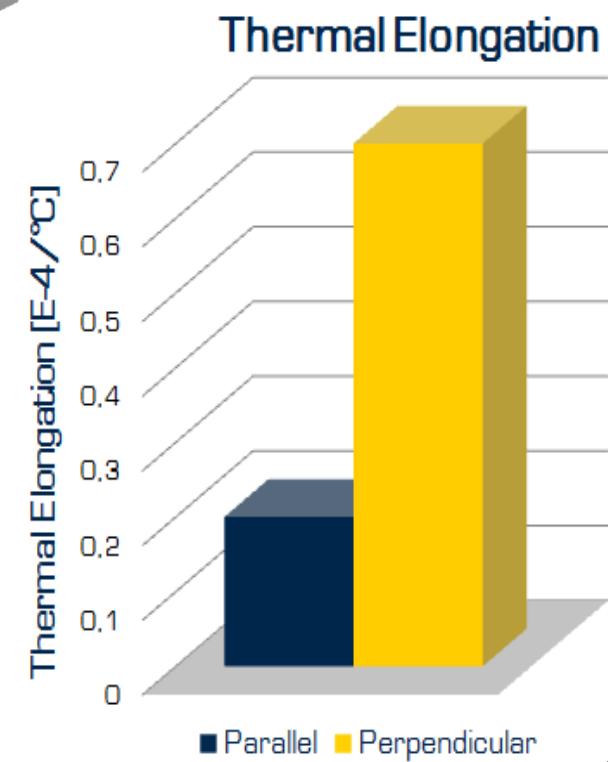
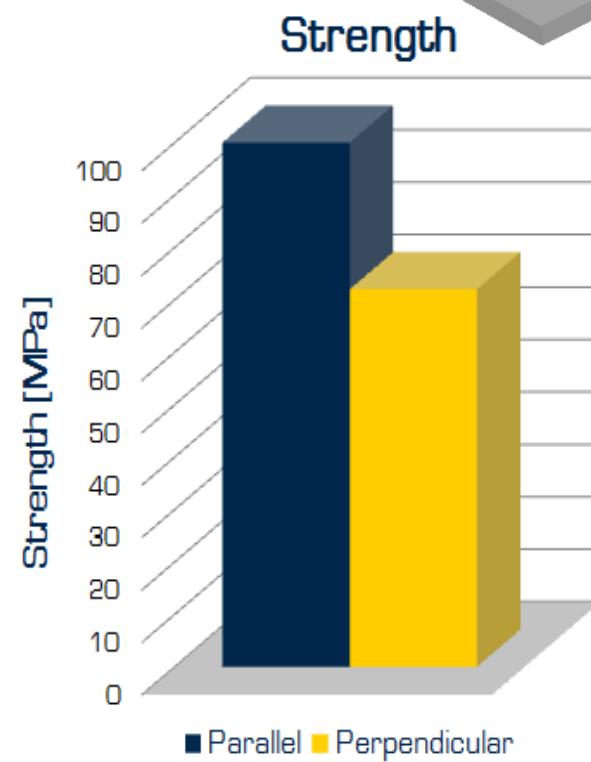
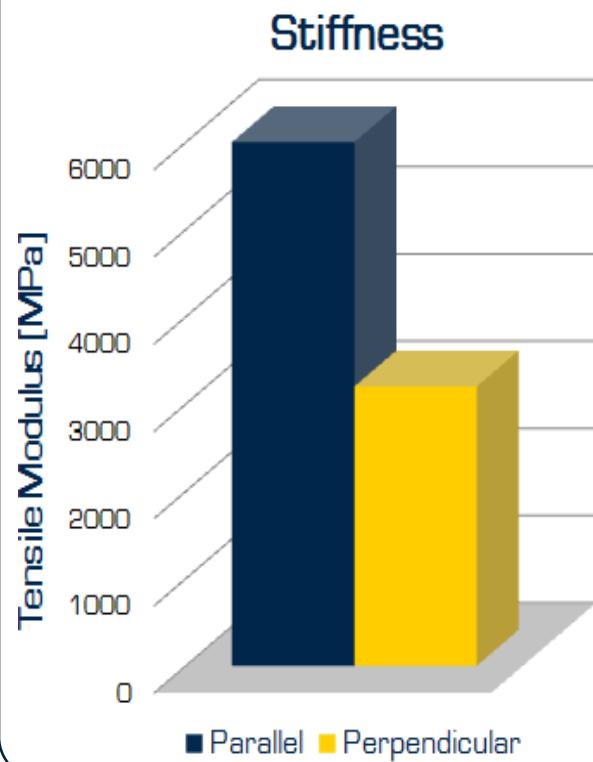
Plastics

Metals



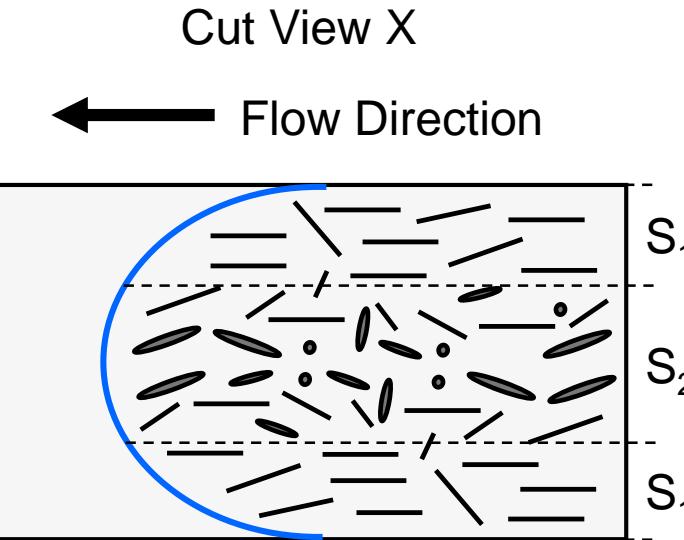
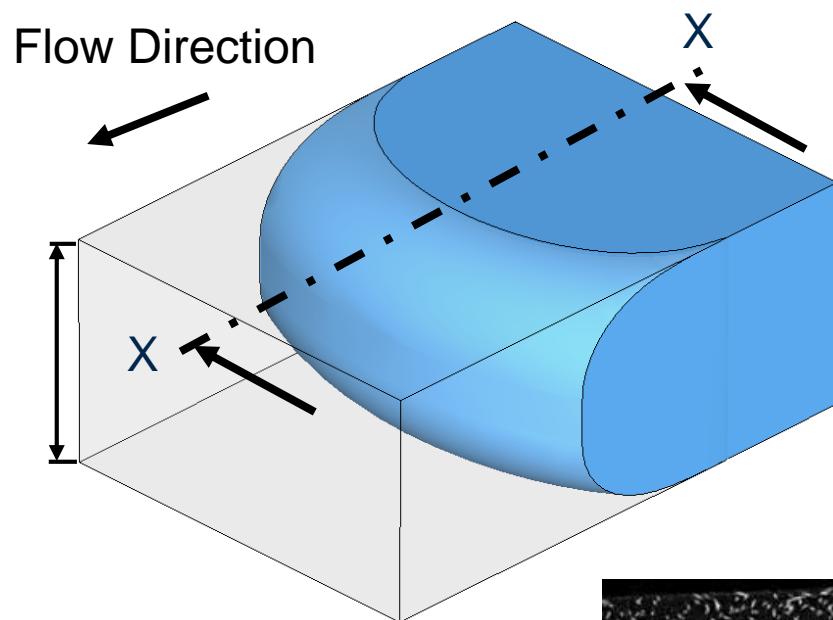


Material:
PA6+GF30

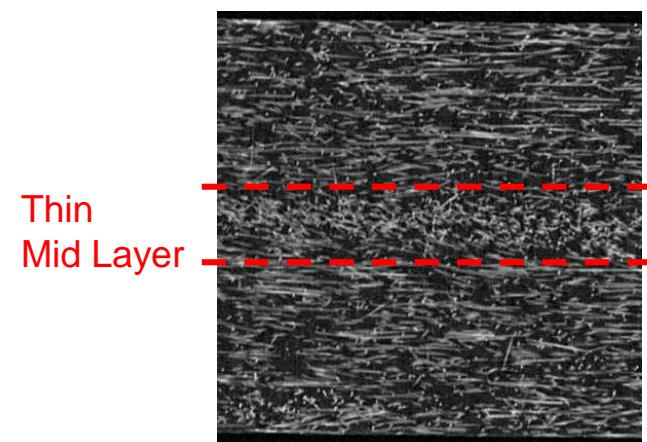
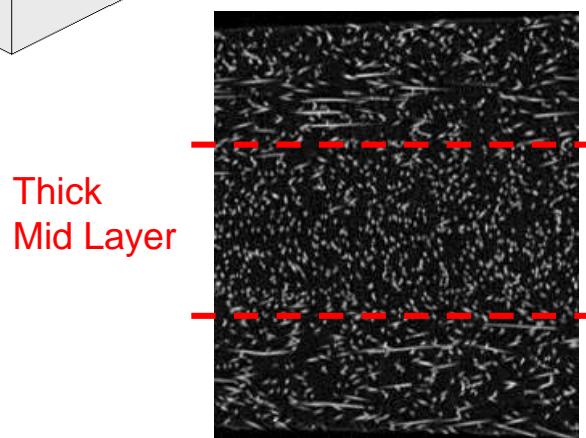


Influence of Fiber Orientation onto Material Properties

S_1 Shear layer: Fibers oriented parallel to flow direction
 S_2 Mid layer: Fibers oriented perpendicular to flow direction



Example
Micrograph
Pictures:



Fiber Orientations in Short-Fiber-Reinforced Plastics

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Fig. 3

The yield function is defined as

$$f = \bar{f}(\sigma) - [\sigma_0 + R(\varepsilon^p)]$$

where the equivalent stress σ_{eq} is defined as an anisotropic yield criterion

$$\sigma_{eq} = \sqrt{F(\sigma_{22} - \sigma_{33})^2 + G(\sigma_{33} - \sigma_{11})^2 + H(\sigma_{11} - \sigma_{22})^2 + 2L\sigma_{23}^2 + 2M\sigma_{31}^2 + 2N\sigma_{12}^2}$$

Where F, G, H, L, M and N are constants obtained by test of the material in different orientations. They are defined as

$$F = \frac{1}{2} \left(\frac{1}{R_{22}^2} + \frac{1}{R_{33}^2} - \frac{1}{R_{11}^2} \right)$$

$$G = \frac{1}{2} \left(\frac{1}{R_{33}^2} + \frac{1}{R_{11}^2} - \frac{1}{R_{22}^2} \right)$$

$$H = \frac{1}{2} \left(\frac{1}{R_{11}^2} + \frac{1}{R_{22}^2} - \frac{1}{R_{33}^2} \right)$$

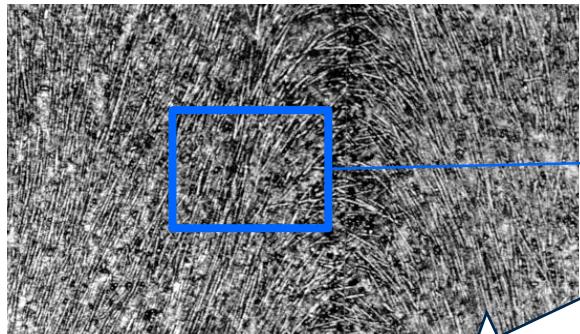
$$L = \frac{3}{2R_{23}^2}$$

$$M = \frac{3}{2R_{13}^2}$$

$$N = \frac{3}{2R_{31}^2}$$

[Source: ls-dyna-971-manual-k]

Orthotropic Elastic Plastic Material Model



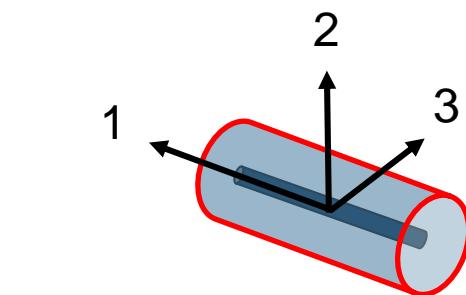
general case

$$\begin{pmatrix} a_{11} & a_{12} & a_{13} \\ . & a_{22} & a_{23} \\ . & . & a_{33} \end{pmatrix}$$



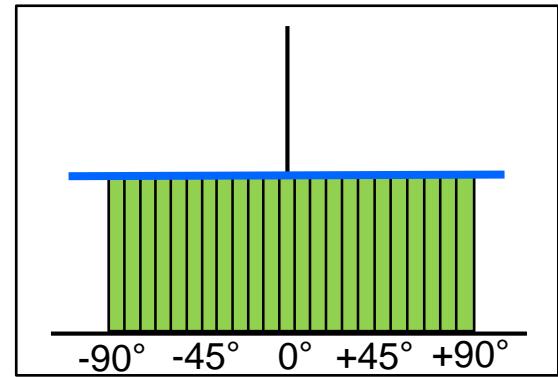
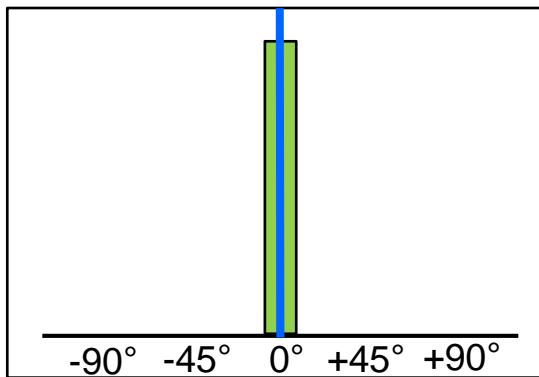
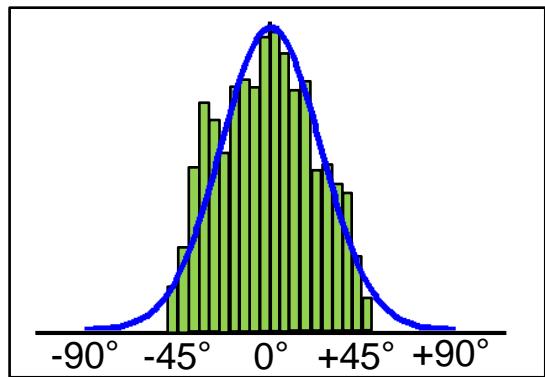
unidirectional

$$\begin{pmatrix} 1 & 0 & 0 \\ 0 & 0 & 0 \\ 0 & 0 & 0 \end{pmatrix}$$

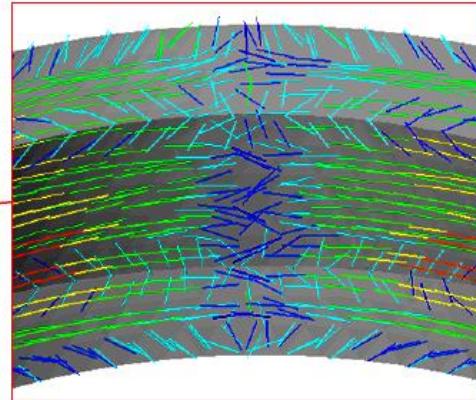
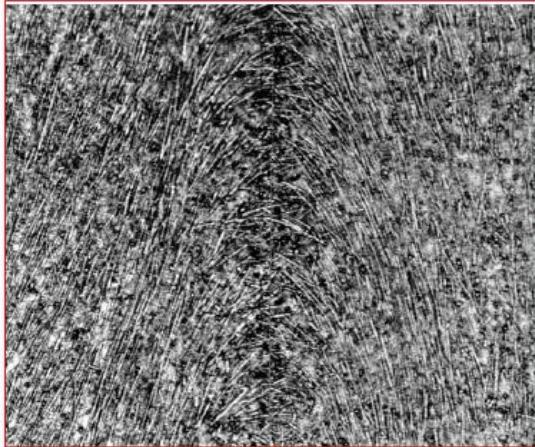


quasi-isotropic

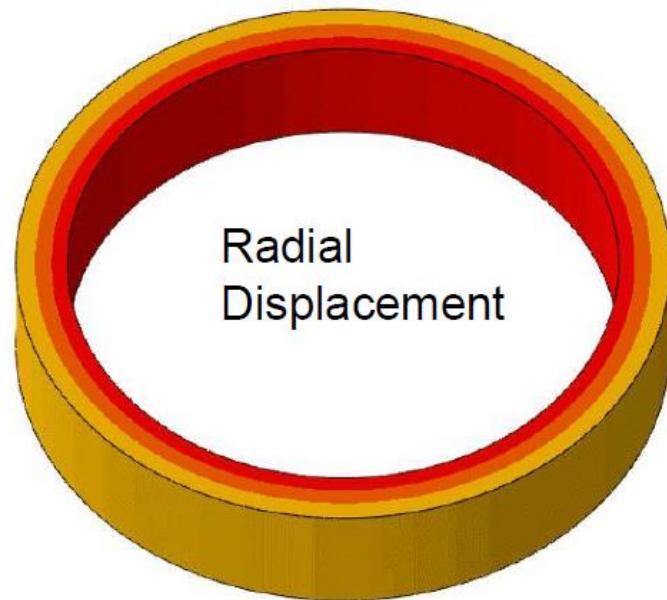
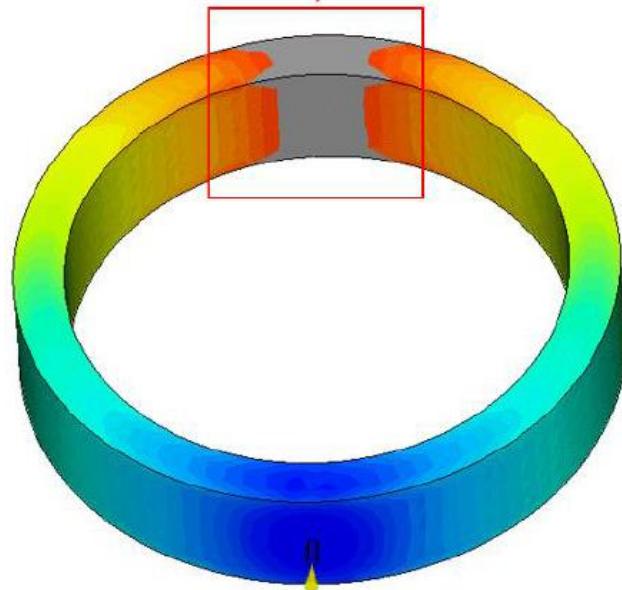
$$\begin{pmatrix} 0.33 & 0 & 0 \\ 0 & 0.33 & 0 \\ 0 & 0 & 0.33 \end{pmatrix}$$



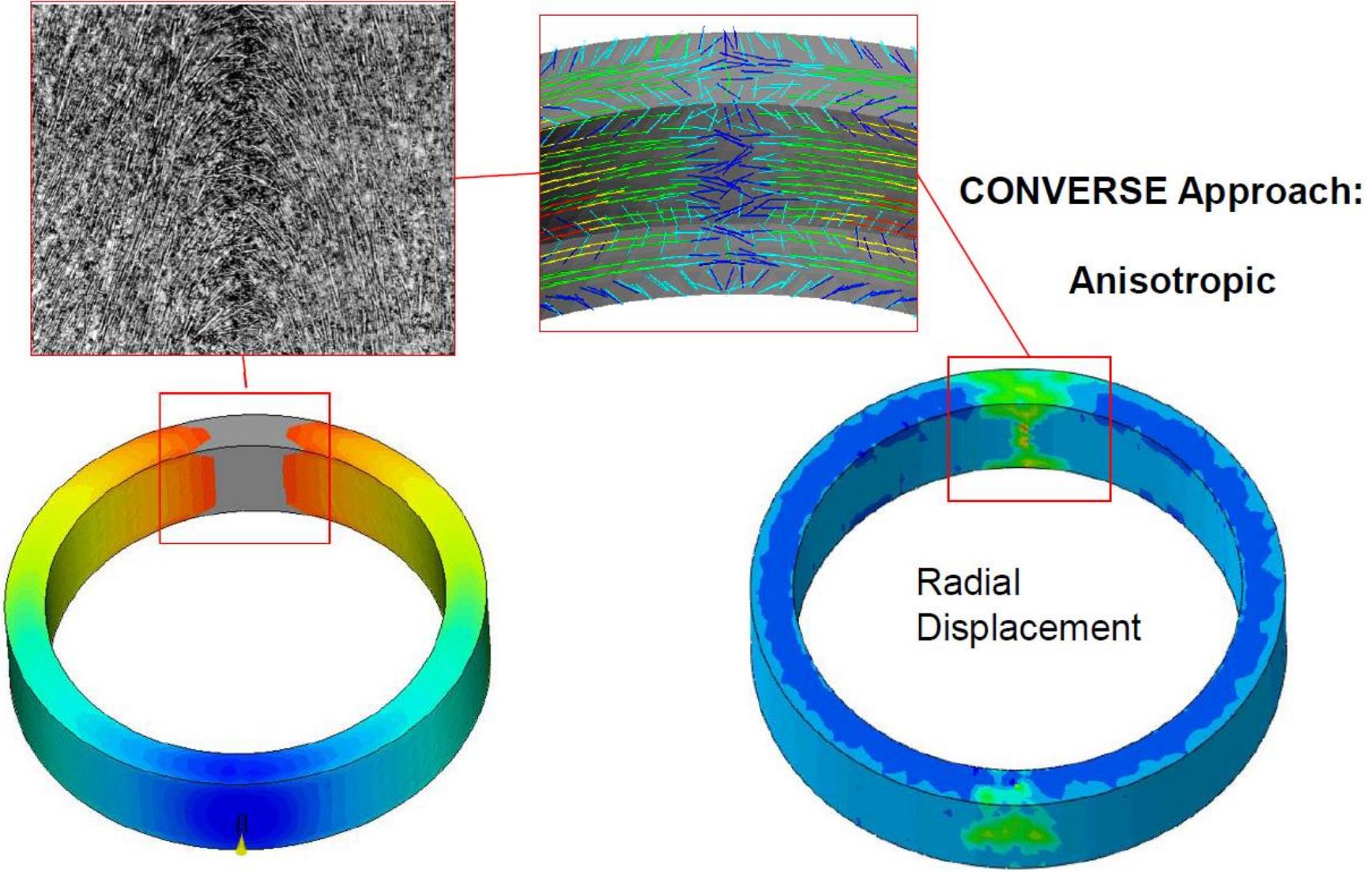
Degree of Orientation



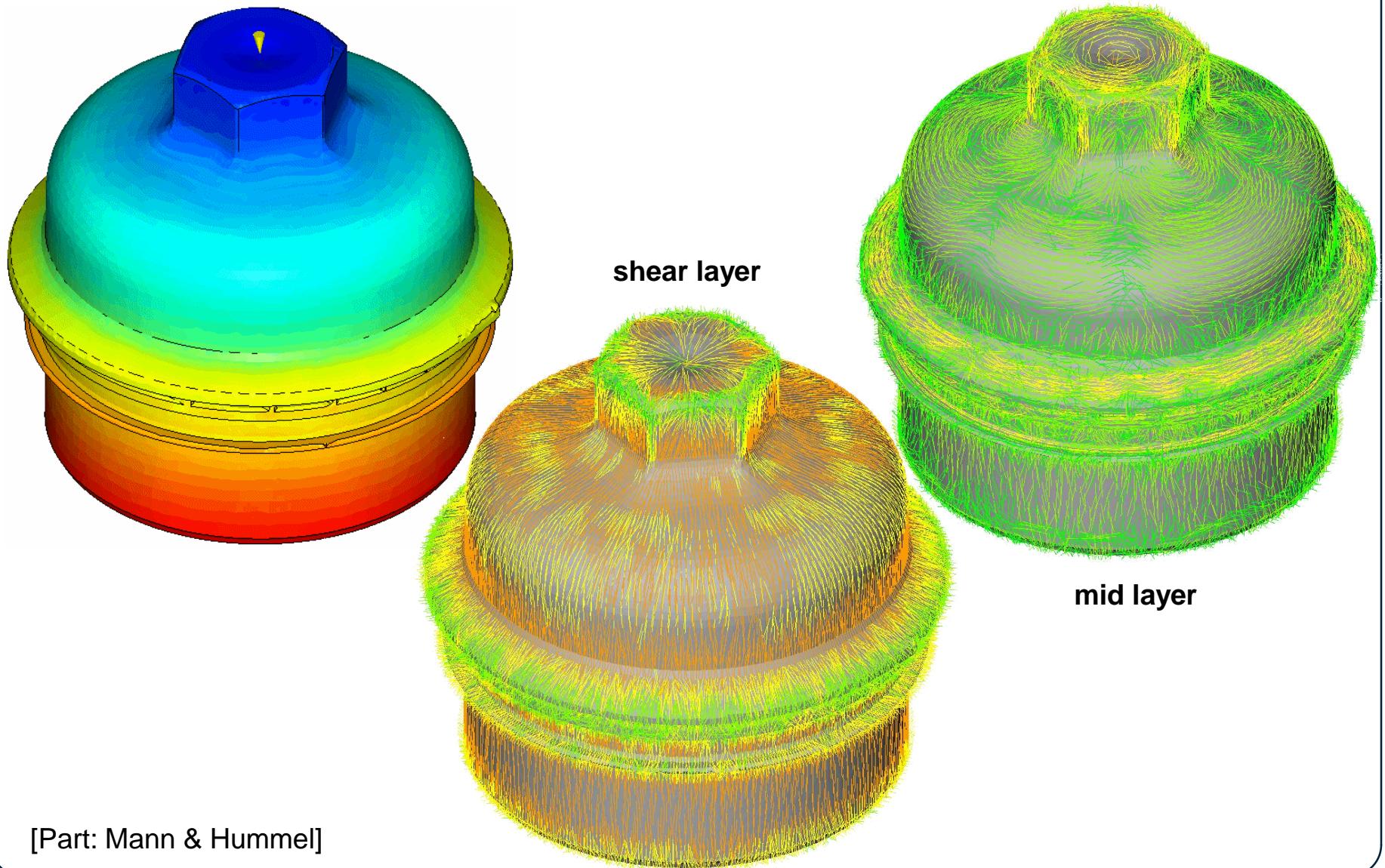
Common Approach:
Isotropic



**Example: Weld Lines
Isotropic Approach**



Example: Weld Lines
Anisotropic Approach

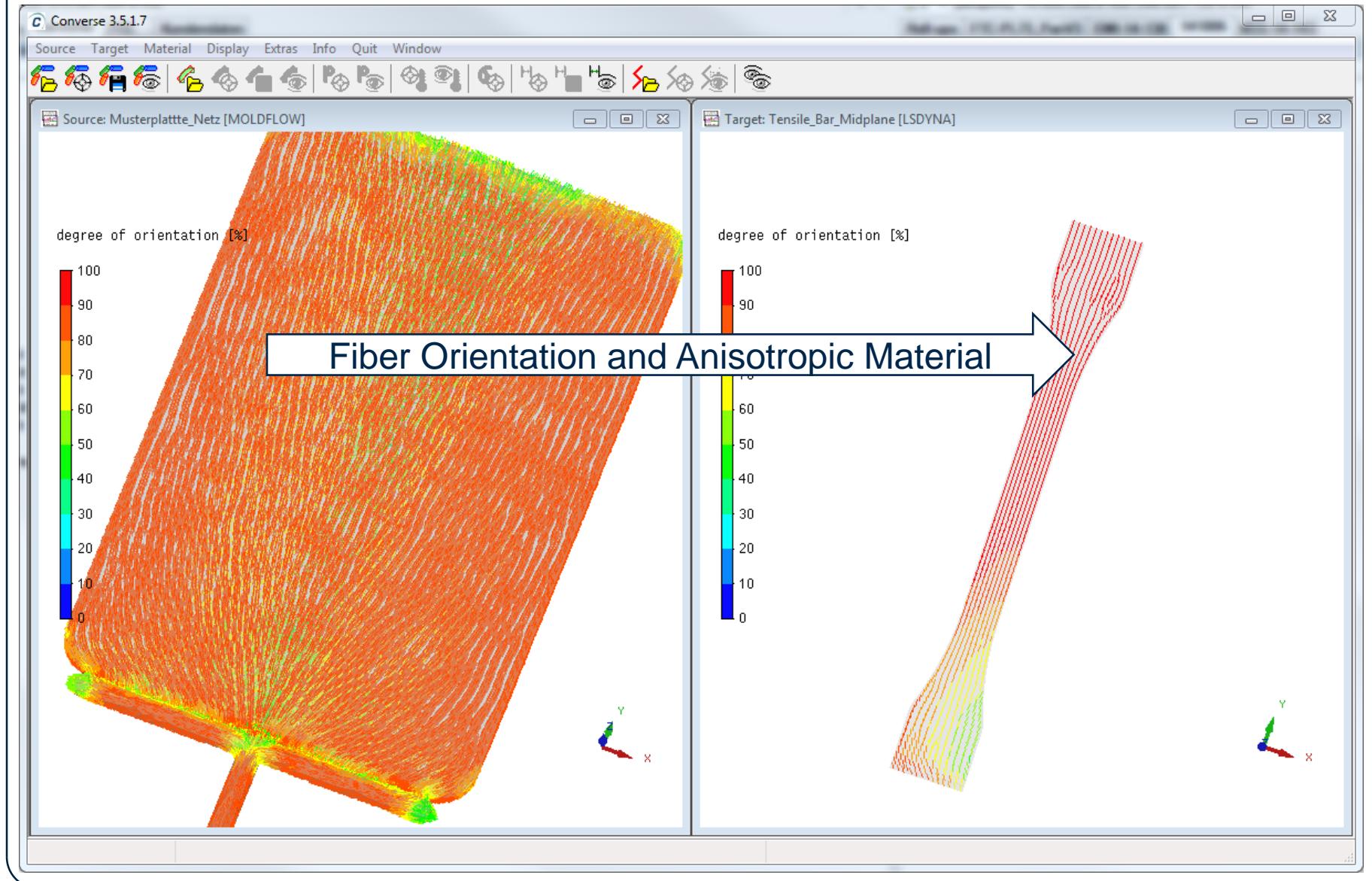


[Part: Mann & Hummel]

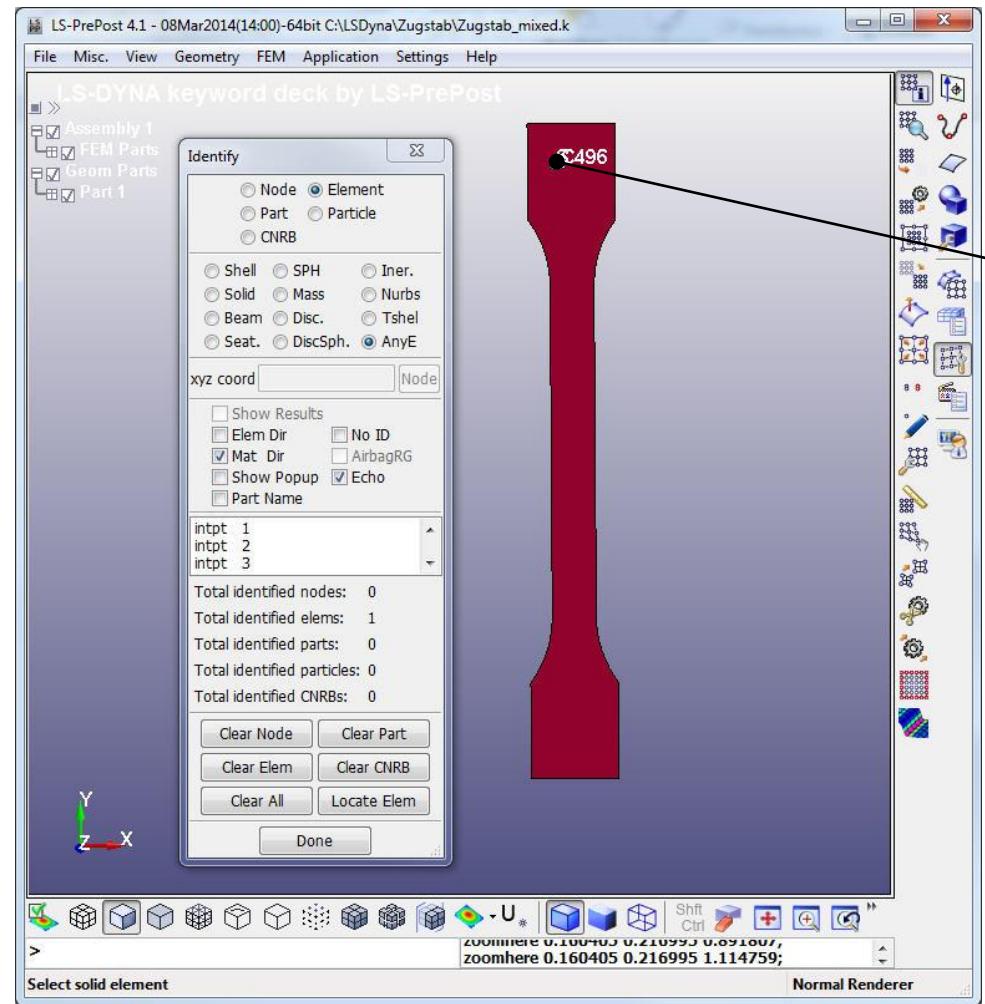
Orientation and Degree of Orientation
from Injection Molding Simulation

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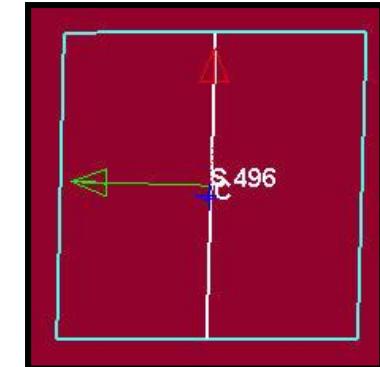
Fig. 8



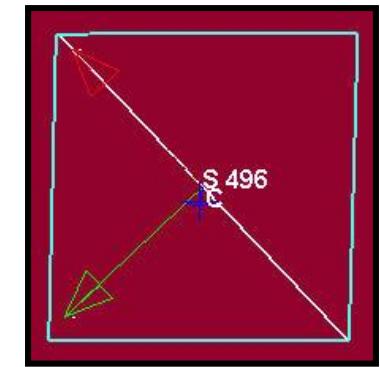
Converse Graphical User Interface



Layer 1



Layer 2



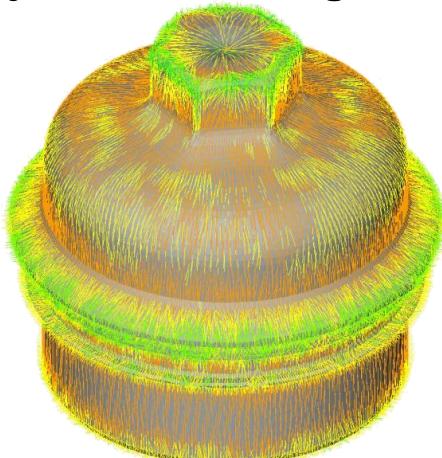
.....

material type 108

*MAT_ORTHO_ELASTIC_PLASTIC

Example: Tensile Bar Specimen

Injection Moulding Solver



- Moldflow
- Cadmould
- Sigma
- Moldex
- Fluent
- Simpoe
- 3D Timon

Orientations

Weld Lines

Pressures

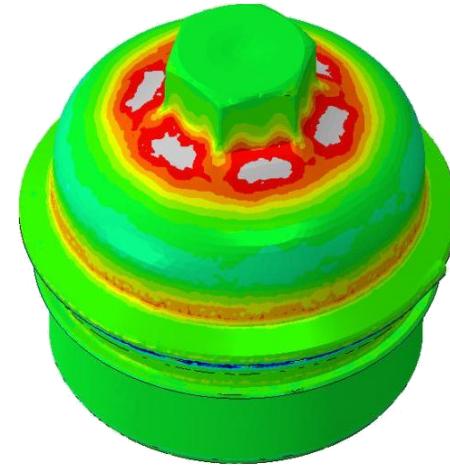
Temperatures

Wall Thicknesses

Residual Stresses

Shrinkage & Warpage

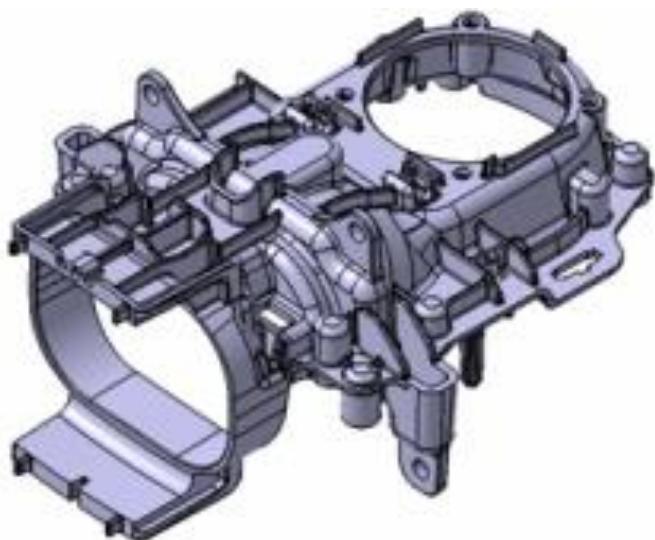
Mechanical Solver



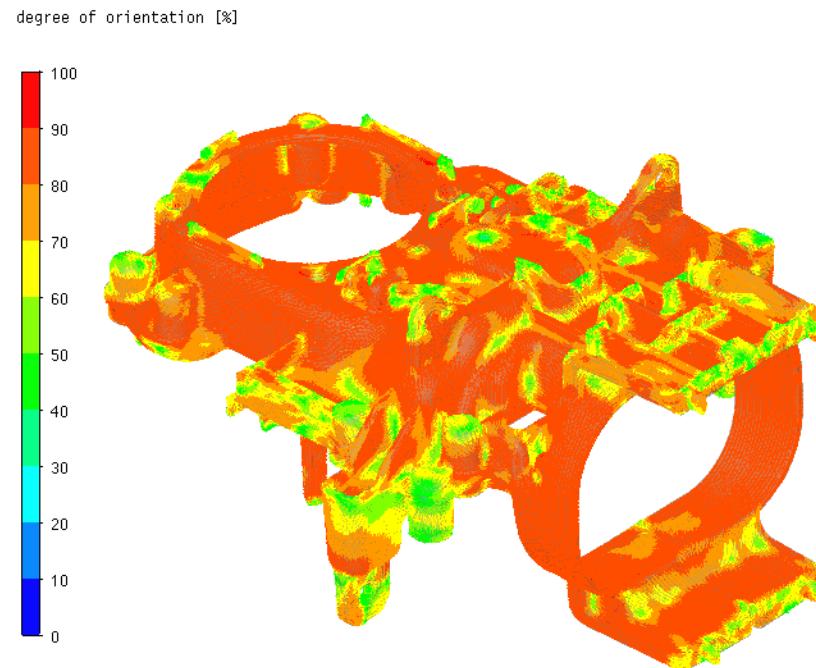
- LS-Dyna
- Ansys
- Abaqus
- Optistruct
- Nastran
- Marc
- Samcef
- FEMFat
- Ncode
- Virtual.Lab

Converse Features and Interfaces

Part Geometry



Fiber Orientation in Converse



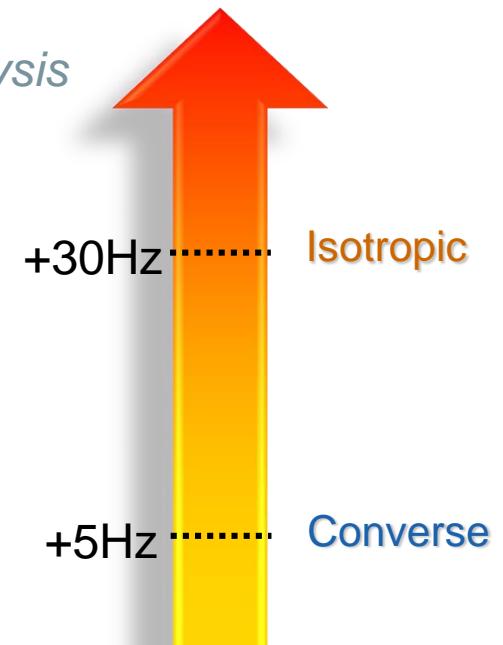
[Valeo Lighting Systems]

Lens Bracket Example

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Fig. 12

Frequency correlation – simulation to Xp. modal analysis

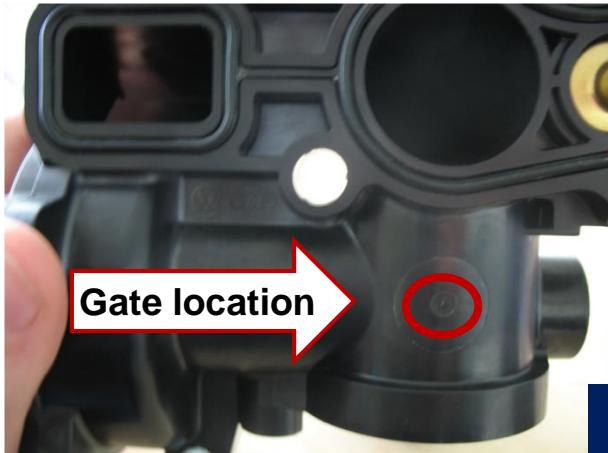


Average error – 4 Modes

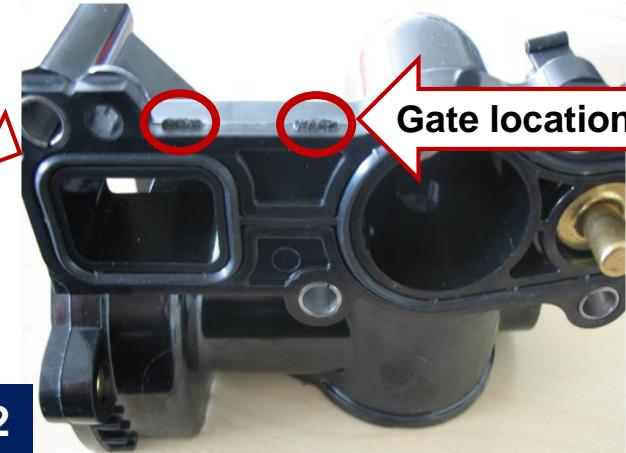
Mode	Experimental (Hz)	Isotropic (Hz)	Converse (Hz)
1	44	76	60
2	56	77	62
3	91	114	94
4	224	270	218

[Valeo Lighting Systems]

Lens Bracket Example



Supplier 1



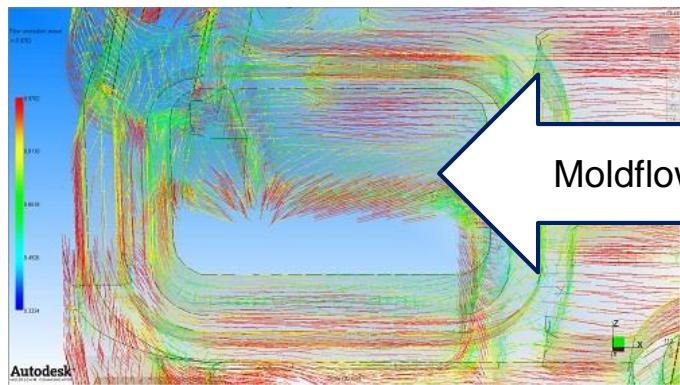
Supplier 2

Water pump housing

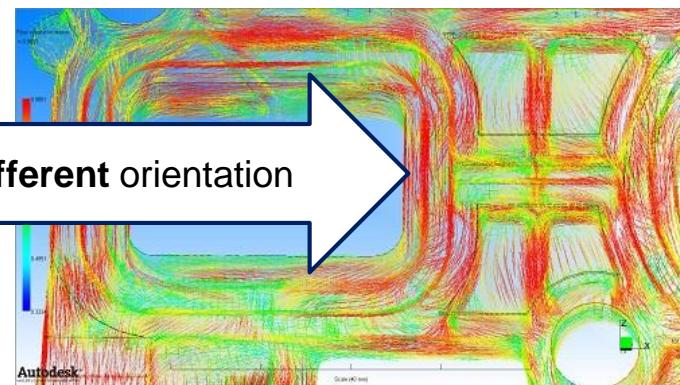
Gate location

- **Two suppliers** but parts are geometrically up to 95% **equal**.
- Same material supplier, same machine settings, etc.
- Different gating location means two **completely different** engine components!

Audi
Hungaria

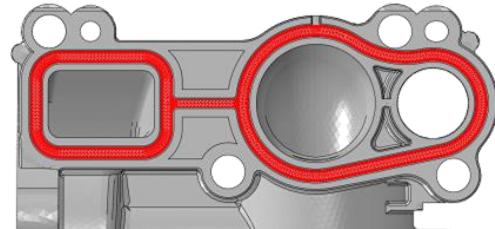


Moldflow results show **different** orientation



Influence Of Production on Fiber Orientation

1. distributed pressure on sealing contact surface

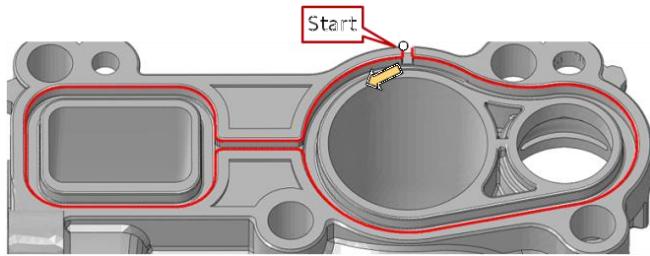


Audi
Hungaria



Untolerable error if homogeneous isotropic material is used!

2. results evaluated on a path

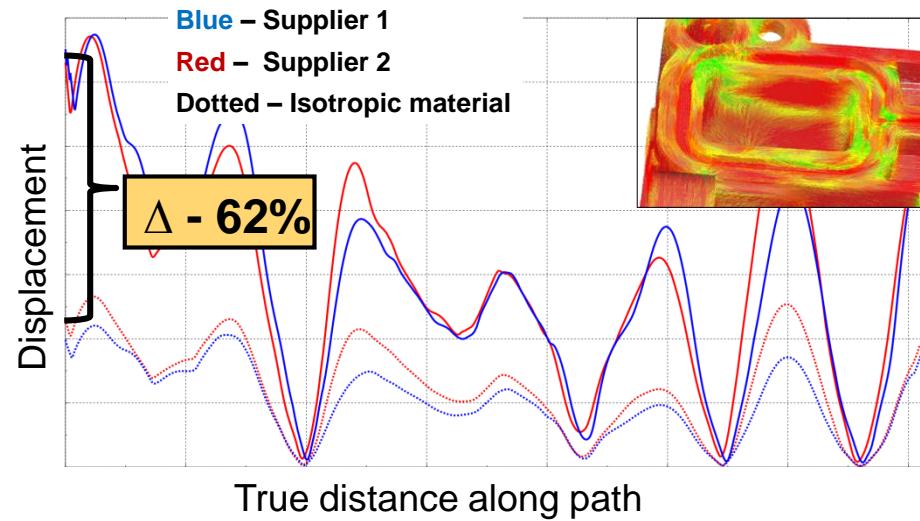
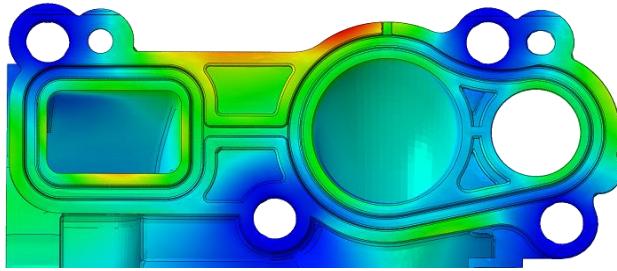


4. isotropic vs. anisotropic results

fiber orientation and material model by



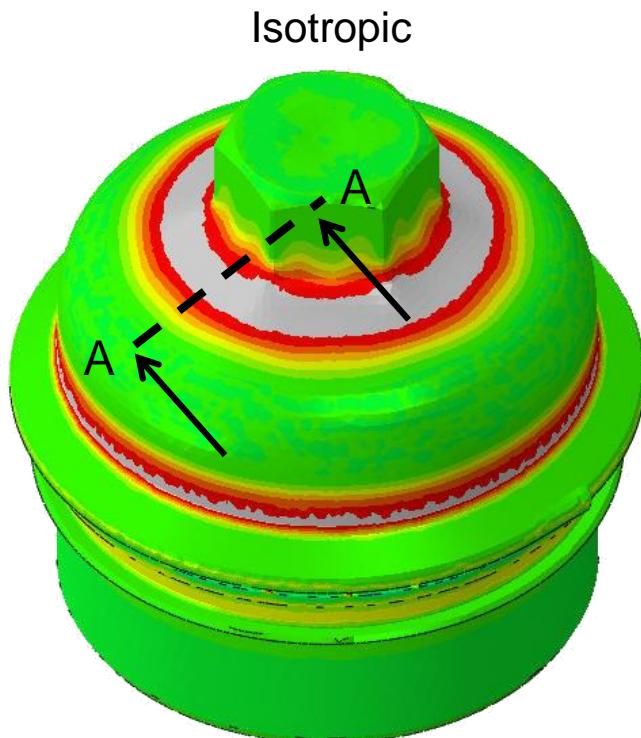
3. displacements



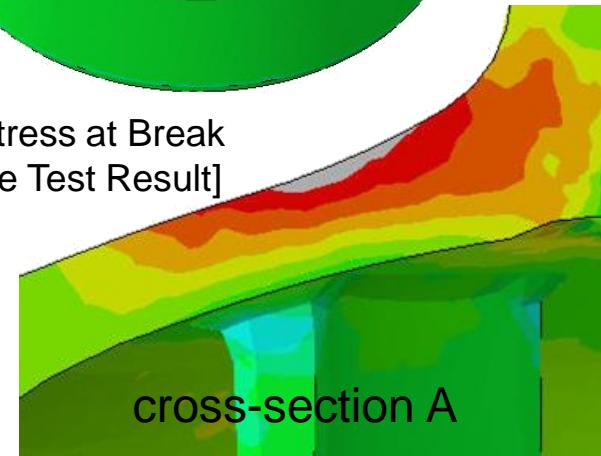
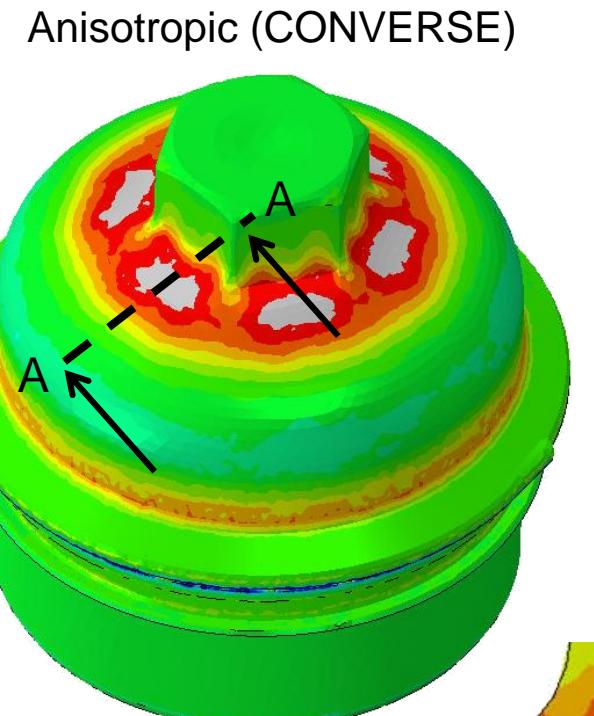
Influence Of Production on Anisotropic Part Stiffness

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Fig. 15



cross-section A

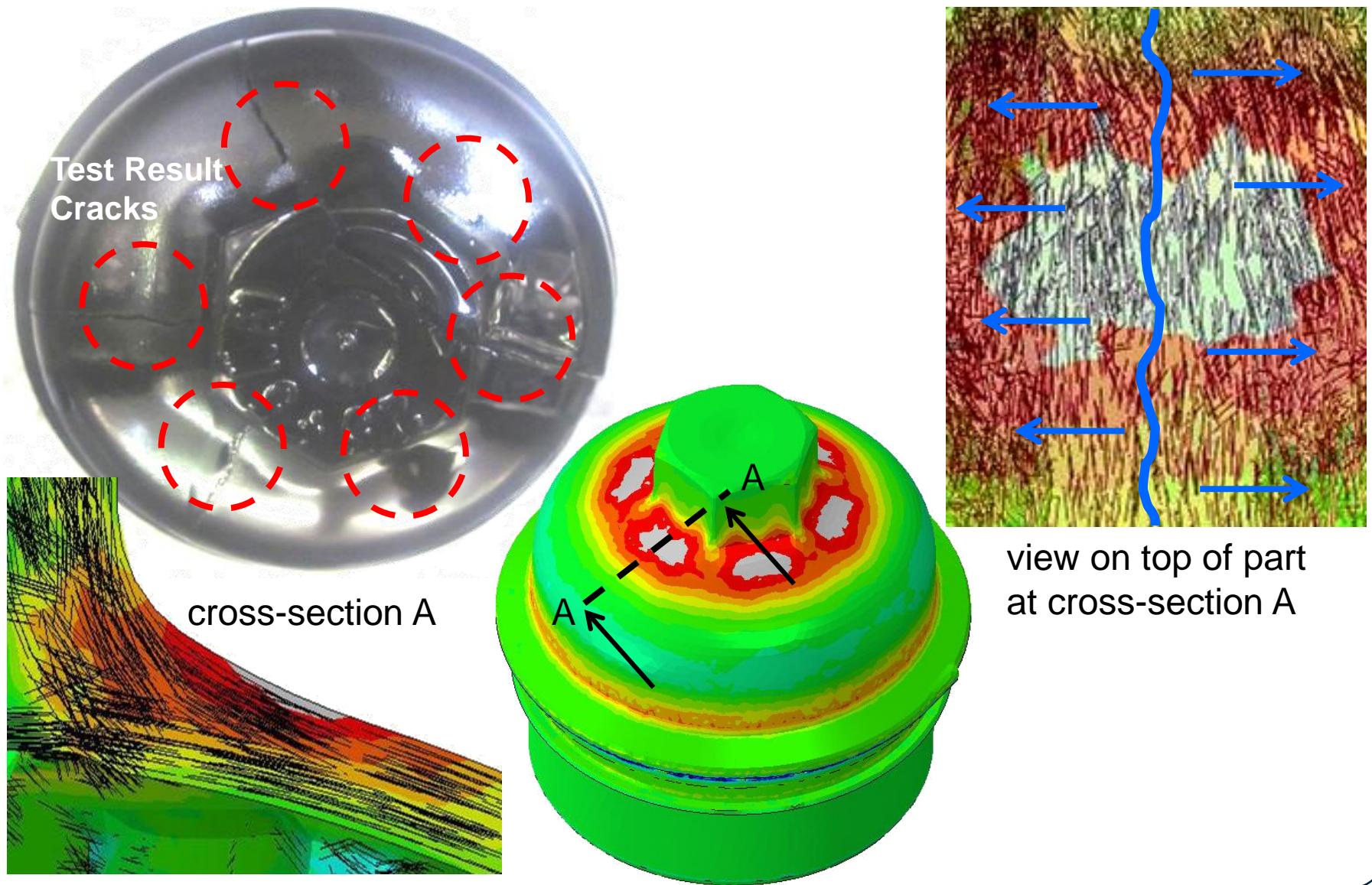


cross-section A

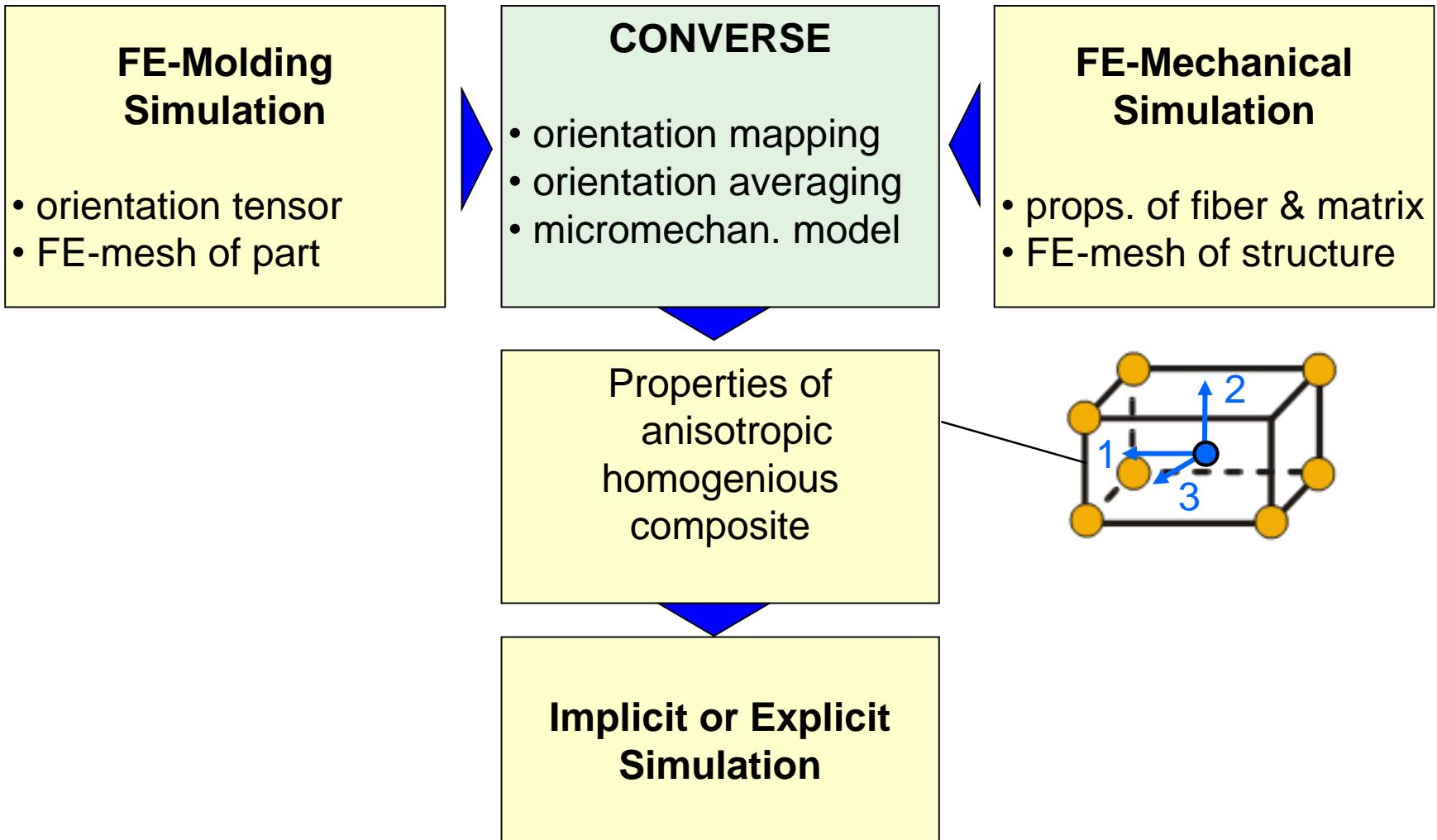
Oil Filter Cover at Burst Pressure 87,5 bar (Test Result)

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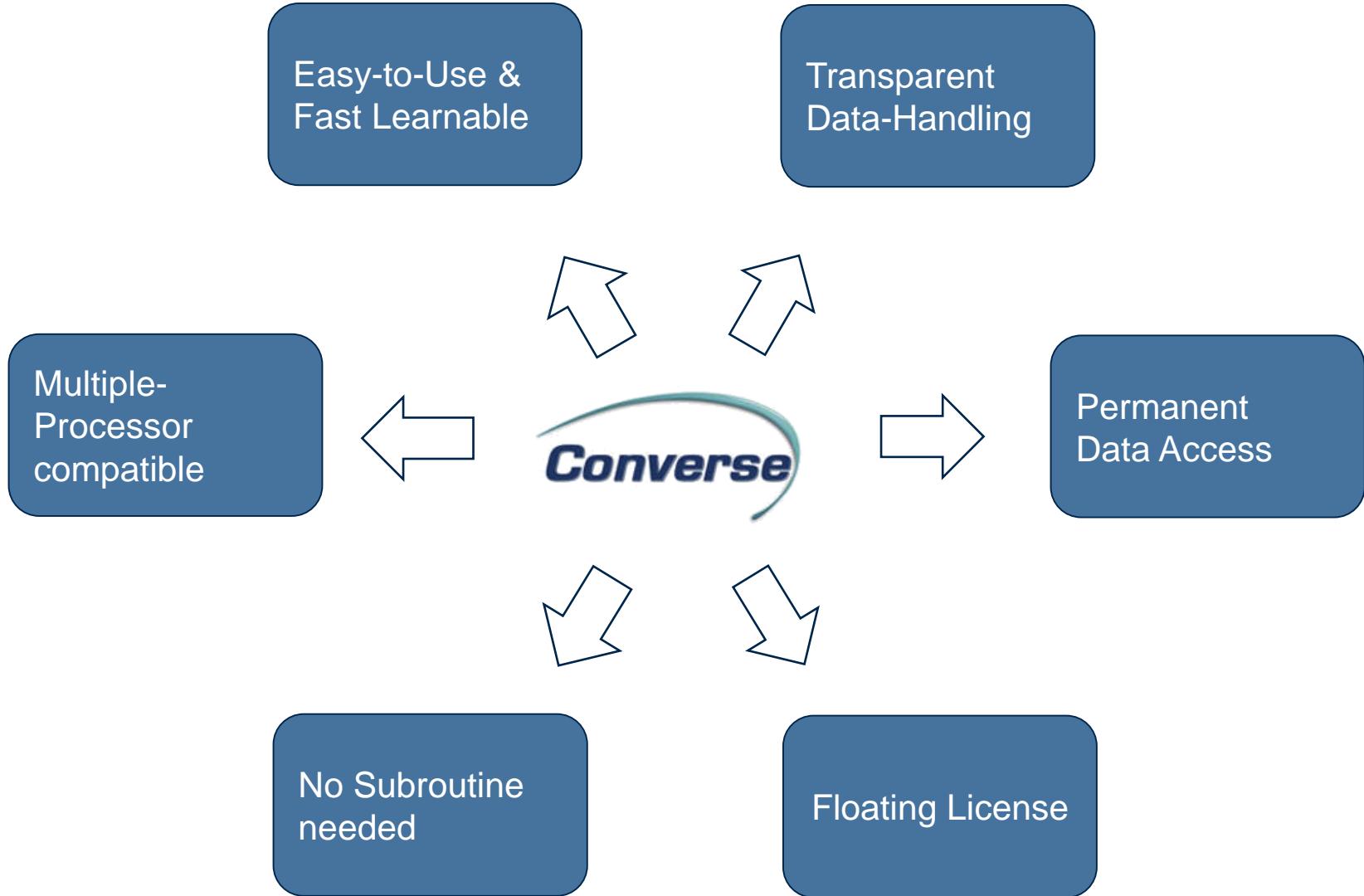
Fig. 16



Oil Filter Cover at Burst Pressure 87,5 bar (Test Result)



Summary of the Procedure for Application in FEA



Benefits