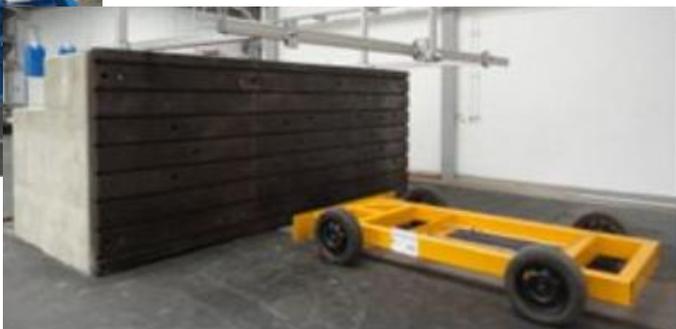
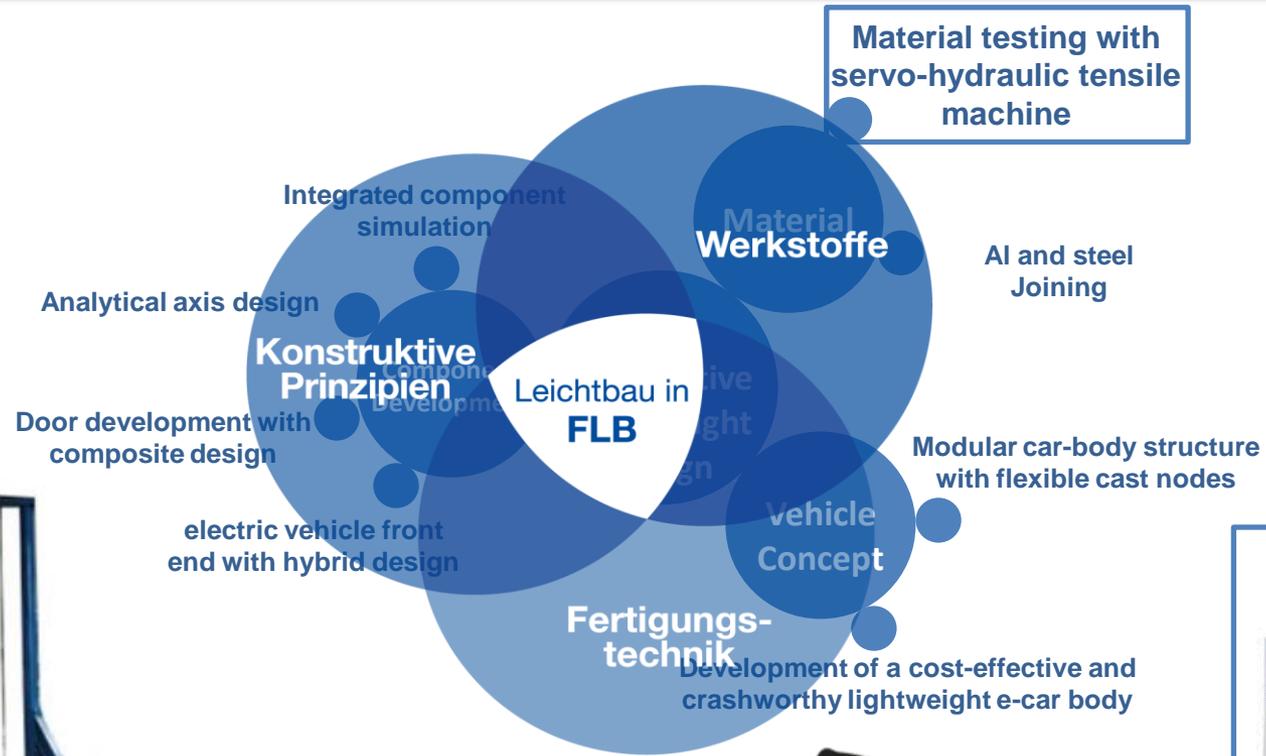


Numerical stress wave analysis in LS-DYNA and force measurement at strain rates up to 1000 /s of a high speed tensile machine

Prof. Xiangfan Fang and Dr. Jie Li

Institute of Automotive Lightweight Design
University of Siegen, Germany



Body development at FLB: StreetScooter City Car



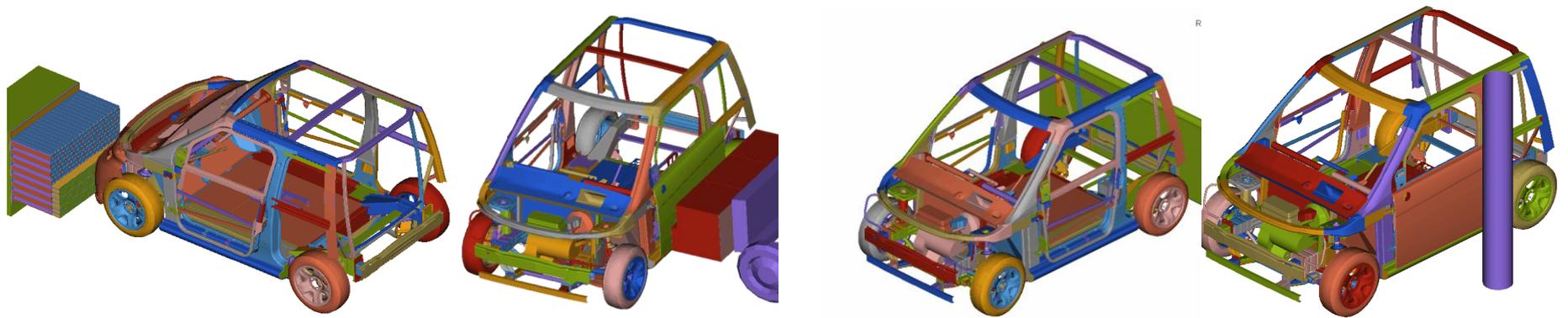
Frankfurt Auto Show 2011



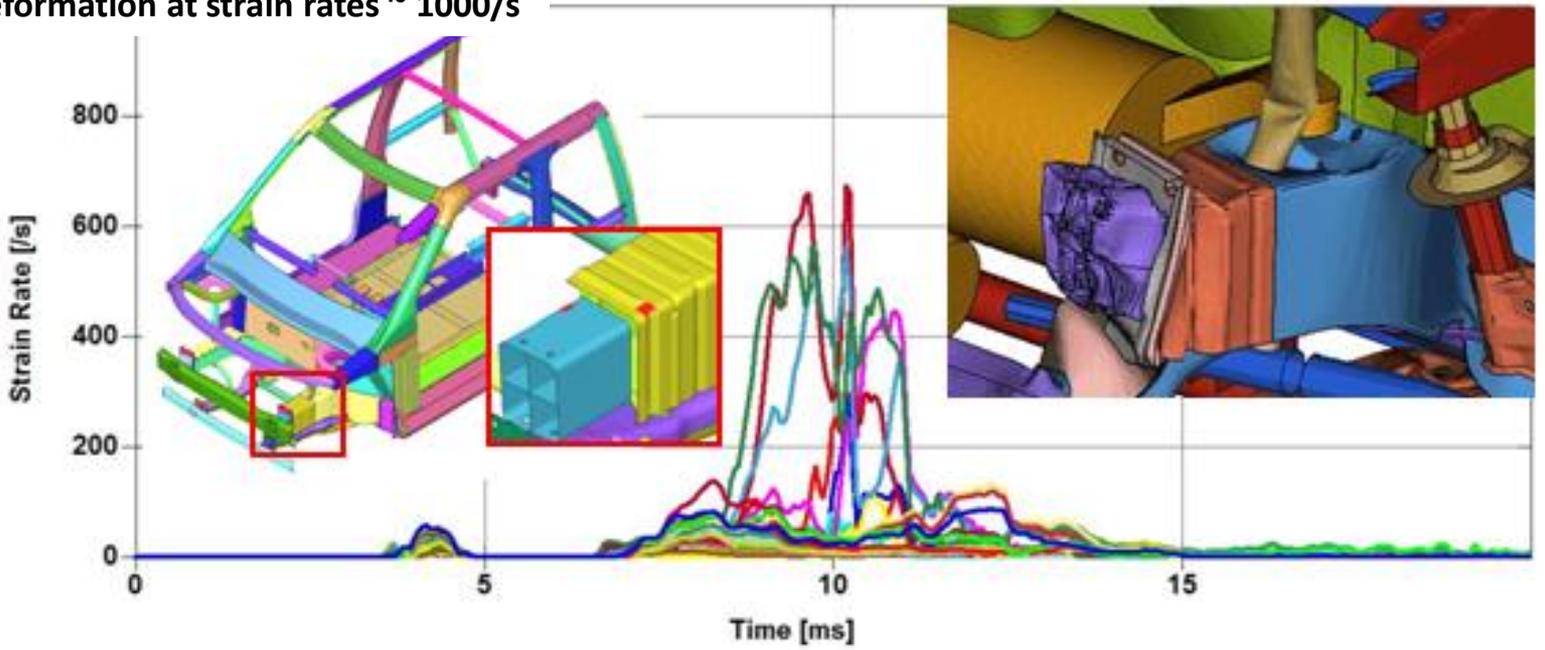
Deutsche Post in Bonn, 79 Cars

Cost-effective Body Structure for an E-vehicle, Xiangfan Fang, Jie Li, Stefan Kurtenbach, ATZ - Automobiltechnische Zeitschrift, May 2014.

Mat. Data for Crash Simulation at Strain Rates up to 10^3 /s

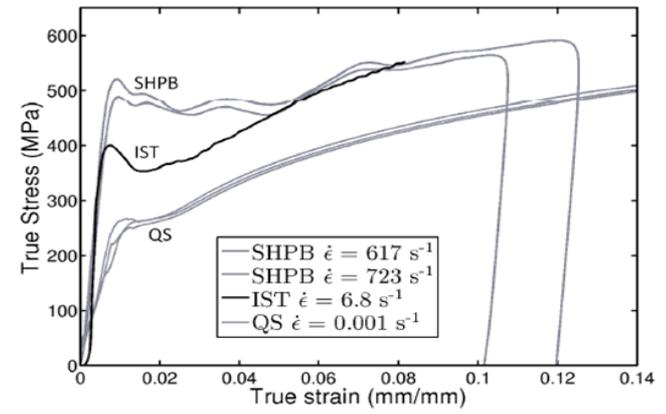
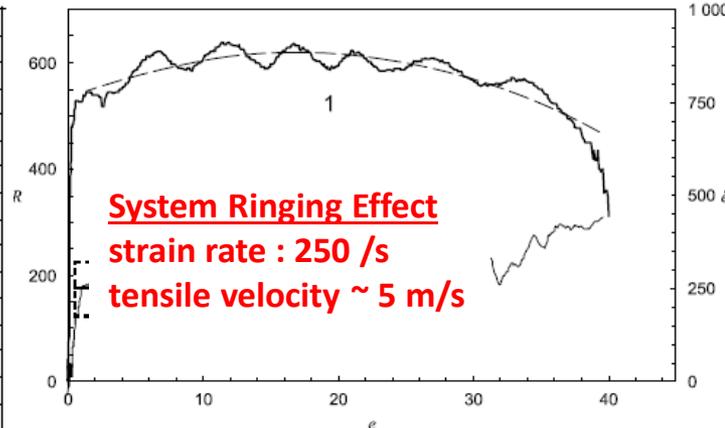
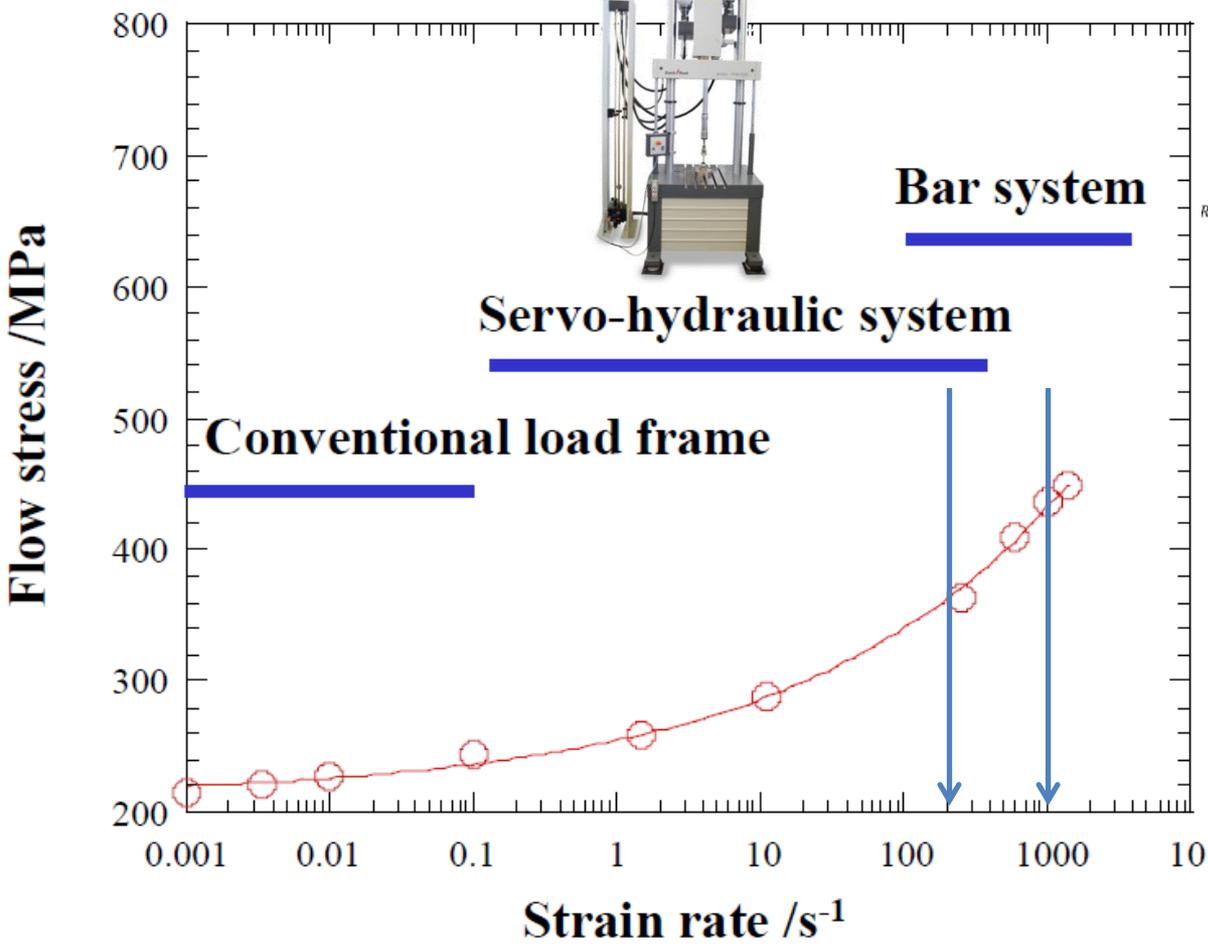


Plastic deformation at strain rates $\sim 1000/s$



Cost-effective Body Structure for an E-vehicle, Xiangfan Fang, Jie Li, Stefan Kurtenbach, ATZ - Automobiltechnische Zeitschrift, May 2014.

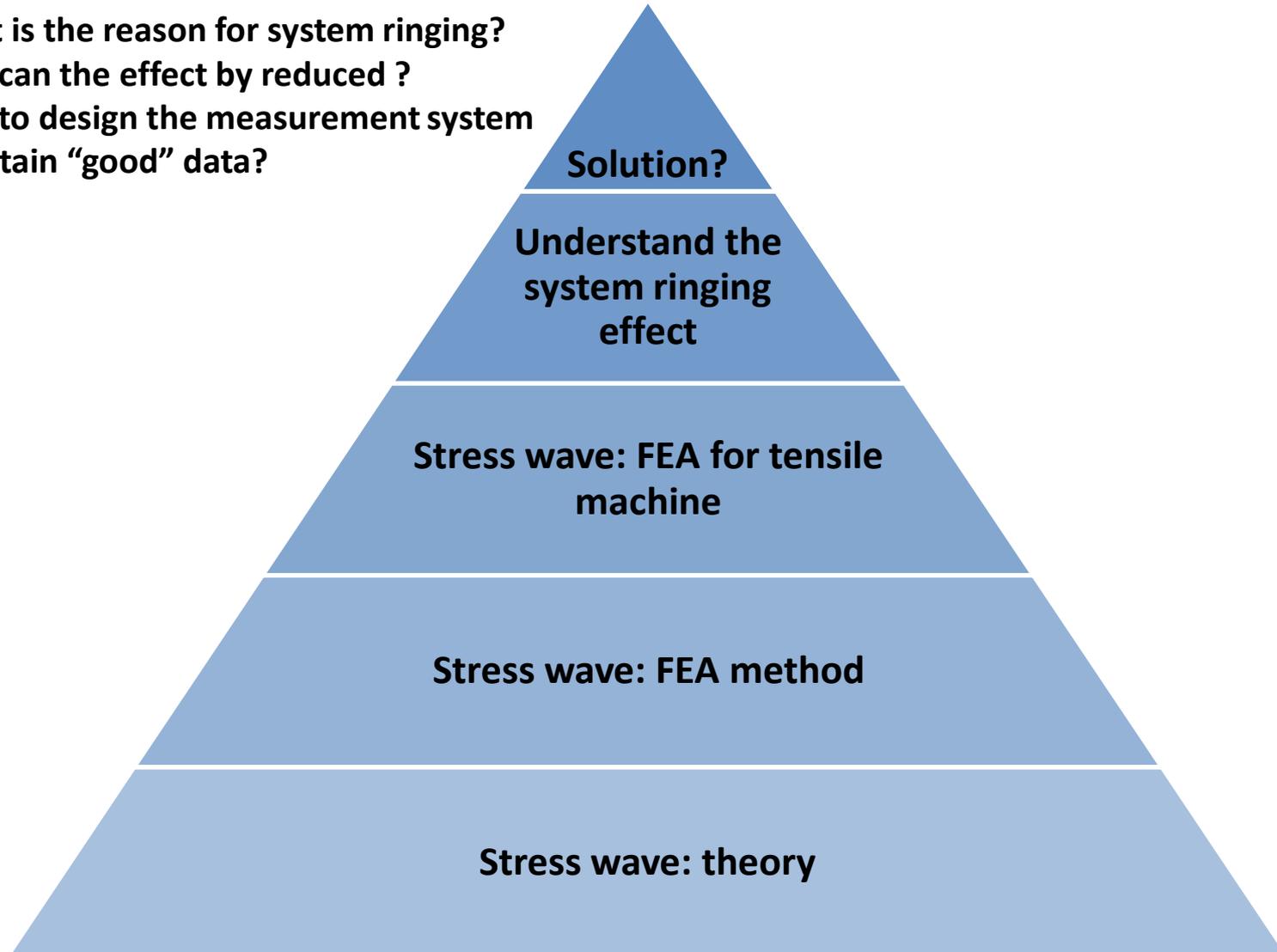
High Strain Rate Tensile Test: The state of the art



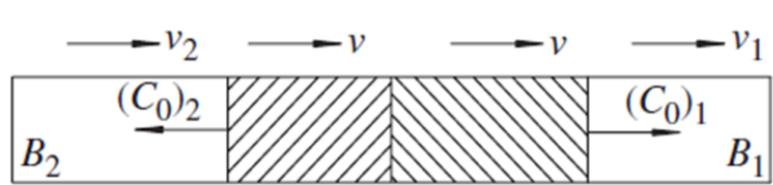
System Ringing Effect: great challenge for force measurement between 2 m/s and 20 m/s.

Borsutzki M, Cornette D, Kuriyama Y, et al. (2005) Recommendations for Dynamic Tensile Testing of Sheet Steels. Intern. Iron and Steel Institute
International Organization for Standardization (2011) Metallic materials -- Tensile testing at high strain rates -- Part 2: Servo-hydraulic and other test systems; ISO 26203-2.

- What is the reason for system ringing?
- How can the effect be reduced?
- How to design the measurement system to obtain “good” data?

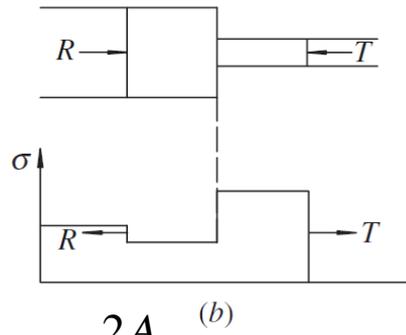
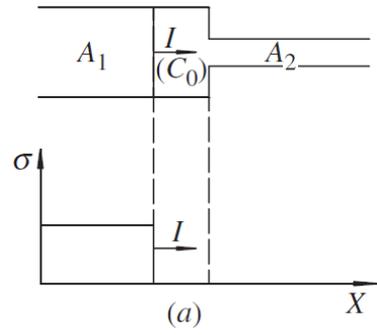


Stress wave: Theory and FEA



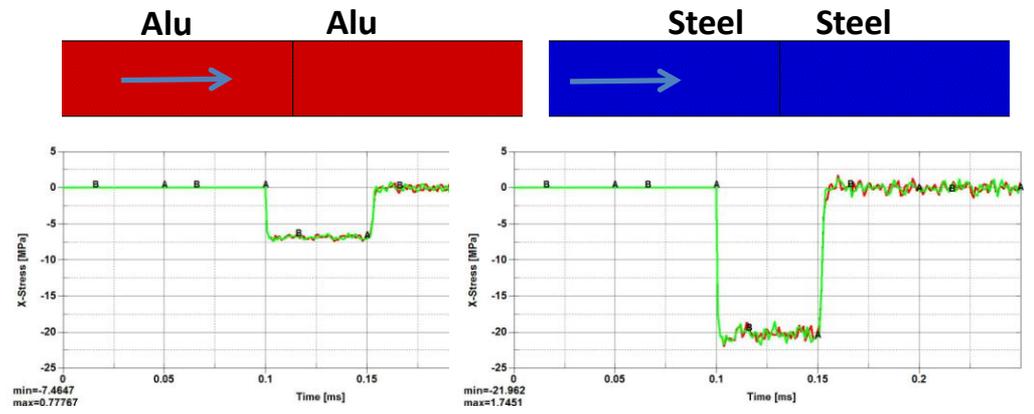
$$\sigma = -(1/2)\rho_0 C_0(v_2 - v_1)$$

$$v = \sqrt{\frac{E}{\rho}}$$

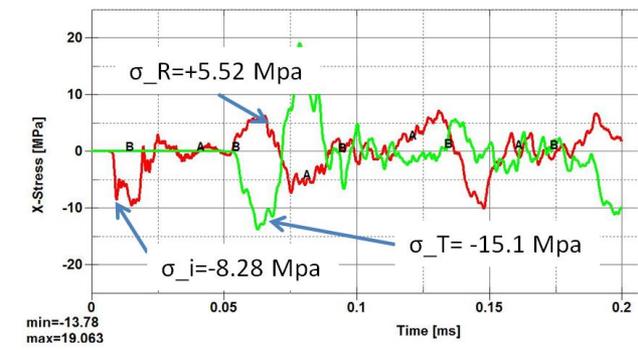
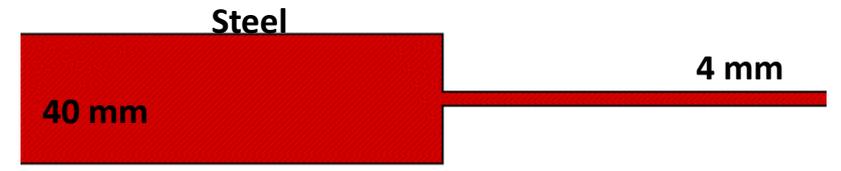


$$\sigma_T = \sigma_i \frac{2A_1}{A_1 + A_2}$$

$$\sigma_R = \sigma_i \frac{A_2 - A_1}{A_2 + A_1}$$



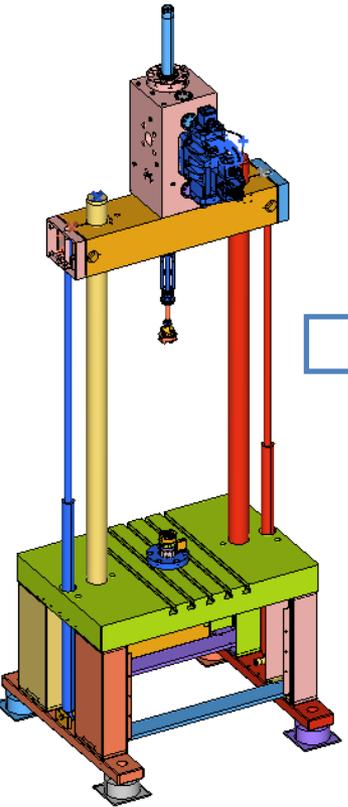
Alu		Steel	
FEA	Theory	FEA	Theory
7.0	6.87	20.27	20.30



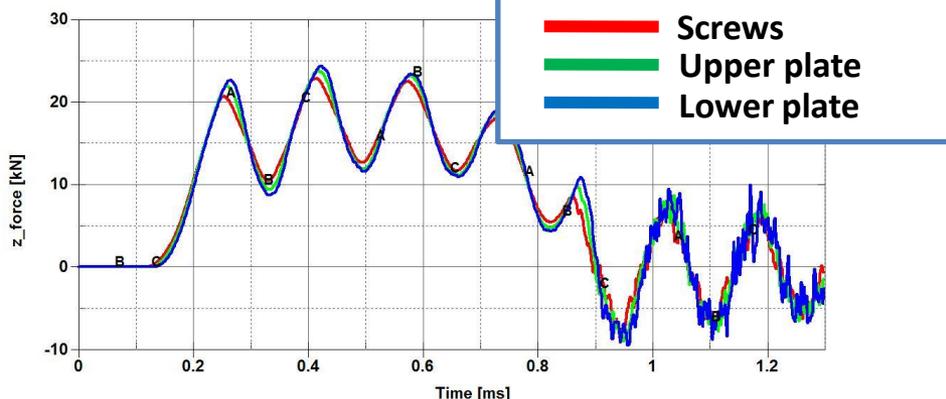
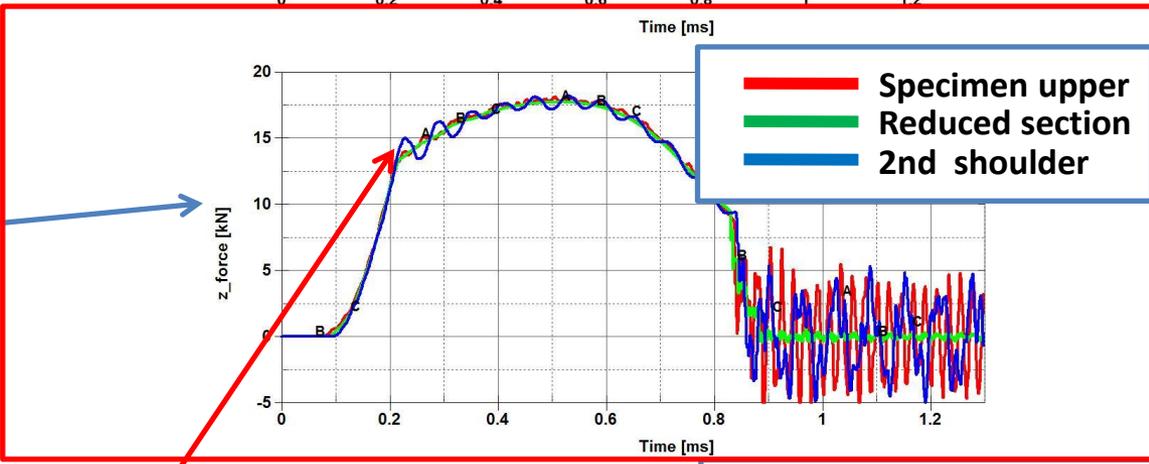
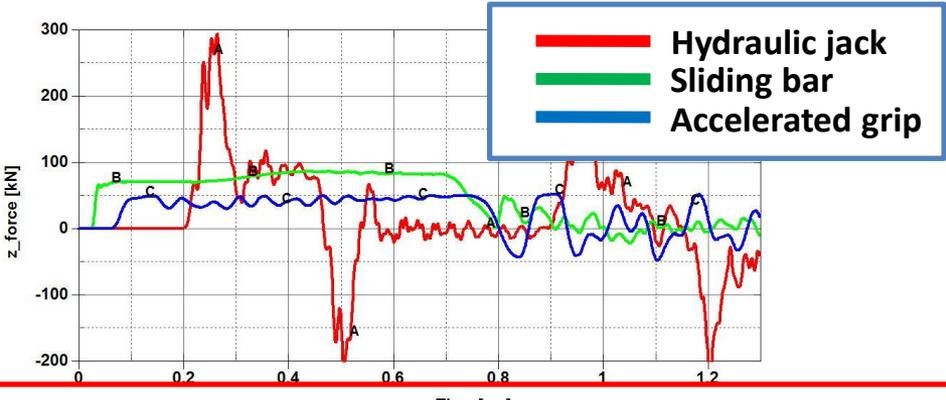
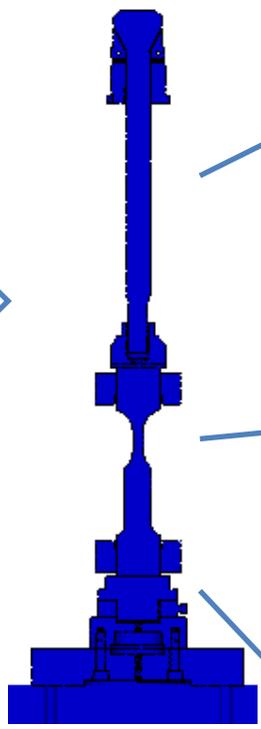
Wang L (2007) **Foundations of Stress Waves**, illustrated edition. Elsevier Science

Stress wave: FEA for HTM 5020 (Zwick)

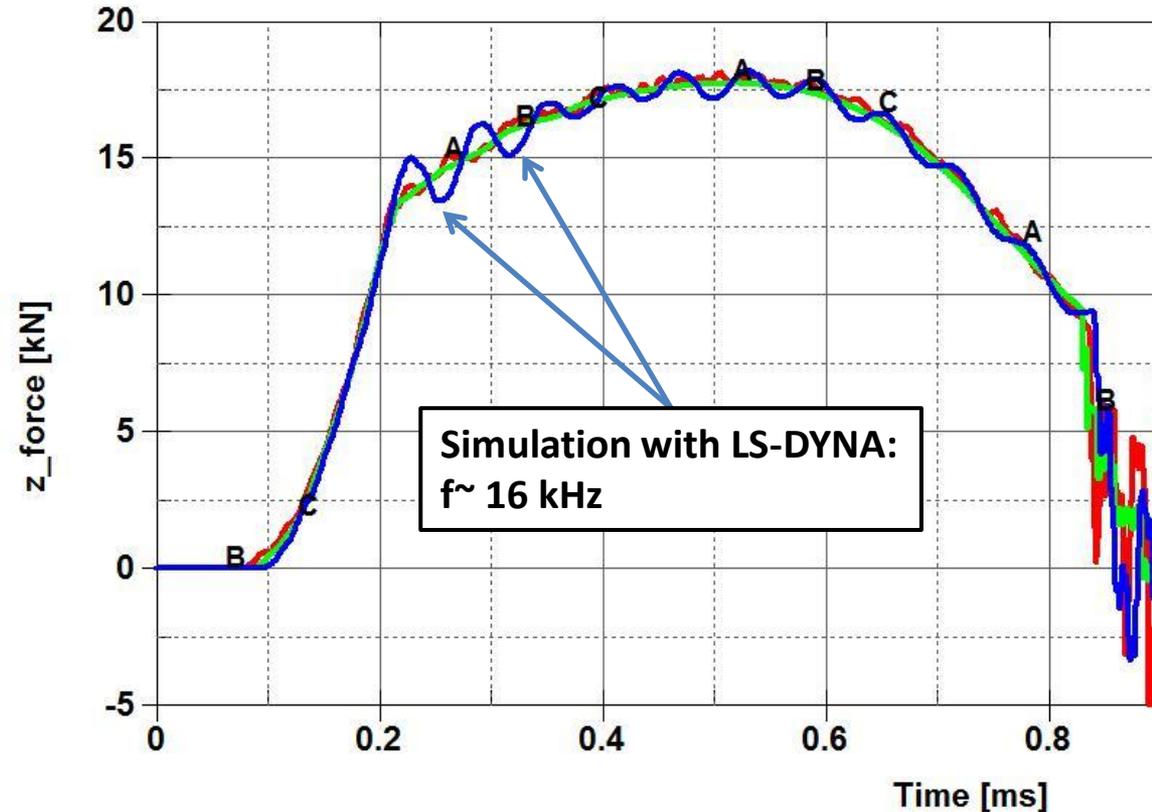
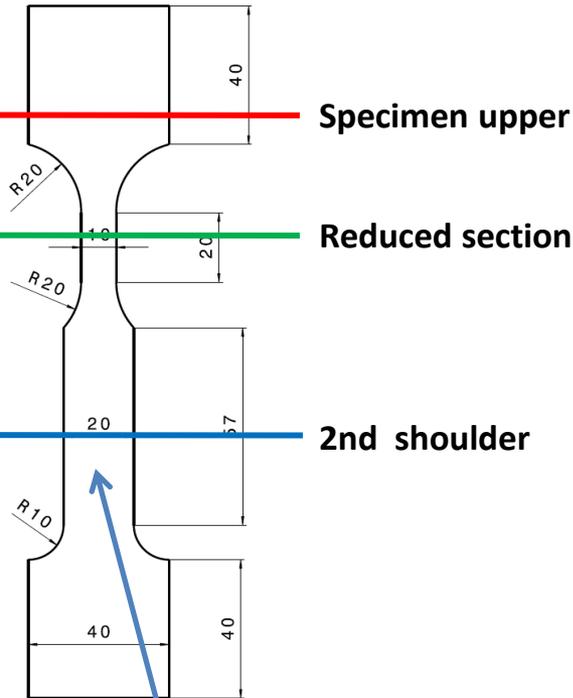
CAD of HTM 5020
(provided by Zwick)



Stress wave simulation
in LS-DYNA



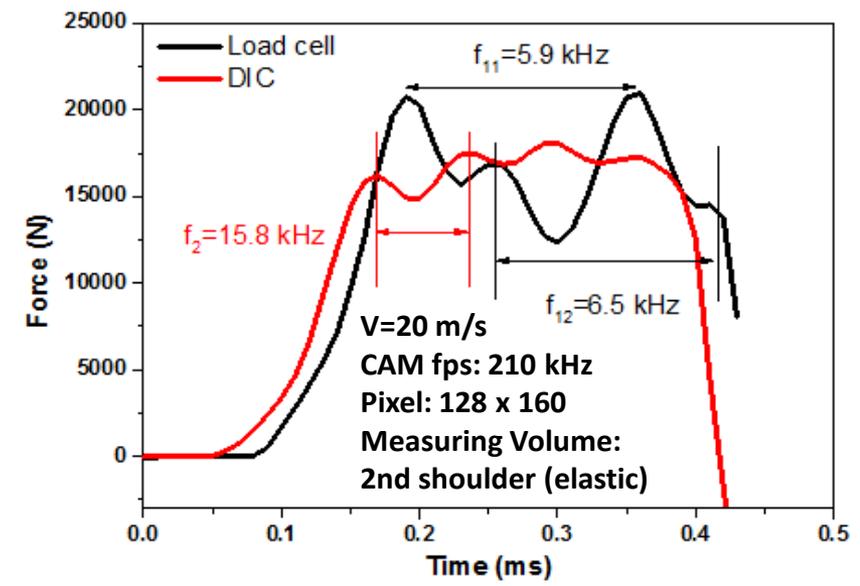
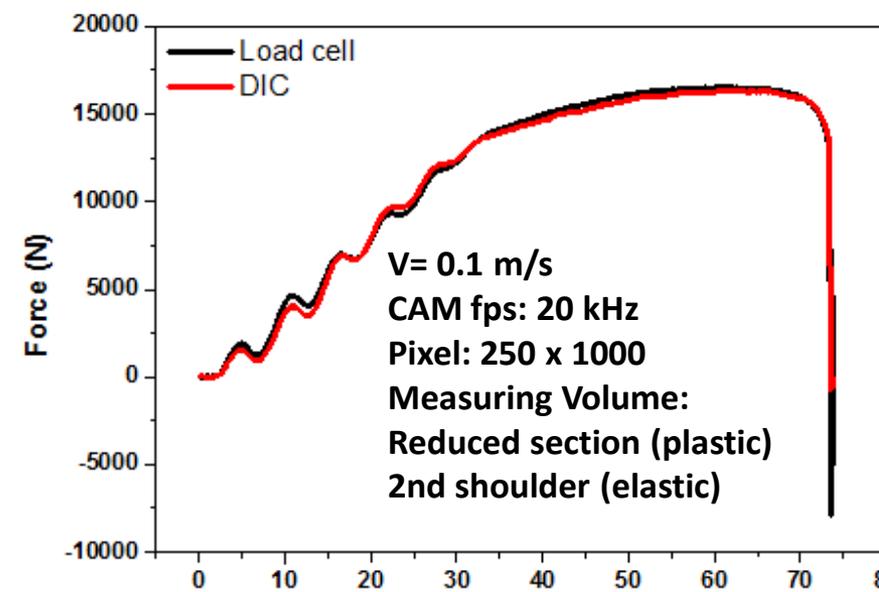
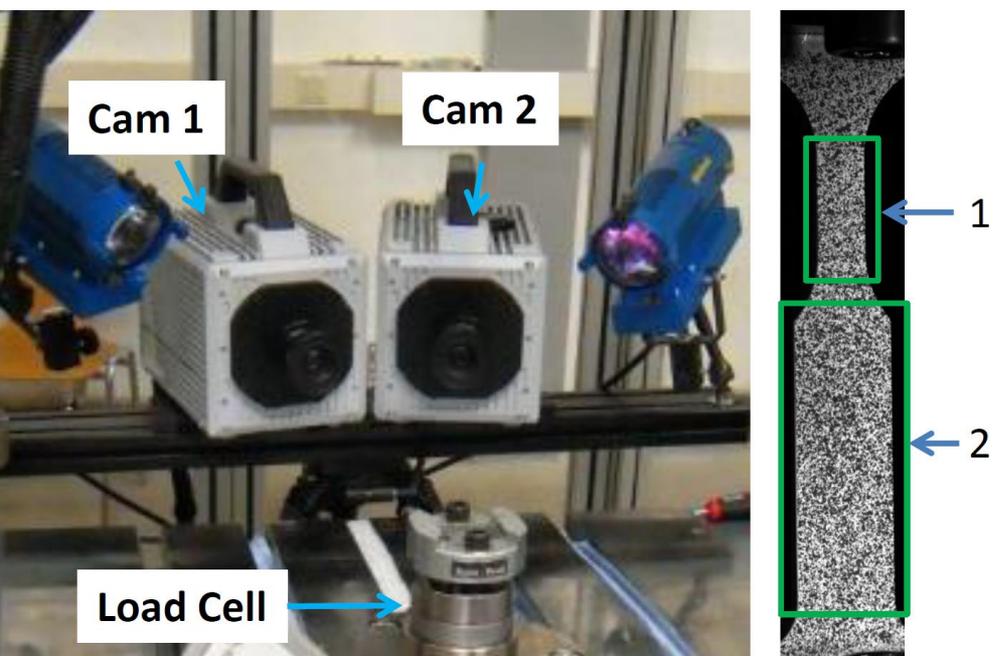
Stress Wave effect negligible within the new Specimen!
 -> Frequency analysis
 -> additional test to confirm



Conclusion:

1. negligible oscillation within the reduced section of the specimen
 2. very little oscillation within the 2nd shoulder with $f \sim 16$ kHz
- > Force measurement with elastic strain of the 2nd shoulder?
 $F = e_{\text{elastic}} \times \text{width} \times \text{thickness} \times E$

DIC force with ARAMIS, Experiments



$F_{DIC} = e_{elastic} \times width \times thickness \times E$

$$f = \frac{1}{2L} \sqrt{\frac{E}{\rho}}$$

E=210 GPa,
ρ= 7.85E-6 kg/mm³
L=149 mm
=> f= 17.4 kHz

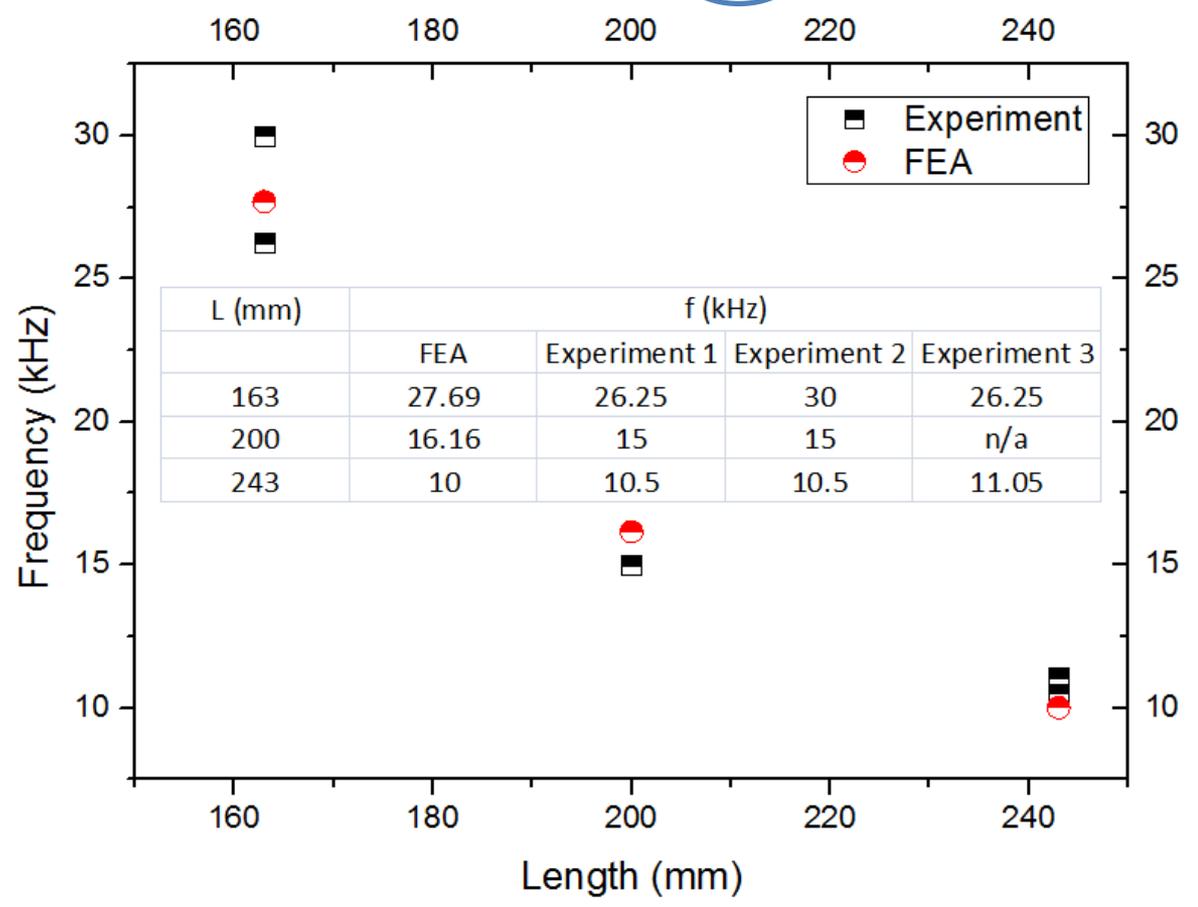
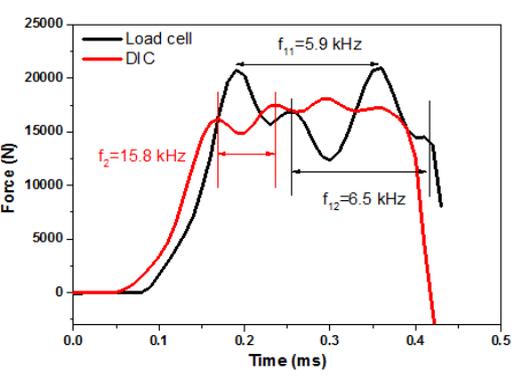
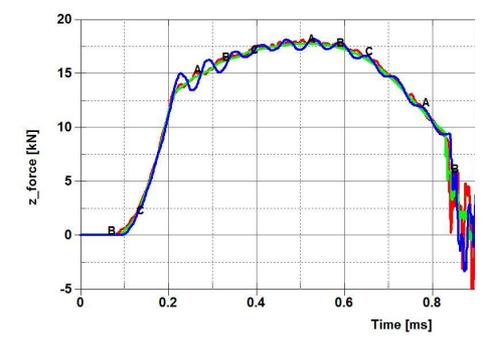
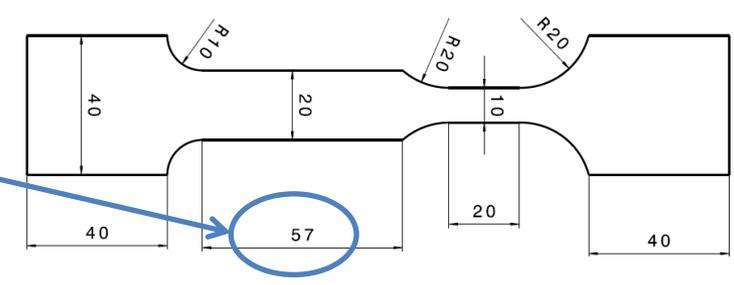
Published in "Experimental Mechanics"
Li J, Fang X (2014) Exp Mech 54:1497–1501

Is the Simulation correct? -> Further Validations

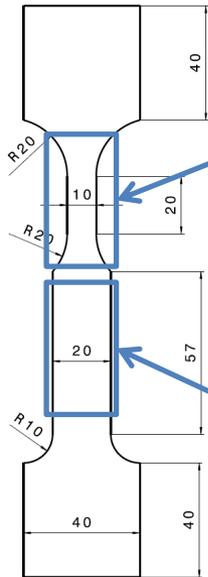
Simulation with LS-DYNA
16 kHz

DIC Experiment: 15.8 kHz

Additional Experiments with different Specimen Length (L)

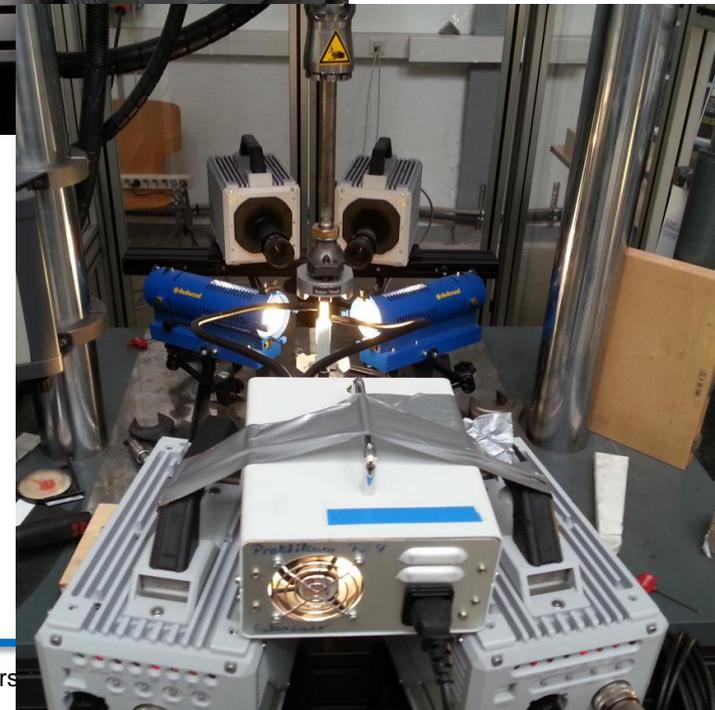


strain-stress measurement at 10^3 /s, 2x 3D DIC measurement

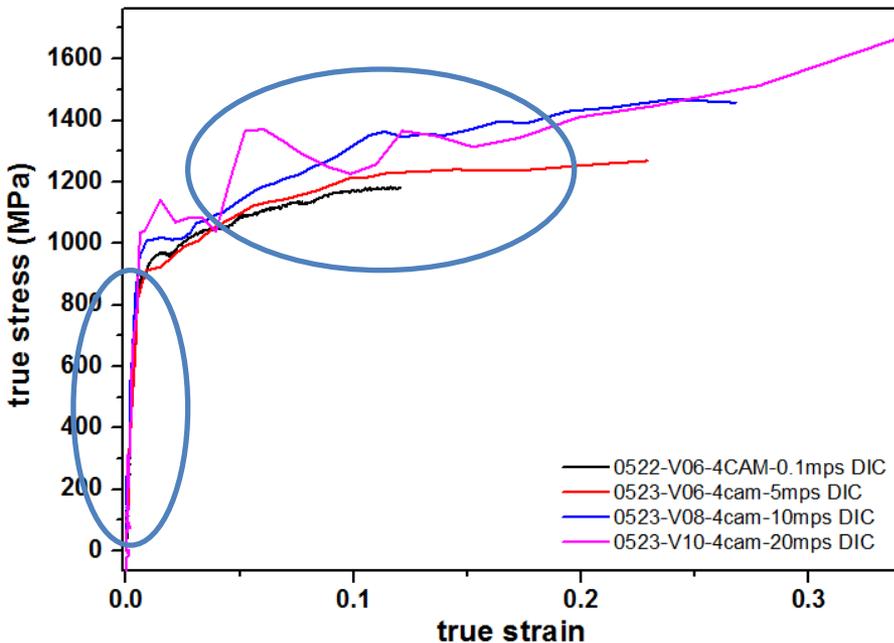


1. 3D DIC with 2 SA 5 Camera
plastic deformation
strain measurement

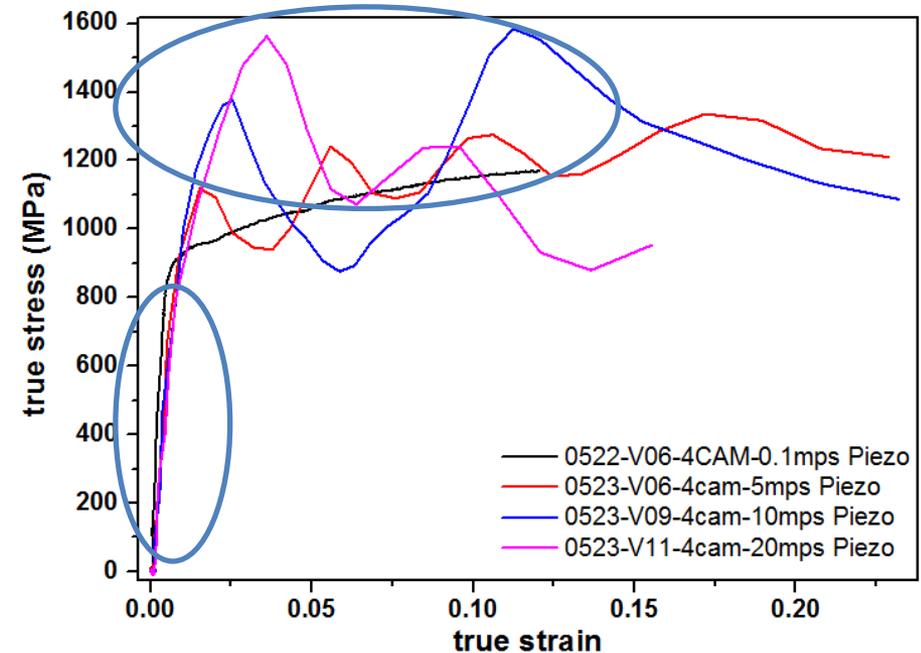
2. 3D DIC with 2 SA 5 Camera
elastic deformation
force measurement
stress measurement



all-optical stress strain determination



conventional method with piezoelectric load cell

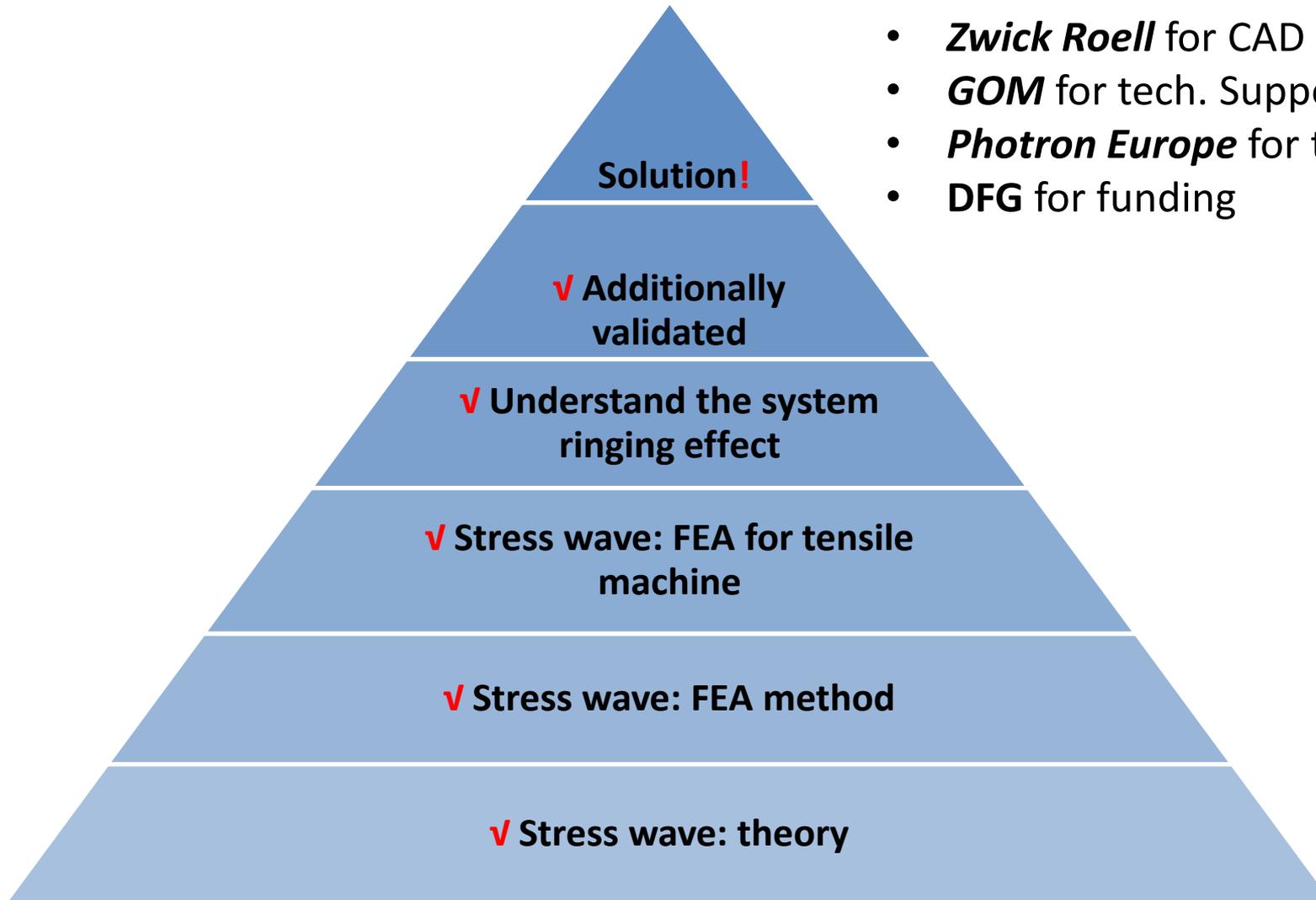


conclusion:

negligible oscillation up to 10 m/s

much lower oscillation at 20 m/s

-> can be further reduced with better specimen geometry and changes on test equipment!



- **Zwick Roell** for CAD of HTM5020
- **GOM** for tech. Support
- **Photron Europe** for tech. Support
- **DFG** for funding